NASA CONTRACTOR REPORT 166362

(NASA-CR-166362) INVESTIBATION OF CORRELATION DETWEEN FULL-SCALE AND FIFTH-SCALE WIND TUNNEL TESTS OF A BELL HELICOPTER TEXTRON HODEL 222 Final Report (Bell Helicopter Co.) 401 p HC A18/HF A01 G3/05 28567

n82-29315

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Investigation of Correlation Between Full-Scale and Fifth-Scale Wind Tunnel Tests of a Bell Helicopter Textron Model 222

Patrick K. Squires Bell Helicopter Textron



CONTRACT NAS2-10773 June 1982



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Prepared for Ames Research Center under Contract NAS2-10773



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MODEL 222

Patrick K. Squires June 1982

Ву

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CR - 166362

Prepared under Contract No. NAS2-10773 by

BELL HELICOPTER TEXTRON INC. Fort Worth, Texas

For

AMES RESEARCH CENTER
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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LIST OF SYMBOLS

D\đ	drag/dynamic pressure wind tunnel axis (positive aft), $\mathcal{E}t^2$
r\đ	lift/dynamic pressure, wind tunnel axis (positive up), ft^2
bw\đ	pitching moment/dynamic pressure wind tunnel axis (positive nose up), ft3
RM/q	rolling moment/dynamic pressure wind tunnel axis (positive right), ft3
đ	dynamic pressure, lb/ft2
A\đ	side force/dynamic pressure wind tunnel axis (positive right), ft^2
M/d	yawing moment/dynamic pressure wind tunnel axis (positive nose right) ft^3 .
α	angle of attack (positive nose up), deg
ψ	yaw angle (positive nose right), deg

SUMMARY

An experimental investigation has been performed to investigate reasons for lack of correlation between data from a fifth-scale wind tunnel test of the Bell Helicopter Textron Model 222 (Vought LSWT 550 November 1977) and a full-scale test of the Model 222 prototype in the NASA Ames 40-by 80-foot tunnel. (November 1977) This investigation centered around a carefully designed fifth-scale wind tunnel test (Vought LSWT 630 November 1981) of an accurately contoured model of the Model 222 prototype mounted on a replica of the full-scale mounting system. Figures 1 and 2 show the improvement in correlation for drag characteristics in pitch and yaw with the fifth-scale model mounted on the replica system. Interference between the model and mounting system was identified as a significant effect and was concluded to be a primary cause of the lack of correlation in the earlier tests. This conclusion is supported by the results presented in this report. The program documented herein was sponsored by contract (NAS2-10773) with the National Aeronautics and Space Administration, Ames Research Center. The Technical Monitor was Dr. #11iam Warmbrodt.

1. INTRODUCTION

The Bell Helicopter Textron Model 222 Light Executive Twin prototypes began flight test development in 1976. Actual performance was less than predicted by analysis based on drag data measured during extensive fifth-scale wind tunnel tests. This performance difference called into question the use of fifth-scale wind tunnel tests to provide airframe drag data for performance prediction.

1.1 BACKGROUND

In a joint effort during the fall of 1977, NASA Ames and BHT conducted two wind tunnel tests of the Model 222 directed toward answering this question. The first test, in the 7- by 10-foot low speed wind tunnel at Vought Aeronautics Corporation, during November of 1977, involved a fifth-scale model. The second test also in November of 1977 was conducted in the 40by 80-foot wind tunnel at NASA Ames Research Center using an actual Model 222 prototype which was removed from flight status, modified for mounting in the test section, and later returned to flight status. References 1 and 2 are reports of the fifthscale test and the full-scale tests respectively. Tables B-I and B-II of the Appendix present the run schedules of these tests. Figure 3 shows the two models in a side-by-side comparison. One objective of these tests was to provide proof that baseline aerodynamic data obtained in the full-scale test of an actual prototype airframe would correlate well with tests of an accurate model of the prototype, and thereby, validate the method of using fifth-scale tests to predict helicopter airframe aerodynamic characteristics. Secondary objectives were to document the validity of using fifth-scale testing to investigate the aerodynamic effects (particularly drag) of the components of the helicopter airframe and to evaluate the effect of modifications intended to reduce drag. To accomplish these objectives, a number of configurations were tested. These configurations ranged from a basic fuselage, with all major components except the fin removed, to the complete helicopter shown in Figure 3. While data on all six components of force and moment were taken, the major thrust of the tests was to investigate drag.

1.2 CORRELATION BETWEEN FULL-SCALE AND ORIGINAL FIFTH-SCALE (LSWI 550) TESTS

The correlation between full-scale and fifth-scale data from these two tests was rather disappointing. Longitudinal data for both the hasic fuselage and complete helicopter showed large discrepancies. Lateral data showed good agreement in side force and yawing moment but compared very poorly in drag.

Figures 4 through 6 compare lift, drag, and pitching moment characteristics of the basic fuselage in pitch for both the fifth-scale test (LSWT 550) and the NASA Ames 40- by 80-foot test (full-scale). The basic fuselage configuration as defined in this investigation included the fuselage, cowling (with inlets, exhausts and cooling screens closed), nose gear door closed, tail rotor hub, production tail rotor gearbox fairing, exhaust ejector fairing and vertical fin with 10 inch cap. The data in these figures are corrected by subtracting tare and interference values obtained in the following ways. For test LSWI 550, T&I corrections originated with a previous test of the Model 222 (LSWI 439 November 1973). The only corrections available for the full scale test were the usual static tares and wind-on tares measured for the support system alone. Figures 7 through 9 compare lift, drag, and pitching moment of the complete helicopter in pitch for the two tests. The complete helicopter configuration as defined in this investigation was identical to the flying prototype except that inlets and exhausts were closed and the main and tail rotor blades were removed. Minor configuration differences between the prototype and the fifth-scale model of LSWT 550 are discussed in Section 2.1. Figures 10 through 12 compare side force, drag, and yawing moment of the complete helicopter in yaw for both tests. Figure 4 shows that the lift curve slope for the LSWI 550 data is approximately two times the full-scale value and the fifthscale angle of zero lift is some 7 degrees lower. Figure 7 which compares lift data for the complete helicopter shows better agreement at nominal angles of attack (-4 degrees to +6 degrees) where slopes are essentially equal and angles of zero lift differ by only 2 degrees. The full-scale and fifth-scale data show considerable divergence, however, at very high angles of attack. Figure 5 compares drag of the basic fuselage for the two tests. The drag at an angle of attack of zero degrees differs by approximately 2 square feet and the angle of attack for minimum drag is quite different. Figure 8, which compares drag for the complete helicopter, shows better agreement in the location of the drag bucket, but the drag at zero angle of attack differs by almost 4 square feet while the variation of drag with angle of attack is also quite different. Figure 6 shows a disagreement in pitching moment slope and the value of pitching moment at an angle of attack of zero for the basic fuselage. Figure 9 shows similar pitching moment slopes for the complete helicopter in the range of -4 degrees to +4 degrees, although the slopes at higher angles and the values of pitching moment at zero angle of attack are considerably different.

Figures 10 and 12 show much better correlation in side force and yawing moment with yaw angle for the complete helicopter. The drag curves in Figure 11, while showing similar shapes, are different by about 4 square feet in minimum drag.

In general, the differences in the aerodynamic characteristics shown in Figures 4 through 12 are typical of those found in the remainder of the data for the full-scale and LSWI 550 tests tests.

Attempts to explain the lack of correlation have tended to the premise that the fifth-scale data were questionable due to Reynolds Number effects, inaccurate modeling of contours and model details, imperfect testing and data reduction, or a combination of these. Another idea was that because of the unique mounting system used for the full-scale test, a large and undetermined amount of interference was present in the full-scale data, even after the wind-on tare corrections were removed.

1.3 APPROACH TO THIS INVESTIGATION

It was the intent of this correlation study to carefully investigate the various possible causes of disagreement between these tests and measure or mitigate their effects in a second well-designed fifth-scale wind tunnel test. The approach used is detailed in the following sections and consisted of the following steps. First, the data generated during the subject tests were reviewed to check for possible errors in comparisons made or corrections applied. Next, the fifth-scale model was measured in an effort to determine how closely it matched the prototype aircraft used for the full-scale wind tunnel test in contour and detail. As a result of contour discrepancies measured, the model was modified to the full-scale lines. A fifth-scale model of the 40- by 80-foot test mounting system was designed and built to duplicate the full-scale mount in both form and function. Additionally, hardware was designed to allow tare and interference measurements. A 90-hour wind tunnel test was conducted of the corrected fifth-scale model on both a conventional single strut and the fifth-scale replica of the full-scale three-point mounting system. The data from this test (LSWT 630) were analyzed and compared with data from the previous tests and led to conclusions about the reasons for disagreement.

2. DATA REVIEW

2.1 COMPARISON OF TEST CONFIGURATIONS

The data review task began with a comparison of the run schedules and configuration nomenclature of the full-scale and fifth-scale (LSWI 550) tests to determine if comparisons were made using equivalent aircraft configurations. There were virtually no perfect configuration matches. In the case of the basic fuselage configuration comparison (LSWT 550 Run 19 versus full-scale Run 68) the LSWI 550 test used the 15-inch rather than the 10-inch fin extension, had no tail rotor hub, and no exhaust ejector fairing. For the complete helicopter comparison in pitch LSWY 550 Run 22 mersus full-scale Run 20 several differences were noted. The LSWT 550 configuration had the main rotor hub fixed rather than rotating, used the 15-inch rather than 10-inch fin extension, no production protuberances, and no open cowling screens. Some of the differences discovered would have no measurable effect on the data. However, it is difficult to make any judgment about many of the configuration comparisons because detailed definition of the parts involved does not exist. An example of this difficulty is the designation P2 which covers production protuberances. An examination of configuration photos (of Ref. 2) shows that while pitot tubes were included in the definition of P2 they were not removed with the rest of the P_2 items after Run 28 (Table B-II) in the full-scale tesc. An additional obstacle to a completely rigorous evaluation of the configurations tested earlier is that many of the components of the prototype and fifth-scale model were one-of-kind items which were documented only by photographs. Consideration of these facts led to the decision, that for the proposed test, an effort would be expended in duplication of only those configurations for which sufficient documentation was available.

2.2 EVALUATION OF CORRECTIONS APPLIED

The corrections applied to the full-scale and fifth-scale data were examined. These corrections were for tare, interference, and flow alignment.

Because of the design of the 40- by 80-foot test section it is not feasible to measure tare and interference (T&I). These measurements require that the model be mounted inverted, as well as upright, and that an image of the support system be suspended from the ceiling of the test section. A detailed discussion of the most widely used methods of obtaining T&I's may be found in Reference 3.

During the full-scale tests a series of runs was made to approximate the tare of the mounting system. These runs (1 through 4 of Table B-II) were made before the aircraft was mounted. Since the vertical strut extended up inside the fuselage to the pylon mounting structure, during the tare runs this portion was removed by fitting a dummy strut which was cut off at the fuselage floor.

Interference effects were expected to be minimized by fairing the vertical strut and placing the faired horizontal strut over seven feet below the model. Since alignment corrections are derived from the same upright and inverted runs used for T&I measurements (see Reference 3), no alignment corrections could be made to the full-scale test data.

The tare and interference corrections used for the LSWT 550 data were made during the original Model 222 fifth-scale test (LSWT 439). These corrections were measured using the conventional upright and inverted runs with and without image system. Alignment corrections were also measured during the original LSWT 439 test. The older corrections were considered to be acceptable because the fifth-scale model had not changed substantially between tests.

Both the full-scale and fifth-scale tests were made with the model on the center line of the test section. No wall corrections were applied in either test.

A check of the data reduction for both tests revealed that the corrections used were applied correctly.

3. EVALUATION OF GEOMETRIC SIMILARITY

Although the original fifth-scale model appeared to accurately represent the Model 222 prototype tested full-scale (Figure 3 shows a side-by-side comparison) this fact was not verified at the time of the LSWI 550 test. This section discusses the procedure used to substantiate the accuracy of the model for this correlation study.

3.1 MEASUREMENT OF FUSELAGE CONTOURS

The differences that existed between the full-scale prototype and the model were determined using a set of templates which represented the fuselage and cowling contours of the prototype. This was done by transferring fifth-scale prototype lines at various station cuts onto aluminum sheets which were then cut to form female templates. These templates were then used to check the model. Figures 13 and 14 show fuselage and cowling contours at several station cuts illustrating the differences between the unmodified model's lines and the prototype lines. These differences are concentrated in the area of the cowling. No contour differences are shown on the basic fuselage because changes to the fifth-scale model for other tests since 1977 made it impossible to determine what the contours had been for the LSWI 550 test.

3.2 MEASUREMENT OF COMPONENT PARTS

Wings were checked and verified to be correctly sized and mounted at the proper incidence.

The horizontal stabilizer used during the LSWT 550 had been destroyed.

The fin used during the LSWT 550 test had been modified and its exact configuration during that test could not be verified. The current configuration did not agree with the prototype.

The main and tail rotor hubs showed evidence of having been modified but the current configuration did agree with the prototype. The configuration for the LSWT 550 test could not be verified.

Endplates were checked and verified to be of the correct size. Configuration photographs of the LSWT 550 test appear to show the endplates mounted with nose left incidence while the correct setting is 3 degrees nose right.

As mentioned in Section 2, the detail items lumped together under the categories of "production protuberances" or "flight test protuberances" were not well documented at the time of the

full-scale and LSWT 550 tests and many were later lost or destroyed. The only items remaining in this category were the tail rotor guard, the tail skid, and a set of windshield wipers. These items appeared to represent their prototype counterparts.

The Model 206 type afterbody (full-scale Run 23 and LSWT 550 Run 27), thin wing (full-scale Run 32 and LSWT 550 Run 41) and flotation bags (full-scale Run 5 and LSWT 550 Run 34) are typical of a large group of one-of-a-kind parts which were not documented and no longer could be located for measurement.

4. MODIFICATION OF THE FIFTH-SCALE MODEL

Based on the measurements described in Section 3, which were made to determine the geometric similarity between the fifth-scale model and the prototype, it was necessary to recontour, modify, or completely rebuild certain components of the model. This section describes the modification process.

4.1 MODIFICATION OF FUSELAGE CONTOURS

The largest discrepancies noted were in the basic fuselage and cowling. The fuselage and tailboom were brought to contour by filling and reshaping the original model. The aluminum templates which were used for contour checking served as a guide to ensure accurate duplication of the prototype lines. The cowling was completely new.

4.2 MODIFICATION OF COMPONENT PARTS

A new set of wings, with dummy landing gears in the retracted position, and a set of landing gear doors were constructed.

A new horizontal stabilizer was constructed with a removable leading edge slat.

The lower portion of the fin was modified to match the prototype and the upper portion was fitted with a removable cap which allowed rapid conversion between the $\rm V_1$ and $\rm V_2$ configurations.

Other miscellaneous components which had to be made included pitot tubes, exhaust ejector fairing, tail rotor gearbox fairing, fuel sump recesses and covers, and pilots sliding window.

5. DESIGN AND FABRICATION OF FIFTH-SCALE SUPPORT SYSTEM

5.1 REQUIREMENT FOR A REPLICA MOUNTING SYSTEM

A suspected cause of disagreement between the full-scale and fifth-scale aerodynamic data was the unique mounting system in the full-scale test. The full-scale system, which is shown in a side-by-side comparison with the fifth-scale mount in Figure 3, was a rather complicated interface between the 40- by 80-foot tunnel's three-point mounts and the pylon mounting structure of the Model 222 airframe. Figure 15 is a schematic of the fullscale mounting system which shows the general arrangement and indicates the motion of the model in pitch. Figure 16 is a schematic of the single strut mounting system used during both fifth-scale tests. An important part of this correlation study was to evaluate the tare and interference effects of the fullscale mount by modeling it in fifth scale and obtaining complete T&I measurements. A straightforward approach using an image system to duplicate the articulation of the three-point mounting was too costly, and instead, an indirect approach was conceived using two separate mounting systems. First, the model would be mounted on the usual single strut system and tested both upright and inverted, with and without the image system in order to measure T&I corrections in the classical manner. The principal advantage of this method of evaluating T&I's was that the image system for the single strut would be quite simple compared to the image required for the three-point mount. Using the T&I corrections obtained in this fashion the single strut data would be processed to produce a set of "model-alone" aerodynamic data for all representative configurations. Next, the model would be mounted on the fifth-scale three-point system and the runs made on the single strut mount would be repeated. By subtracting the previously obtained model-alone data from the raw data with this replica three-point mount, a set of T&I corrections would be derived for each of the repeated runs.

5.2 <u>DESIGN AND FABRICATION OF MOUNTING HARDWARE</u>

Based on drawings and photographs of the original full-scale mounting system, BHT designed and fabricated a fifth-scale replica system. This replica, shown in Figure 17, duplicated the original very closely in both form and function with the following exceptions. Because the 40- by 80-foot test section would correspond to a fifth-scale 8- by 16-foot section it was necessary to shorten the replica mounting system by 6 inches (2.5 ft full-scale) in order to locate the model on the centerline of the 7- by 10-foot section. The portion removed from the fifth-scale replica was at floor level and not considered to produce a significant contribution to interference because of its distance from the model. The other exception was in the

representation of the rear pitch strut of the three-point mount. The pitch strut in the 40- by 80-foot test section is a series of nested lead screws of graduated diameters which are rotated automatically to change overall length and thereby pitch the model. In this replica the pitch strut was represented by a strut of constant diameter.

The replica three-point system was also provided with removable vertical fairings and a dummy vertical strut. The vertical fairings were removed for yaw runs during the full-scale test while the dummy strut was used to represent that portion of the support strut below the belly of the aircraft during wind-on tare runs. In addition to the hardware associated with the three-point mounting system, an image system for the single strut mount was designed and built.

6. WIND TUNNEL TEST

During the period of 29 October to 16 November 1981, Bell Helicopter Textron conducted a wind tunnel test of the refurbished fifth-scale model of the Model 222 helicopter in the 7- by 10-foot test section of the Vought Corporation Low Speed Wind Tunnel. Reference 4 is the Vought Corporation report of that test (referred to as LSWI 630).

6.1 FACILITIES AND EQUIPMENT

The modified model employed a BHT designed and fabricated pitch mechanism and angle of attack readout module which interfaces with Vought tunnel hardware. This system, including actuators, sensors, remote controls, power supply, and readout devices, is independent of the wind tunnel operating and control systems and may be moved from model to model. The purpose of the system is to allow the model to be positioned accurately at a given pitch angle. This device is capable of positioning the model to within ±0.1 degree of the desired pitch angle. Yawing of the model is accomplished by rotating the external balance turntable. The support fairing remains streamlined during yaw. Reference 5 contains more detailed information about the balance system and its capabilities.

Figure 18 shows the Model 222 mounted upright on the single-strut mount. Figure 19 shows the model mounted in the inverted position with the image system in place. This image system consists of the image strut which is attached to the model and the image fairing which is attached to the ceiling of the test section. There is no contact between the image strut and image fairing. Thus, with the image system in place, the tare of the strut, the interference between model and strut, and the interference of the fairing on the strut and model are all included in the measured aerodynamic data.

Figures 20 and 21 show the fifth-scale model mounted on the replica three-point mounting. In Figure 20 the mounting system is in the pitch configuration with both the large stationary vertical fairing and the smaller vertical strut fairing in place. Figure 21 shows the mounting system in the yaw configuration with both vertical fairings removed. Pitch motion is accomplished by moving the rear strut vertically which pivots the model about the trunnion located inside the horizon-tal fairing. Yaw motion is accomplished by rotating the balance turntable. The large vertical fairings over the main support struts between the floor and horizontal fairing rotate with respect to the turntable to remain streamlined with the airflow.

6.2 TARE AND INTERFERENCE CORRECTIONS

T&I corrections were obtained for Low Speed Wind Tunnel test 630 by first making a series of pitch runs with the model inverted and no image system for ten representative model configurations. These runs were then repeated with the image in place.

By taking the difference between corresponding runs the tare and interference effects of the single strut mounting system were isolated. These T&I effects were then used to correct the runs made with the model upright on the single strut.

6.3 OTHER CORRECTIONS

A flow alignment correction was obtained using the technique outlined in Reference 3, which involved one additional run upright with the image system. The lift data from this run were then compared with the lift data from the corresponding inverted image in run. When these two lift versus angle of attack curves are plotted together (with negative lifts plotted as if positive), the angle of attack variation between the curves is equal to twice the alignment error. The alignment error determined by this method was such that when the indicated angle of attack was zero degrees, the actual angle with respect to the airflow was one quarter degree.

Static weight tares were measured for each significant model change and applied during data reduction.

Following standard practice in the Vought tunnel as detailed in Reference 5, solid and wake blockage and compressibility corrections were combined into one expression, which was then multiplied by the desired test q to obtain a q setting. Thus when a test q of 75 psf was desired, the tunnel was operated at a q setting given by the equation, thereby eliminating the need for blockage and compressibility corrections during data reduction. The cross-sectional areas of the model and three-point mount are 1.78 ft² and 2.17 ft² respectively which produces approximately 6 percent blockage of the test section. The reduction in q setting which results from this blockage is approximately 3 percent.

6.4 TEST DYNAMIC PRESSURES

The majority of runs during the LSWI 630 test were made at the model design dynamic pressure of 75 psf although a few pitch runs were repeated at q = 100 psf. Yaw runs were made at q = 75 psf and 83 psf.

Pitch runs during the full-scale test were made at q = 62.5 psf rather than 75 psf as originally intended. Yaw runs were conducted at q = 16.2 psf due to structural limitations of the mounting system in yaw. However, it should be noted that this value of dynamic pressure corresponds to a velocity of 70 knots which is realistic for flight at high yaw angles.

Table I presents a comparison of Raynolds numbers for the two tests. There seems to be no generally accepted reference length for relicopters. Therefore, the table uses a unit value or Reynolds number per foot which is quite useful for comparison. Note that this value is expressed in model scale while the RN/ft of the Vought LSWI 630 data (shown in Appendix A) was given as an actual full-scale value. In addition, calculated Reynolds numbers are given for wing, horizontal stabilizer, fin, and mounting strut.

6.5 THREE-POINT MOUNTING SYSTEM TARE RUNS

Table II presents the final run schedule of the LSWI 630 test. Configuration designations are defined in the pictorial nomenclature presented in Figure 22. Table III is a comparison of configuration nomenclature used for the LSWI 630, LSWI 550, and full-scale tests. As shown in Table II the first ten runs were made using the three-point mount installed without the model. Runs 1 through 8 were made in yaw configuration although Run 8 was actually a pitch run. Small changes were made to the model during this series of runs in an effort to match drag levels with Run 1 of the full-scale test. Run 10 was made in the same configuration as Run 3 of the full-scale test. Run 6 supplied wind-on tare corrections in yaw, while Run 10 was used for wind-on tares in pitch for all runs with the model on the three-point mount.

6.6 SINGLE STRUT TARE AND INTERFERENCE RUNS

Next, the single strut mounting system was installed with the model inverted and a series of ten representative configurations were run, beginning with the complete helicopter and concluding with the basic fuselage. Following this series, the image system was installed and the same ten configurations were rerun. By taking the difference between corresponding runs of these two series, T&I corrections were derived for the remainder of the single strut runs. After the T&I runs the model was run upright with the image (Run 31). The data from this run and the previous inverted image—in run were combined to yield the flow alignment correction. Next, the image was removed and normal data runs began with a repeat of the ten representative configurations of the T&I series.

6.7 COMPARISON RUNS IN LAWY 550 CONFIGURATION

After these baseline runs the model was modified by the addition of transition strips and a series of seven runs (42 through 48) made with configurations identical to those of Runs 15 through 20 and Run 24 of the LSWT 550 test. The purpose of these runs was to determine the effects of modifications to the model since the LSWT 550 test.

6.8 COMPONENT BUILDUP ON SINGLE STRUT MOUNTING

Runs 49 through 73 represent a step-by-step process of adding or removing components one at a time to match representative configurations of the full-scale test for which comparisons were desired. The full-scale runs to be matched were Runs 14, 20, 21, 22, 30, 31, 68 and 69. The data from Runs 49 through 73 after correction for T&I and alignment would provide modelalone data to be subtracted from later runs on the three-point mount, yielding T&I corrections for that mounting system.

Two small configuration deviations were necessary. The run schedule called for the addition and removal of the exhaust ejector fairing (F_1) and the production tail rotor gearbox fairing (Y_p) . Since these items were modeled of clay, their addition and removal was rather time consuming. Therefore it was decided that after their removal, these two items would remain off and their effects added to or subtracted from the data as each configuration required.

6.9 COMPONENT BUILD-UP ON THREE-POINT MOUNTING

Runs 74 through 124 were made with the model mounted on the replica 40- by 80-foot three-point system. Runs 74 through 76 were made before it was discovered that the model was yawed 0.79 degree nose left. These runs were repeated after the error was corrected. Runs 77 through 107 are repeats of configurations tested on the single strut mount in the series from Runs 32 to 73.

Note that in order to measure the angular deflection of the entire three-point mounting system, the angle of attack readout module (nicknamed the " α bubble") remained installed in the model. By comparing the actual angle of the model, measured by the α bubble, with the indicated angle from the wind tunnel balance the amount of pitch error due to system deflection under airload was determined. The maximum errors were limited to one-quarter of a degree. After verifying that the deflection of the system was very small, the α bubble was removed. Pitch and yaw runs before and after the removal of the bubble (on Run 95) were made to evaluate the effect of external wires associated with control and α readout devices. The effect of the wires proved negligible.

6.10 EVALUATION OF ROUGHNESS AND PROTUBERANCES

Beginning with Run 108 an effort was made to match drag levels of the full-scale test through "tuning" the model by using grit strips as noted in the configuration nomenclature. While grit is normally applied to wind tunnel models for the purpose of assuring transition to realistically turbulent boundary layers, the intent here was also to simulate the characteristically rough surface, as well as multiple joints, cracks, and small protuberances of a prototype helicopter. Run 123 was intended to measure the effect of the more significant protuberances on the prototype aircraft.

6.11 DATA REDUCTION

Six component force and moment data (lift, drag, pitching moment, side force, rolling moment, and yawing moment) were recorded from the external balance during each run in units of pounds and foot pounds. Data reduction was accomplished using Vought computer programs.

In the case of the LSWI 630 test, all the basic force and moment data were divided by the test dynamic pressure, then transferred from balance resolving center to trunnion to model moment reference center, converted to full-scale values and finally corrected for static tares. Blockage and compressibility corrections are automatically applied in the setting of the tunnel q as discussed earlier. Wind axis data in this form (i.e. before tare and interference corrections) for all LSWT 630 runs are presented in Part l of Appendix A. Three other sets of data were also supplied by Vought. The first was data for the single support runs corrected for T&I. This could be referred to as "model-alone" data. Second was three-point mounting data with wind-on tares removed, and finally, there was a set of three-point mounting data with the appropriate single strut "model alone" data removed. Wind axis data from these three sets are presented in Parts 2, 3, and 4 of Appendix

7. PRESENTATION AND DISCUSSION OF TEST DATA

This section, including Figures 23 through 72, presents selected data from the LSWI 630 test. These data are representative of trends in the data taken during the test, and are discussed in five related groups.

7.1 COMPARISON OF FIFTH-SCALE RESULTS

Figures 23 through Figure 31 present comparisons between the original fifth-scale wind tunnel test (LSWI 550) and the LSWI 630 test. These figures show the effect of modifications that were made to the fifth-scale model. Lift characteristics appear to have changed only slightly for the complete helicopter, while the basic fuselage shows a positive lift increment ranging from almost zero at positive alphas to approximately 2.0 ft² at negative alphas. Drag is as much as 1.0 ft² less in the LSWI 630 test with the basic fuselage data again showing the greater difference. Pitching moment data showed good agreement at positive angles of attack, while negative angles showed considerable divergence, particularly in the case of the complete helicopter. In addition to differences in the model contours between tests, some of the disagreement may also be due to an improvement in the technique of sealing around the clearance hole where the mounting strut enters the fuselage. This later explanation is quite plausible in the case of drag which is lower in the LSWT 630 test reflecting a better job of sealing. The apparent cause of the large increase in pitching moment discrepancy for the complete helicopter is the difference in stalling characteristics of the horizontal stabilizer, possibly due to a change in the slat configuration between the two tests.

Figures 29 through 31 show that comparisons between the two fifth-scale tests for side force and yawing moment versus yaw angle of the complete helicopter are better than that of longitudinal data. Drag versus yaw angle is approximately 1.0 ft lower.

7.2 COMPARISON OF WIND-ON TARES

Figures 32 through 37 compare fifth-scale versus full-scale wind-on tares for the three-point mounting system in pitch and yaw with the dummy strut (as described in Section 5.2) in place.

Figures 32 through 34 show lift, drag, and pitching moment characteristics versus angle of attack. Lift is seen to be less than the full-scale value and drag is as much as 0.5 ft² greater. The direction of these differences is expected considering the disparity in Reynolds number (Table I). Pitching moment compares surprisingly well at positive angles of attack.

The reason for the difference at negative angles may be related to a moment shift in the full-scale data of approximately 4 ft³ at zero angle of attack.

Figures 35 through 37 show side force, drag, and yawing moment characteristics versus yaw angle. Side force differs by a considerable amount particularly at negative and smaller positive yaw angles. The full-scale data in this case appear questionable because the side force is non-zero at zero yaw angle. Similar comments apply to the yawing moment characteristics. Drag data compare exceptionally well throughout the yaw angle range. This excellent correspondence in drag prompts the thought that the reason for the discrepancies in side force and yawing could be that those quantities were too small, relative to the full-scale balance system's limits, to be accurately measured.

7.3 COMPARISON OF FIFTH-SCALE AND FULL-SCALE DATA ON THREE-POINT SYSTEM

Figures 38 through 58 compare data from the full-scale test with LSWT 630 data for which the model was mounted on the replica three-point system. These data have been corrected by subtracting the wind-on tares of the mounting system alone from the raw data. The configurations selected for comparison were those in which the fifth-scale model could be made to closely match the full-scale aircraft tested. Some of the configurations selected were identical to full-scale. Those which compare with full-scale runs 14, 20, 21, and 22 differ in that the open screens of the prototype could not be duplicated.

Figures 38 through 40 compare lift, drag, and pitching moment versus angle of attack for the basic fuselage. The lift curve slope of the fifth-scale data is greater than that of the full-scale data and the angle of zero lift is displaced 6 degrees. Drag shows better agreement with the maximum difference on the order of 0.6 ft² at negative angles and closer agreement at positive angles. The angle for minimum drag and general shape of the curve are also close. Pitching moment curves agree quite well in the mid-angle range. Note that for Run 109, grit was added to the fuselage at several locations in an effort to increase drag by simulating the roughness of the prototype airframe. This roughness produced a small increment in drag with little or no apparent change in lift or pitching moment characteristics.

Figures 41 through 43 show lift, drag, and pitching moment comparisons for the basic fuselage with wings added. In general the agreement between the two tests in terms of slopes and shape of the curves is good. However, the effort to adjust the drag level by simulating the roughness of the wing walk with various grit sizes produced some rather large magnitude changes

in lift and drag. These drag level adjustments produced agreement within 0.5 ft², although the additional roughness significantly decreased lift. Because of the wings' location, these adjustments had little effect on pitching moment correlation which remained good. In addition, it should be noted that the full-scale data show what is apparently wing stall while all the fifth-scale data are stall free.

Figures 44 through 46 compare lift, drag, and pitching moment versus angle of attack for the complete helicopter minus the wing. Lift differs very slightly in slope and by about 2 degrees in zero lift angle. The fifth-scale lift diverges rapidly at negative angle indicating stall of the horizontal surface. The drag curve shows very good agreement in both shape and angle for minimum drag. Pitching moment slope agrees well, but the angle for zero moment is shifted approximately 1 degree and data at larger negative angles exhibit the same divergence noted in lift. Runs 99 and 100 were made at q = 75 psf and q =100 psf respectively before the addition of any grit. Runs 120 and 121 were repeats of Runs 99 and 100 after grit had been added. The change in Reynolds number has a noticeable effect in the previously noted stall behavior at negative angles for lift and pitching moment in the smooth condition and very little effect after grit was added. Drag in the smooth condition increases with increased Reynolds number, indicating that a laminar boundary layer existing on the smooth fifth-scale model transitioned to turbulent flow with increasing Reynolds Number producing higher drag. The improvements in lift and pitching moment indicate a reduction in separation which is consistent with a turbulent boundary layer. With the model in the roughened state of Runs 120 and 121 the drag would be higher and change little with Reynolds number.

Figures 47 through 49 compare lift, drag, and pitching moment versus angle of attack for the complete helicopter. Two fullscale runs are plotted. Runs 20 and 21 differ only in that the main rotor hub was rotating in Run 20 and locked at a 60° azimuth in Run 21. Bell Helicopter experience with rotating hubs has shown that a hub locked at 60 degrees exhibits approximately the same aerodynamic characteristics; as is shown by Figures 47 through 49. Lift characteristics of the smooth model agree rather well except for the apparent wing stall behavior at positive alpha in the full-scale data. Runs 122 and 123 with the roughened model and added protuberances differ in angle of zero lift. The drag data show good agreement in the shape of the curve and angle for minimum drag. The drag values of the roughened model are 0.2 ft² to 0.8 ft² lower than full-scale. Pitching moment data show very little correlation except in the shape of the curves at nominal angles of attack.

Figures 50 through 52 show side force, drag, and yawing moment versus yaw angle. In the case of yaw data the Reynolds number of the fifth-scale data is only different by a factor of 2, due to the lower test q used for full-scale yaw runs (see Table I). Therefore the yaw data show better agreement than the pitch data. The side force compares well. The smooth model drag data of Runs 96 and 106 compare almost perfectly with full-scale. The roughened model has somewhat higher drag at small positive yaw angles. Yaw moment data show very good agreement in the slope and shape of the curves which all exhibit the characteristic unstable region or "flat spot" around zero yaw also noted during flight testing. Yawing moment data for the roughened model exhibit a divergence at large yaw angles.

Figures 53 through 55 show lift, drag, and pitching moments in pitch for the complete helicopter minus the tail rotor hub and mast. This configuration is virtually identical to the smooth model configuration of Figures 47 through 49 and, as might be expected, exhibits very similar characteristics.

Figures 56 through 58 show lift, drag, and pitching moment characteristics for the complete helicopter with the landing gear doors open. The smooth model lift data agree well with full-scale, while the roughened model has less lift throughout the alpha range. Drag data for the smooth model are approximately 1.0 ft² less than full-scale. The roughened model data match full-scale drag almost perfectly for $\alpha = 0^{\circ}$ to $\alpha = 6^{\circ}$ with some divergence occurring at negative angles. Pitching moment correlation is poor except that the shape of the roughened model data matches full-scale.

7.4 TARE AND INTERFERENCE OF THE THREE-POINT SYSTEM

Figures 59 through 64 illustrate the magnitude of tare and interference effects measured during LSWT 630 for the three-point mounting system. Figures 59 through 61 show lift, drag, and pitching moment versus angle of attack, while Figures 62 through 64 show side force, drag, and yawing moment versus yaw angle. In Figures 59 through 61 four sets of data are shown. First are the wind-on tares measured without the model from Run 10. The remaining curves of each figure are obtained by subtracting model-alone data measured on the single strut from the raw data for the same configuration measured on the three-point mounting. This yields a tare and interference correction for the three-point system which may be compared with the wind-on tare. The three configurations treated in this fashion are the basic fuselage, basic fuselage plus wing, and complete helicopter.

The comparison shows some very striking differences between the wind-on tare curves and the measured T&I curves, implying that

interference effects in the full-scale test data were not negligible. In the case of lift corrections the wind-on tare is almost a constant 1.0 ft² while the T&I with the basic fuselage is zero at $\alpha=0^{\circ}$, but has a considerable negative slope. With the addition of the wing the T&I curve shifts upward approximately 2.0 ft² while the negative slope steepens slightly. The curve then shifts downward and steepens for the complete helicopter configuration. T&I corrections for drag are roughly twice the basic wind-on tare values. Most of the difference appears to be due to the fuselage with smaller increments of interference added by the wing and the remainder of the items which make up the complete helicopter configuration. The T&I corrections for pitching moment, unlike those for lift and drag, are much less than the wind-on tares.

Figures 62 through 64 compare wind-on tares and derived T&I corrections for side-force, drag, and yawing moment versus yaw angle. Side force T&I corrections are approximately equal to the wind-on tare values at zero yaw but the variation with yaw is four to five times steeper. The T&I corrections to drag are approximately 60 percent greater than the wind-on tare values, but the variation with yaw angle is almost identical. Yawing moment T&I's, like those for side force, have a much greater variation with yaw and exhibit stall-like behavior at larger angles.

7.5 COMPARISON OF FIFTH-SCALE AND FULL-SCALE COMPONENTS ON THREE-POINT SYSTEM

Figures 65 through 72 compare fifth-scale and full-scale lift, drag, and pitching moment versus angle of attack for the wing, horizontal stabilizer, slat, and end plates. The LSWT runs used for these comparisons were all made with the model mounted on the three-point mounting system.

Figures 65 through 67 compare the lift, drag, and pitching moment characteristics of the wing-alone obtained by taking the difference between runs with and without the wing. The smooth wing data from LSWT 630 have approximately the same slope as the full-scale data, while the angle of zero lift varies by 2 degrees. The full-scale data show a stall, however, which is not evident in any of the fifth-scale wing data. Correlation is poor for the roughened wing in lift. In drag, however, the roughened wing compares very well while the drag of the smooth wing is too low. Pitching moment data are quite scattered for both full-scale and fifth-scale wings. Pitching moment slopes in fifth-scale are lower than full-scale values and there is very little agreement in any of the data.

Figures 68 through 70 compare the full-scale and fifth-scale aerodynamic characteristics of the horizontal stabilizer in

pitch. Foth lift and pitching moment show very little correlation is slope or zero angle. Drag compares very well except at the larger legative angles.

Figure 71 compares the effect of the slat on aerodynamic characteristics in pitch. Generally, the agreement between full-scale and fifth-scale is good, particularly in the case of drag. There is some divergence at the larger negative angles except in the pitching moment data. While the pitching moment data from the full-scale test shows considerable scatter there is good agreement with fifth-scale particularly in the shape of the curve.

Figure 72 compares the effect of the endplates on aerodynamic characteristics in pitch. Lift, drag, and pitching moment data agree extremely well throughout the range of angle of attack. It should be noted that, because the endplates are vertical surfaces, the data presented in Figure 70 should be considered as endplate effect on the lift, drag, and pitching moment of the horizontal surface. The primary effect of the endplates would be seen as variations in side force, drag, and yawing moment with yaw angle.

8. CONCLUSIONS AND RECOMMENDATIONS

This section discusses the conclusions which were drawn from the data obtained during the fifth-scale testing of the modified Model 222 wind tunnel model and the comparison of that data with full-scale and earlier fifth-scale data. Figures 73 through 81 present these summary comparisons and illustrate the improvements in correlation obtained from testing on the replica three-point mount.

8.1 CONCLUSIONS

The primary cause of the lack of agreement between the fifthscale data of LSWT 550 and the full-scale data of the Ames test was the effect of interference related to the three-point mounting system used for the full-scale test. The effect of the mounting system was most obvious in the drag data comparisons but was also noticeable in lift and pitching moment data.

When the tare and interference effects measured during this test are applied to the full-scale test data, the drag is seen to be substantially lower than originally believed. The prototype drag value at $\alpha=0^\circ$ was reported as 13.5 ft² (from Run 20) after the full-scale test. If the wind-on tare of 2.84 ft² is added back in and then the fifth-scale tare and interference of 5.8 ft² is subtracted, the result is a corrected drag of 10.54 ft².

Several other conclusions are suggested by comparison of the LSWI 630 test data with the LSWI 550 and full-scale data.

Figures 23 through 31 show that the effects of contour differences were minimal. The differences seen in the data (primarily in lower drag for the LSWT 630 test), could be explained by either the cleaner cowling of the modified model or by an improvement in the sealing of the model in the area of the mounting strut.

Reynolds number effects were concluded to have been a relatively small factor in the lack of correlation, except at large angles of pitch and yaw. In these instances the fifth-scale data exhibit stall-like behavior which might be expected at lower Reynolds number. Runs which were made at dynamic pressures of 100 psf, as well as 75 psf, showed an improvement at the 15 percent higher Reynolds number.

Some of the disagreement between full-scale and fifth-scale drag data was due to the unrealistically smooth surface of the model. While the flow on the model was generally turbulent, it seemed necessary to further increase skin friction by the addition of grit to adequately simulate the rough surface of

the prototype. This roughening usually did not improve correlation in lift or pitching moment.

Correlation between full-scale and fifth-scale data for the wing, horizontal stabilizer, slat, and endplates was mixed as shown in Figures 65 through 72. The only obvious Reynolds number effect noted was a premature stall of the model horizontal stabilizer in the negative angle range as shown in Figure 66.

8.2 RECOMMENDATIONS

Based on the major conclusion of this investigation it is recommended that the determination of tare and interference corrections receive greater emphasis in full-scale wind tunnel testing. This greater emphasis is of particular importance when unconventional mounting systems are used. The technique employed in LSWT 630 to evaluate T&I corrections by testing a scale model of the aircraft on a scale model of the mounting system seems to be a promising alternative when full-scale T&I measurements are not feasible.

With regard to the use of small-scale testing to determine T&I corrections, some further recommendations are offered. As with any wind tunnel test, complete documentation of model contours, configurations, test conditions, and data reduction is crucial.

The small-scale test should follow the full-scale test so that all runs and configurations of the full-scale test are known and may be easily duplicated. This is particularly important in a typical development testing situation where unforeseen runs and configurations may be added during the full-scale test based on data from earlier runs. The disadvantage inherent in this testing sequence is that the corrected full-scale data are not available until the small-scale T&I's are measured. This problem could, however, be eased somewhat by running the tests concurrently.

An effort should be made to ensure that several representative full-scale configurations can be duplicated exactly for the tare and interference measurements. In addition to the expected faithfulness of contour, this would also include careful sealing of the full-scale model to eliminate any airflow or leakage which could not be duplicated in the small-scale model.

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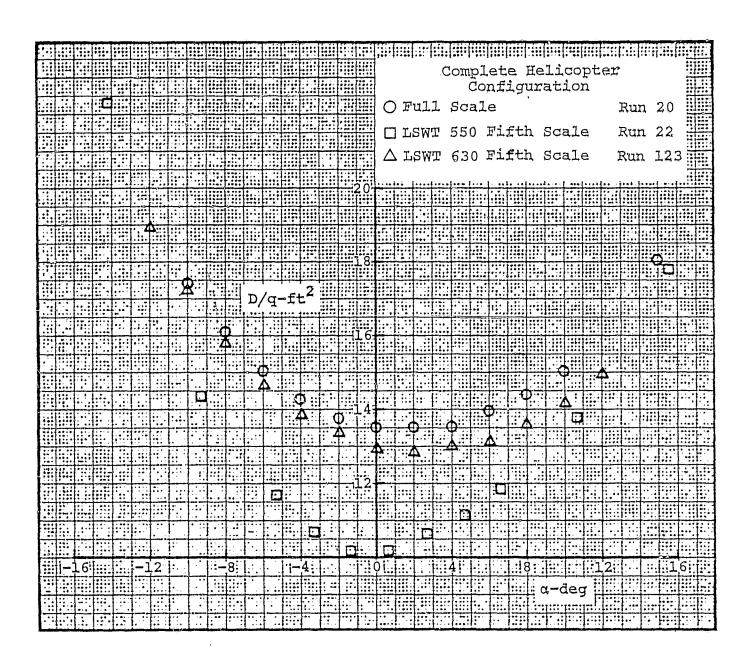
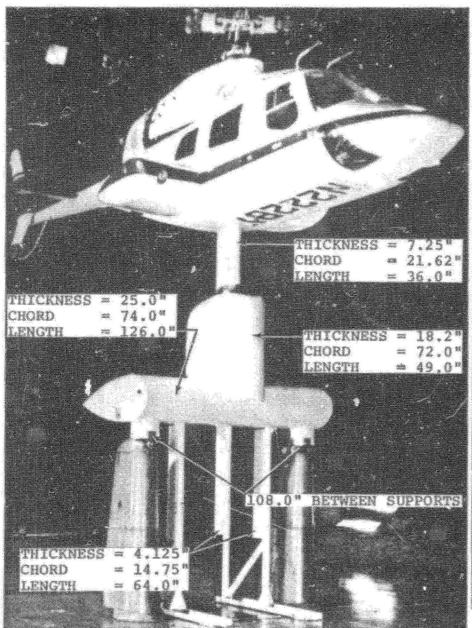


Figure 1. Correlation Improvement for Helicopter Drag Characteristics in Pitch

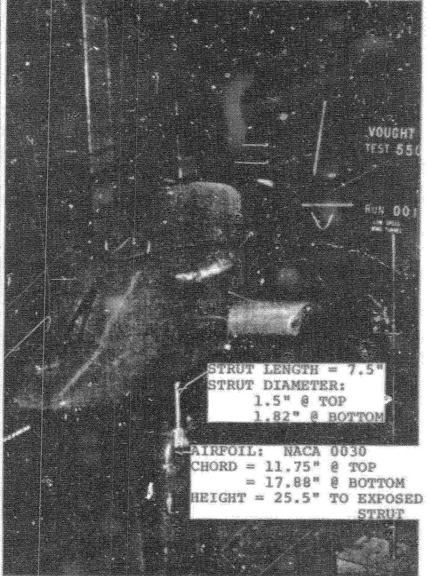
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Figure 2. Correlation Improvement for Helicopter Drag Characteristics in Yaw



M222 Prototype in NASA/Ames 40 by 80 Poot Wind Tunnel



Fifth Scale M222 Model in Vought Corp. 7 by 10 Foot Wind Tunnel

Figure 3. Comparison of Prototype and Fifth Scale Model.

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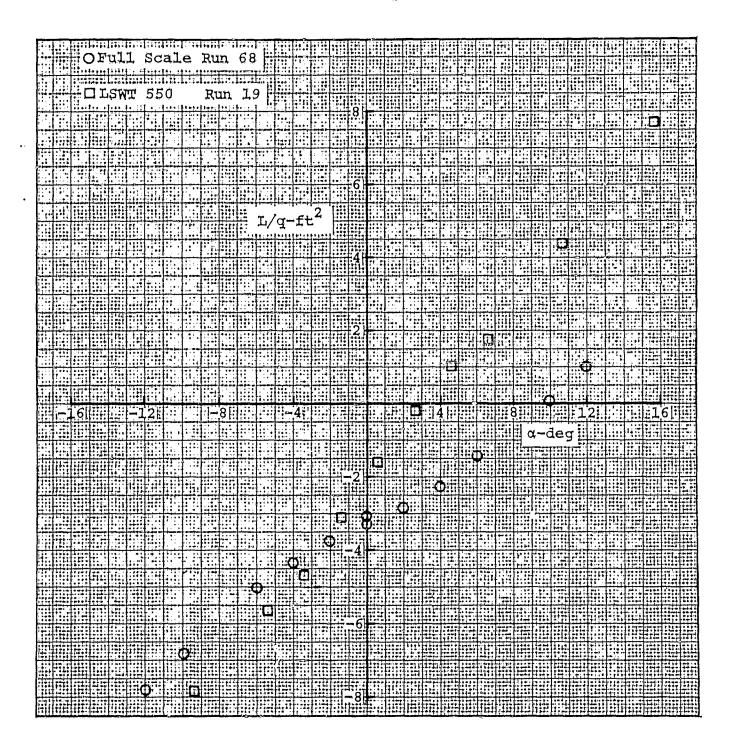


Figure 4. Original Comparison of Lift Characteristics in Pitch for Basic Fuselage

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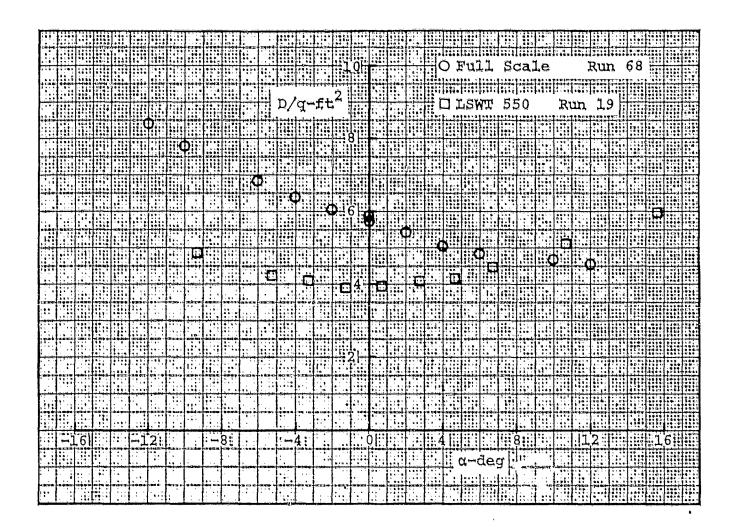


Figure 5. Original Comparison of Drag Characteristics in Pitch for Basic Fuselage

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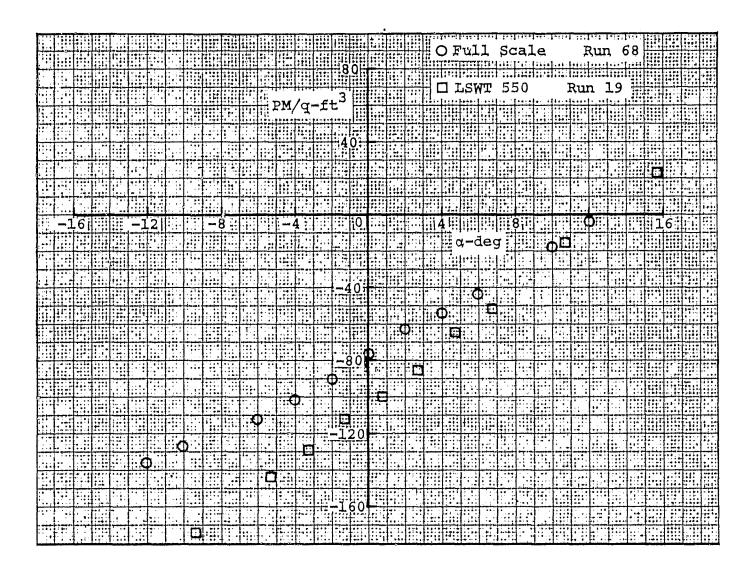
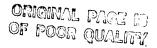


Figure 6. Original Comparison of Pitching Moment Characteristics in Pitch for Basic Fuselage



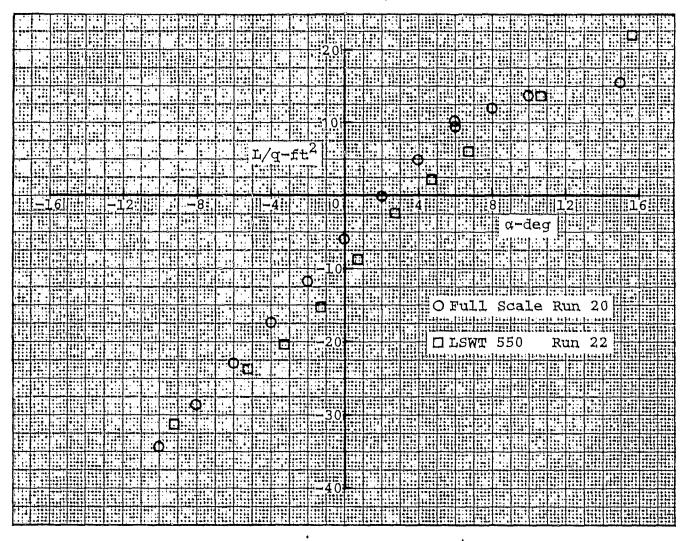


Figure 7. Original Comparison of Lift Characteristics in Pitch for Helicopter

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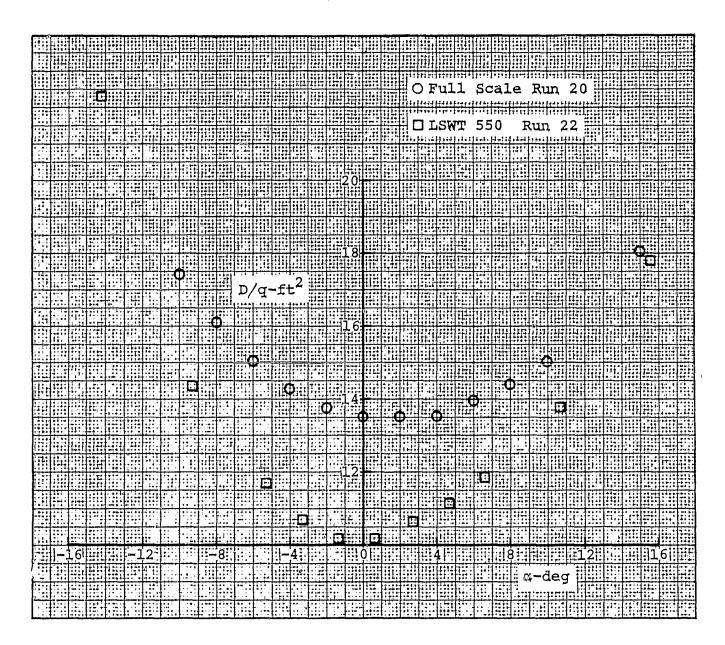


Figure 8. Original Comparison of Drag Characteristics in Pitch for Helicopter



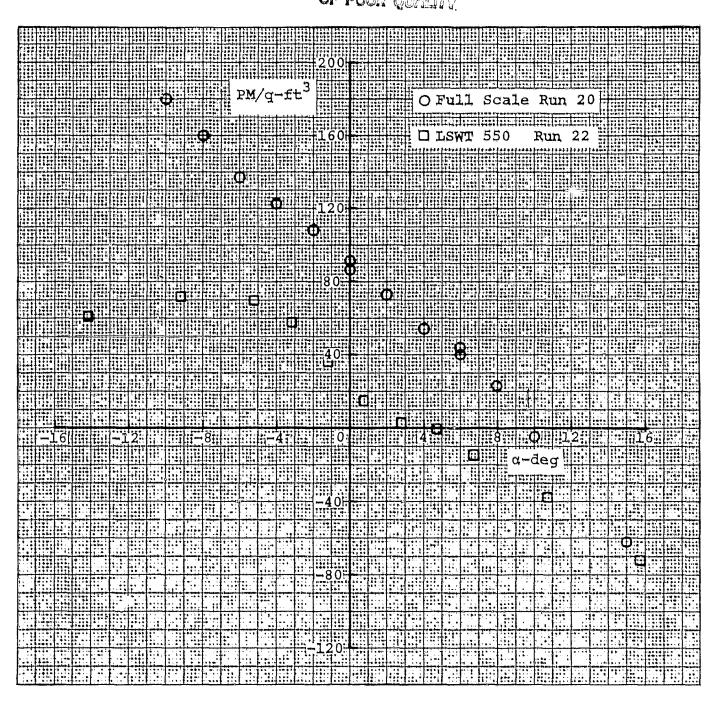


Figure 9. Original Comparison of Pitching Moment Characteristics in Pitch for Helicopter

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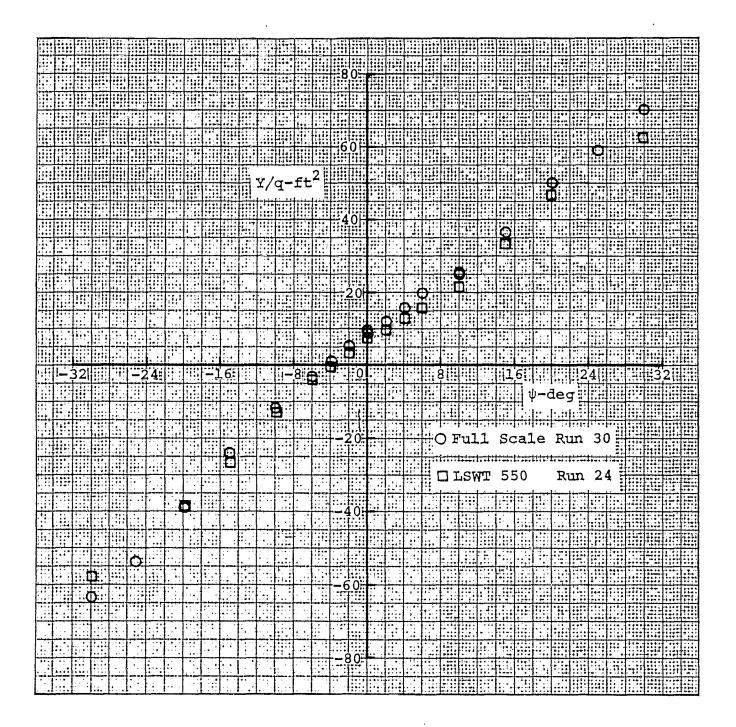


Figure 10. Original Comparison of Side Force Characteristics in Yaw for Helicopter

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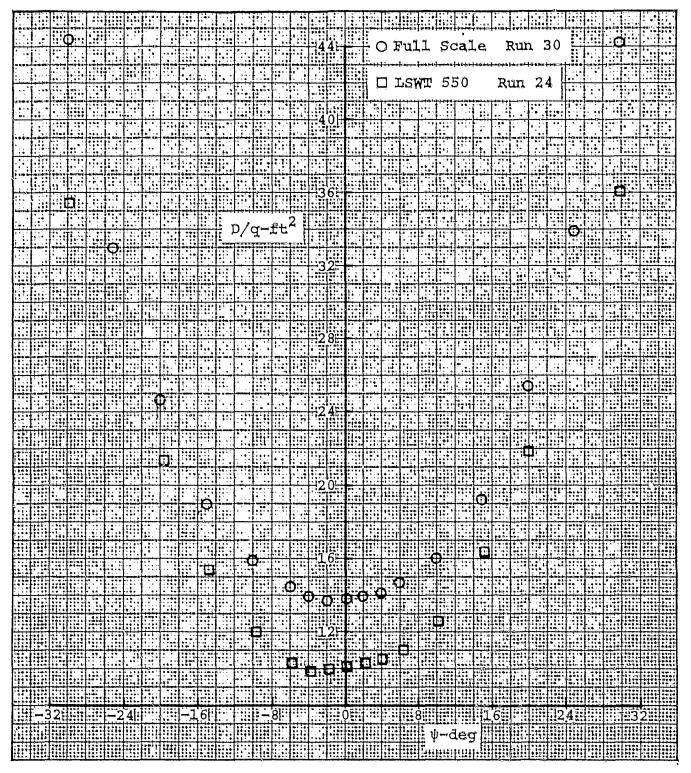


Figure 11. Original Comparison of Drag Characteristics in Yaw for Helicopter

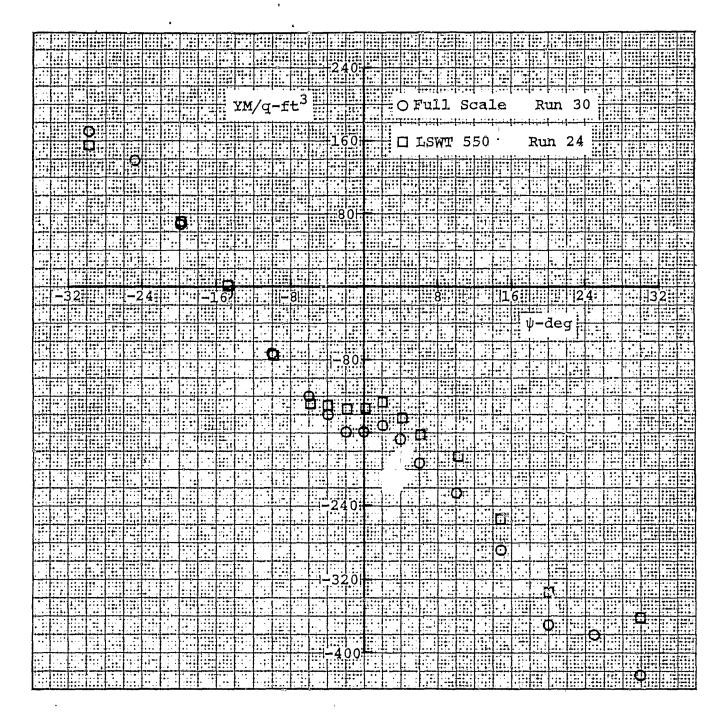


Figure 12. Original Comparison of Yawing Moment Characteristics in Yaw for Helicopter

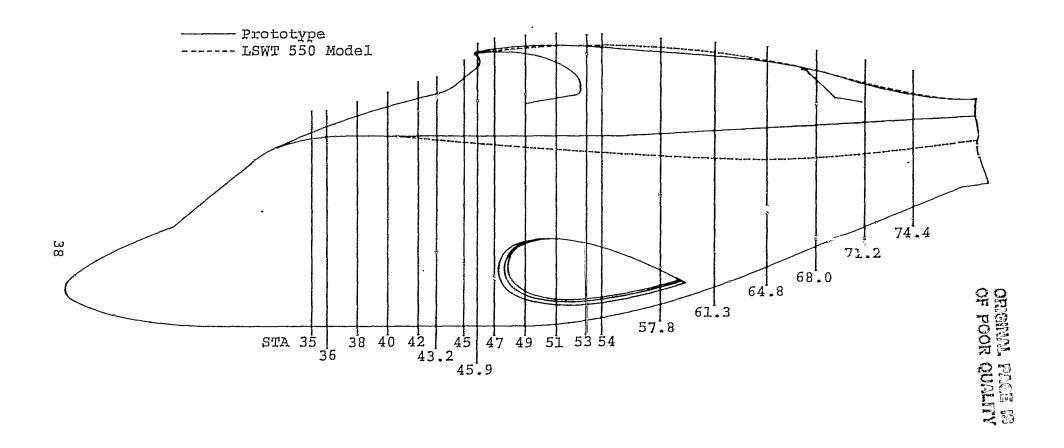


Figure 13: Contour Discrepancies of M222 Model (Sideview)

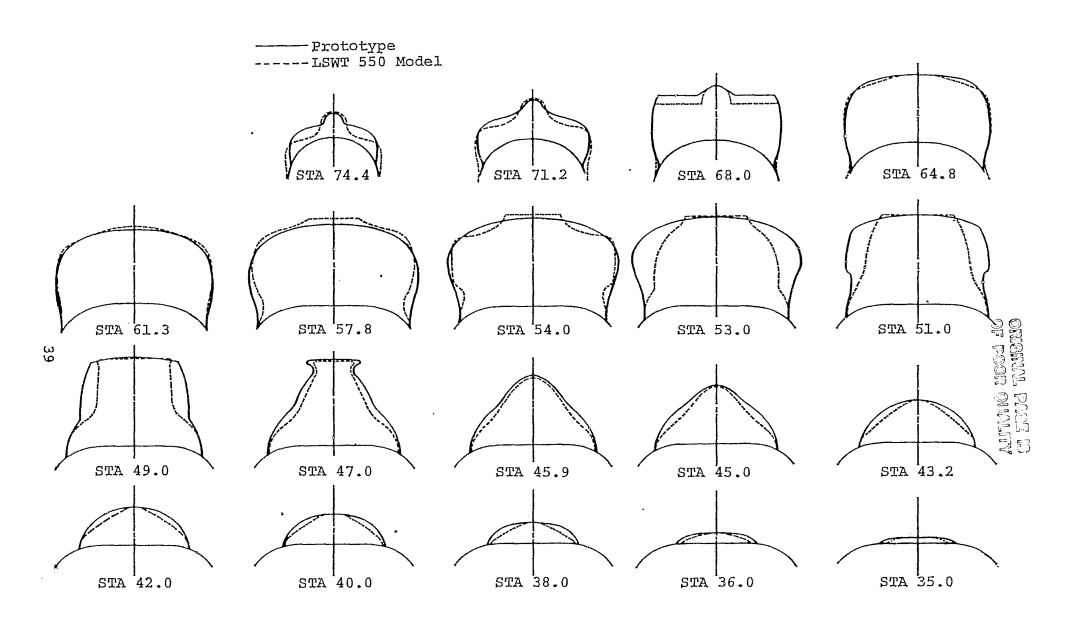


Figure 14. Contour Discrepancies of M222 Model Cowling

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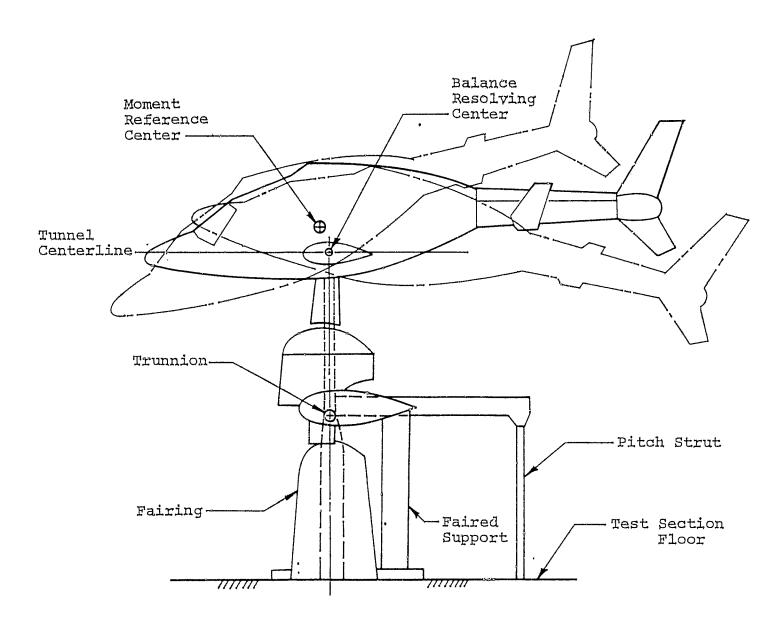


Figure 15. Schematic Drawing of 40 x 80 Mounting

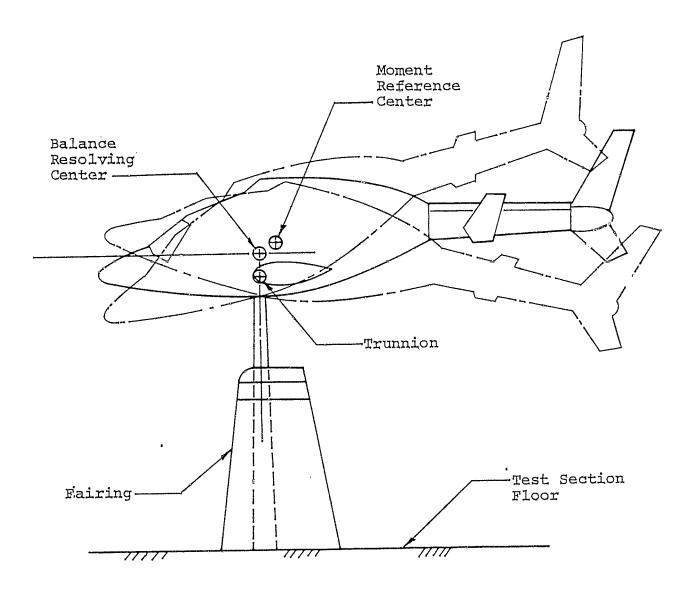
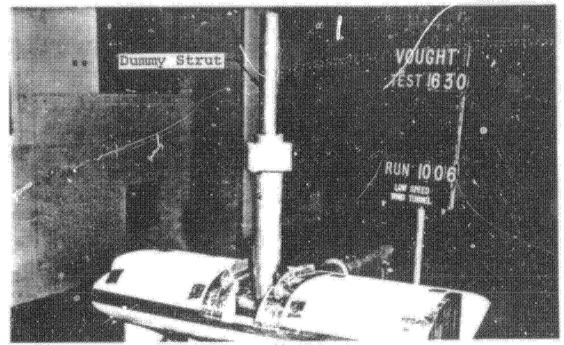
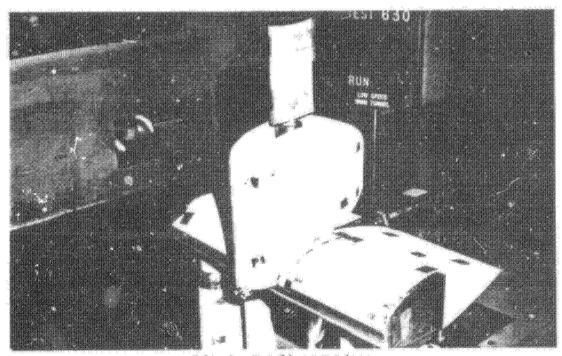


Figure 16. Schematic Drawing of Single Strut Mounting



Yaw Configuration



Pitch Configuration

Figure 17. Three-Point Support Configuration for Yaw and Pitch Run Testing.

Figure 18. Fifth Scale M222 Model Installed on Single Support.

Figure 19. Fifth Scale M222 Model Installed Inverted with Image System

Figure 20. Fifth Scale M222 Model on Three-Point Support (Pitch Run Configuration).

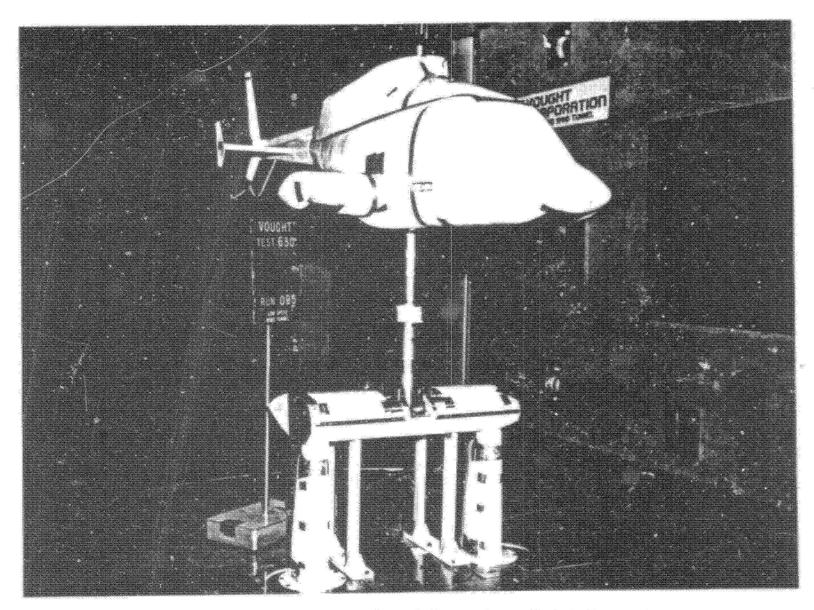
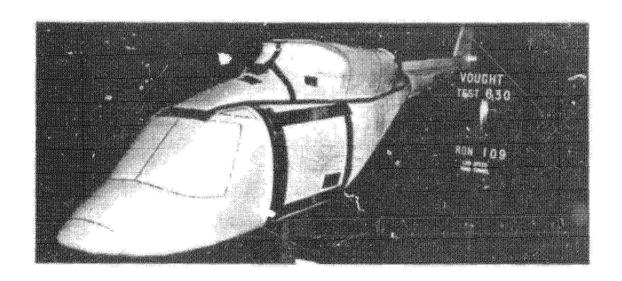


Figure 21. Fifth Scale M222 Model on Three-Point Support (Yaw Run Configuration)

B Smooth fuselage and tail rotor.



C Prototype cowling.

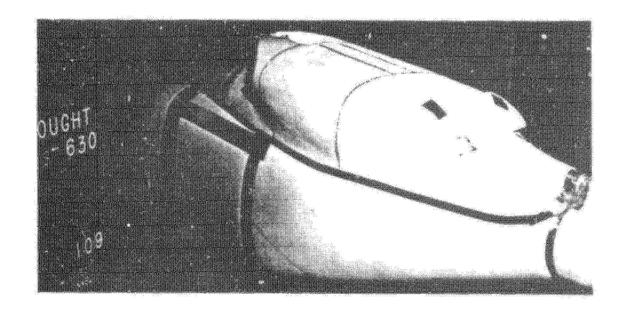
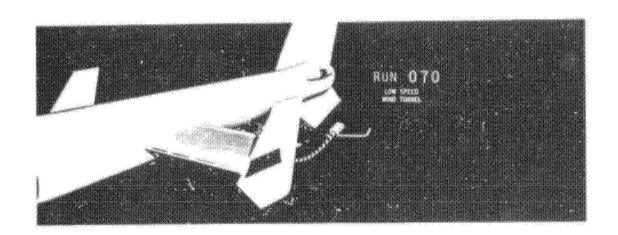


Figure 22. Pictorial Nomenclature.

Endplates on horizontal stabilizer. Endplates were canted 3° nose right.



E₁ Exhaust ejector fairing.

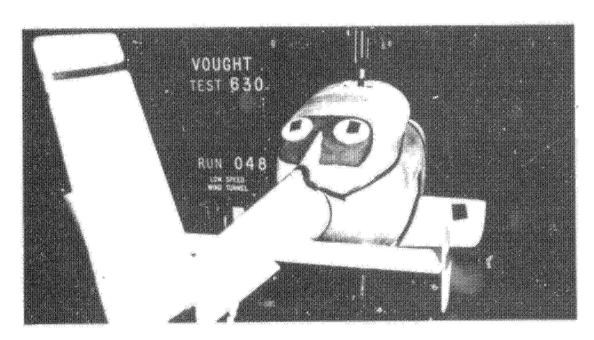
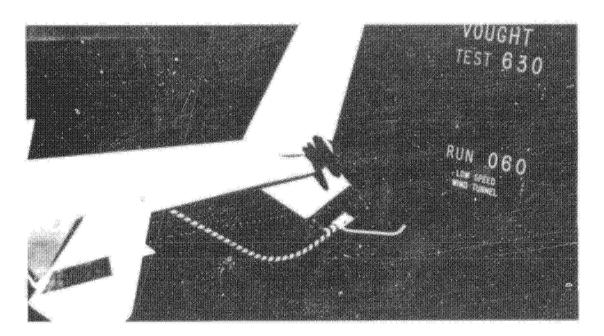


Figure 22. Continued.

G Tail rotor guard antenna.



 ${
m H}^+$ NACA 0015 horizontal stabilizer (with T.E. tab) set at -7° incidence. A (+) superscript indicates that a leading edge slat was installed on the stabilizer.

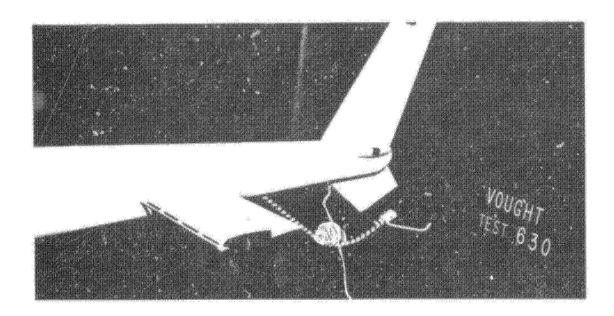
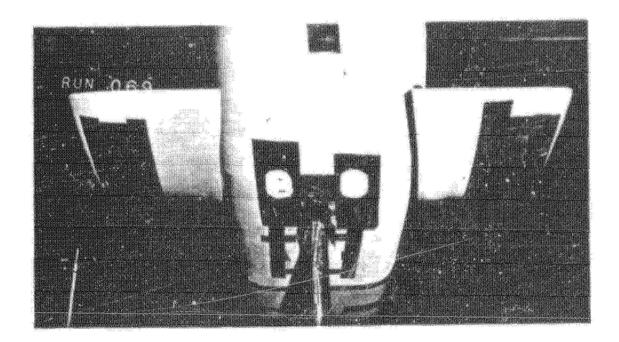


Figure 22. Continued.

M₁ Main landing gear retracted with doors closed.



M₂ Main landing gear retracted with no doors.

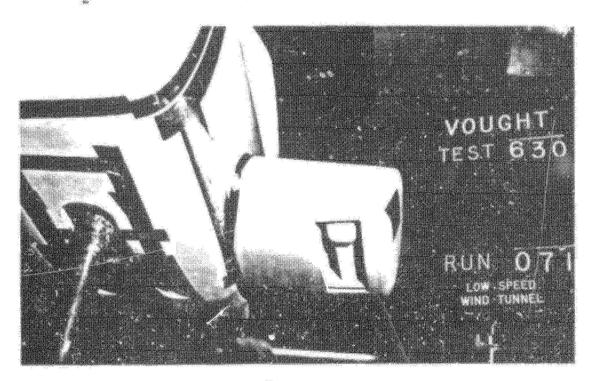
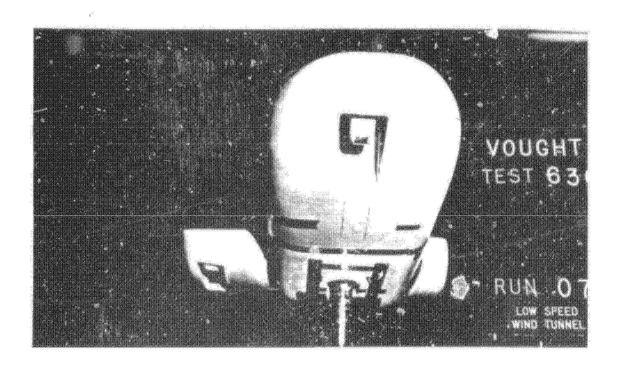


Figure 22. Continued.

N₁ Nose gear retracted with doors closed

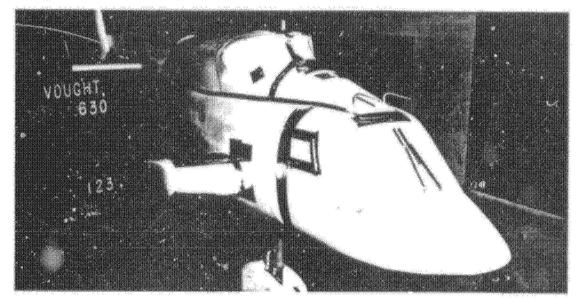


Nose gear retracted with no doors (shown)

O₄ All screens on cowling closed. See photograph of "C" configuration.

Figure 22. Continued.

Production protuberances: pitot tubes, windshield wipers and pilot's sliding window on L. H. side.



- P₃ Fuel sump recesses covered.
- P₄ Fuel sump recesses open.

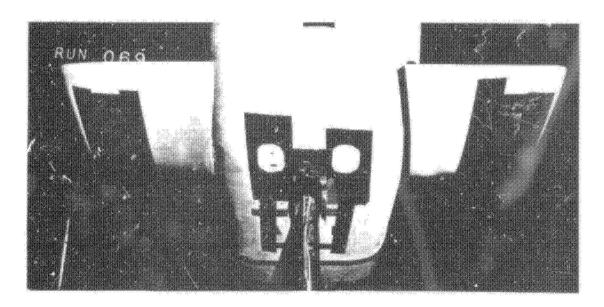
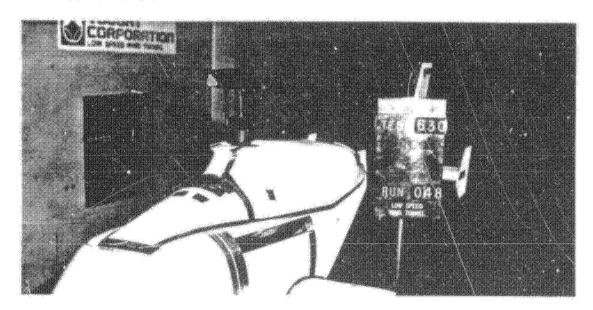


Figure 22. Continued.

- Q Plugged inlet and exhaust ejectors on prototype cowling. See photograph of "Q" configuration.
 - R_1^{60} Main rotor hub; mast controls set at 60° azimuth (fore and aft is 0°).



T Tail rotor hub, mast; controls set at 60° azimuth.

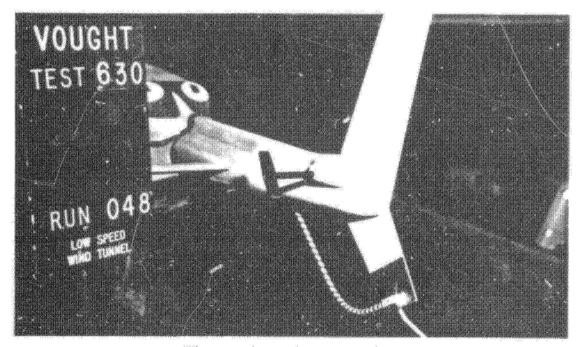
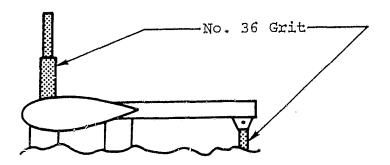


Figure 22. Continued.

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(TS) No. 36 carborundum grit on forward and rear struts of Ames type supports.



- (TS)₂ Transition strips of No. 50 carborundum grit applied in 0.125-inch wide bands to the model as follows:
 - a) nose
 - b) windshield outline
 - c) outline of engine inlets on cowl
 - d) (2) bands on cowl aft of inlets
 - e) top of cowl parallel to airstream
 - f) both sides of vertical fin 5% aft of L.E.

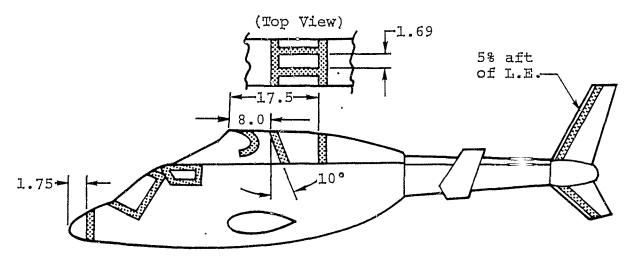
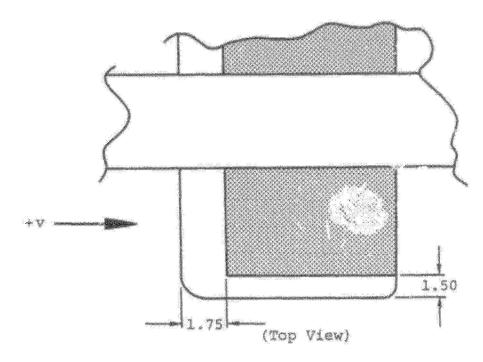


Figure 22. Continued.

 $(\mathrm{TS})_3$ $(\mathrm{TS})_2$ plus wing-walks made of No. 80 sandpaper on upper surface of both wings.



 ${\rm (TS)}_4$ ${\rm (TS)}_2$ plus wing-walks made of No. 180 sandpaper on upper surface of both wings as for ${\rm (TS)}_3$.

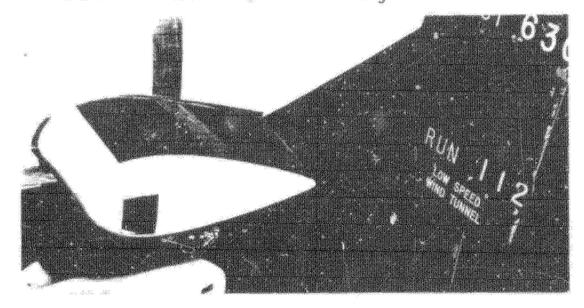


Figure 22. Continued.

- $(TS)_5$ Configuration $(TS)_4$ with addition of No. 50 carborundum grit on leading edge of endplates extending back approximately 0.20 inches from the leading edge.
- (TS)₆ Configuration ("S)₅ with 0.10-inch wide strip of No. 50 carborumdum gri. applied to lower surface of horizontal stabilizer 0.25 inches back from the leading edge.
- (TS) Configuration (TC) with grit removed from vertical fin.

V, Vertical fin with stinger and 15-inch cap (extends to W.L. 156).

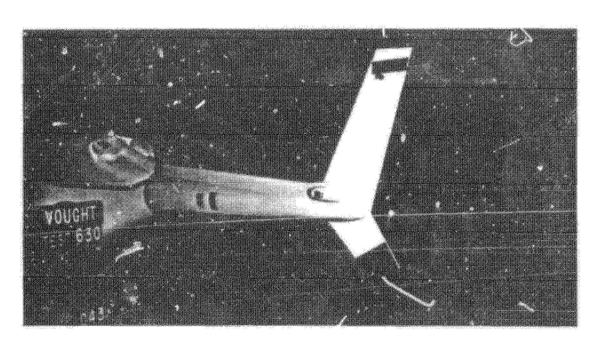
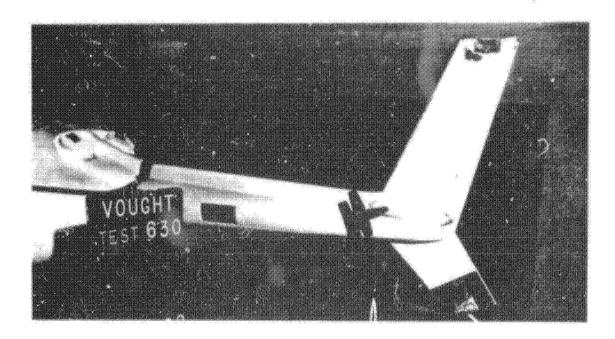


Figure 22. Continued.

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V₂ Vertical fin with stinger and 10-inch cap (extends to W.L. 151).



W₁ Prototype NACA 0035 wing with standard tip.

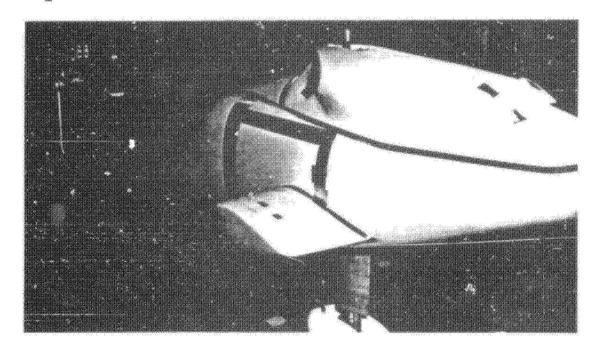
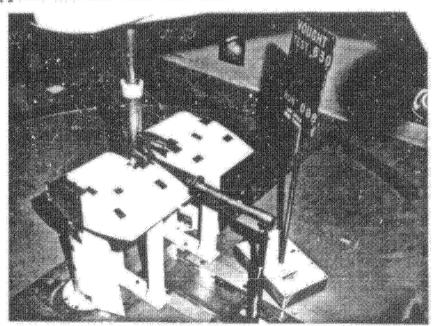


Figure 22. Continued.

 X_1^* Ames 40x80 type mount with no fairings on vertical support strut. Asterisk denotes that wiring which was taped to support struts was removed.



Ames 40x80 type mount with both fairings for vertical support strut. Asterisk denotes that external wiring for bubble package was removed.

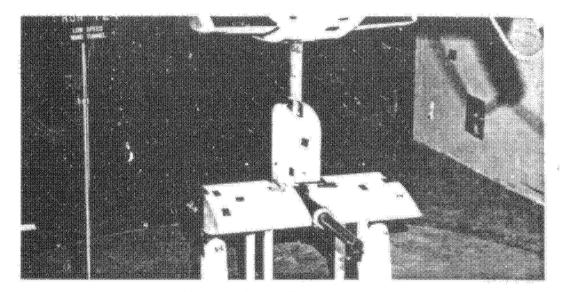
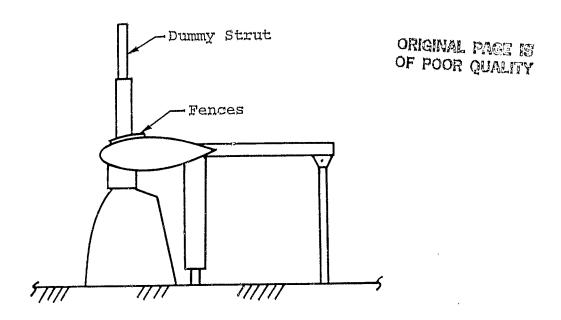


Figure 22. Continued.

Ames 40x80 type mount with dummy strut and no fairings. Fences mounted on horizontal fairing adjacent to support.



X₃ X₃ configuration, but with material removed from horizontal fairing as shown in sketch.

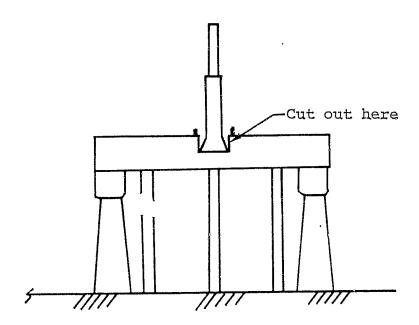
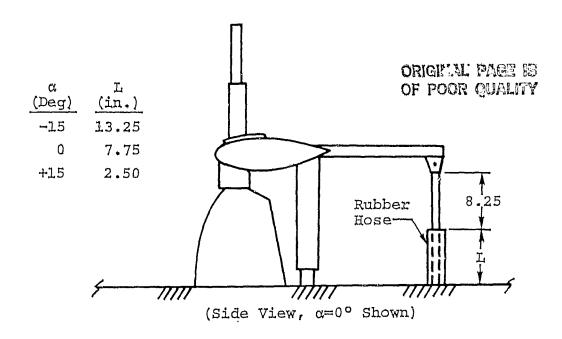


Figure 22. Continued.

 X_3^2 Configuration X_3^1 with rubber hose added to rear strut as shown to increase diameter.



 X_3^3 Configuration X_3^2 with simulated joint at base of dummy strut as shown. Joint was made from foam material.

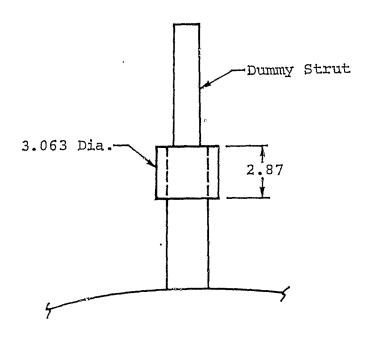
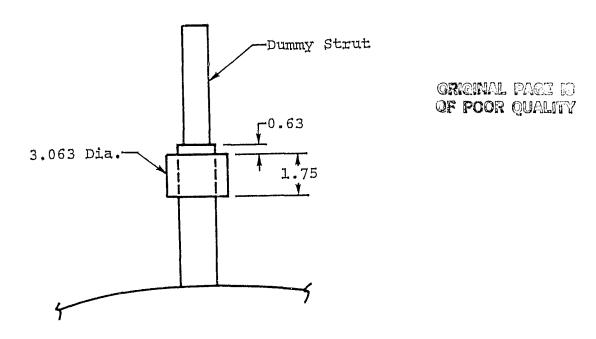


Figure 22. Continued.

 x_3^4 Joint of configuration x_3^3 modified as shown in sketch.



 X_{4} Configuration X_{3}^{4} with dummy strut removed and fences off.

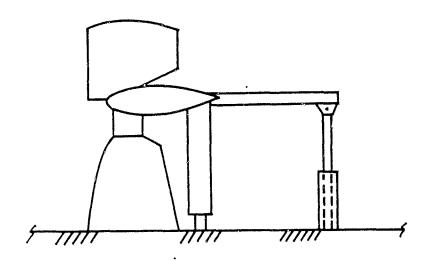
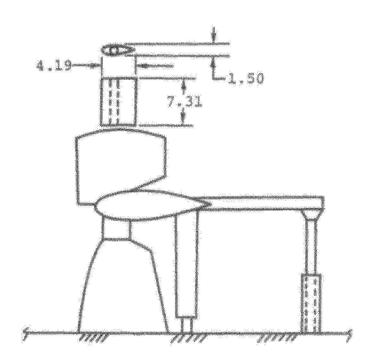


Figure 22. Continued.

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 X_5 X_4 configuration with dummy strut and small fairing as shown in sketch.



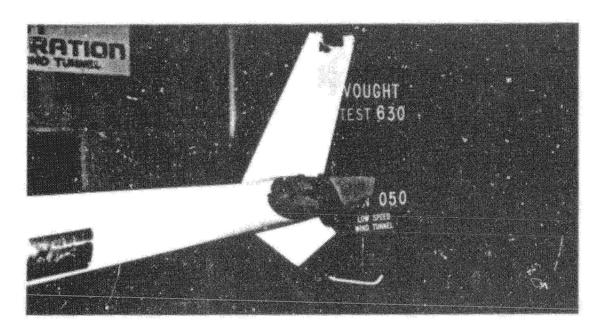
Y₁ Original prototype tail rotor gearbox fairing.



Figure 22. Continued.

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Yp Preliminary "production" tail rotor gearbox fairing.



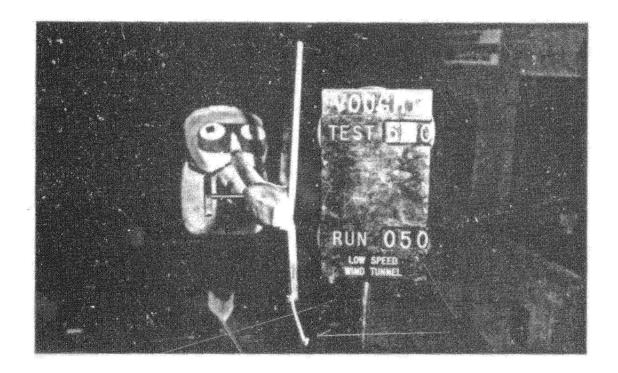


Figure 22. Concluded.

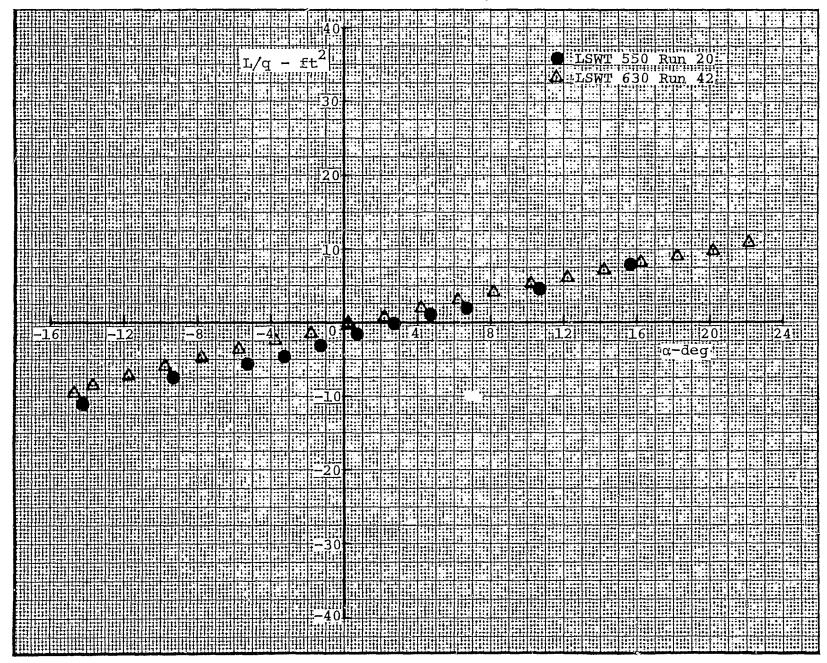
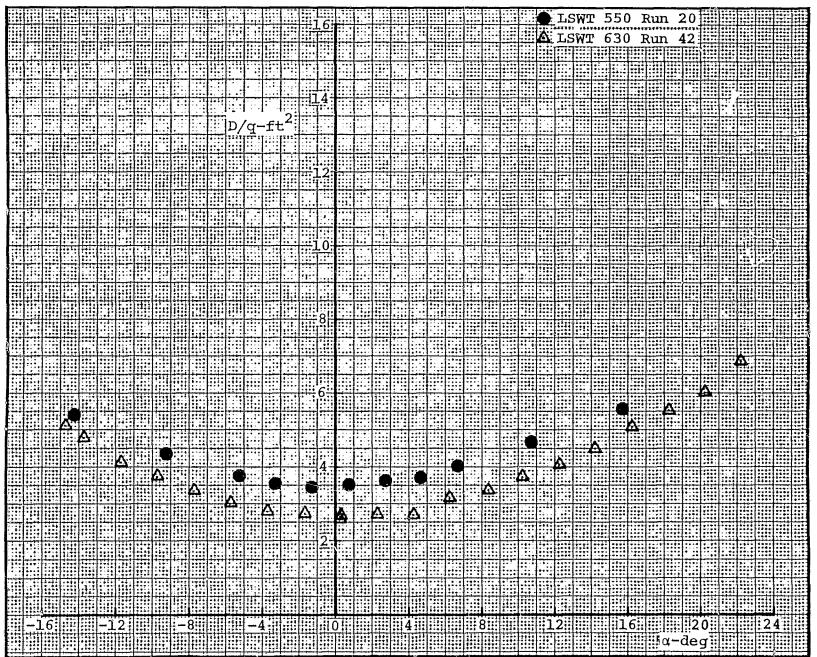


Figure 24. Comparison of Fifth-Scale Drag Characteristics in Pitch for Basic Fuselage



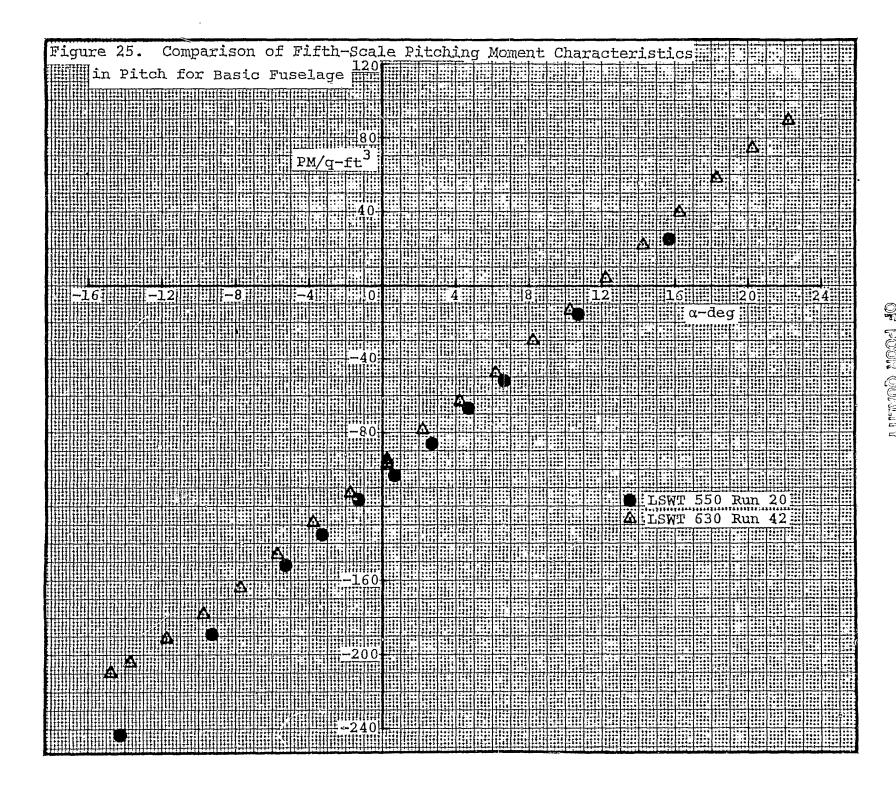
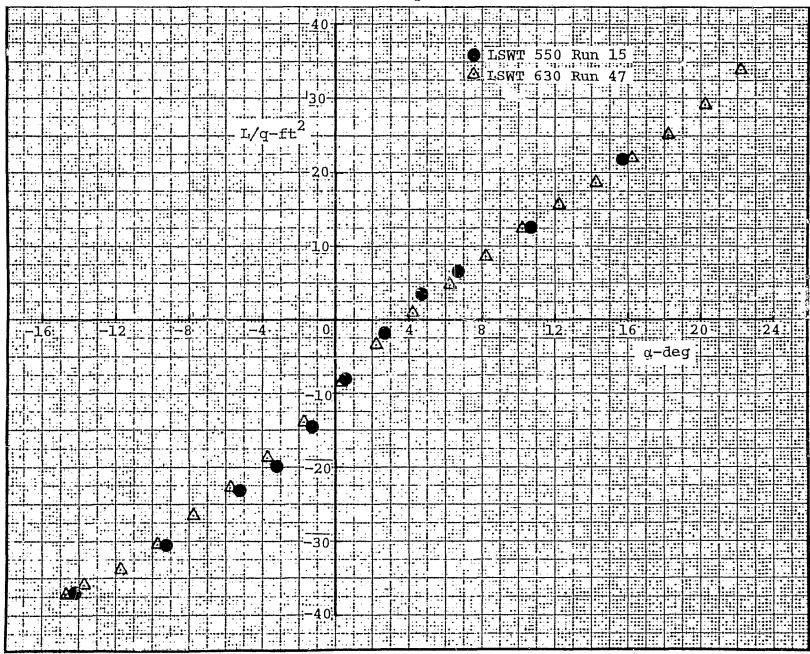
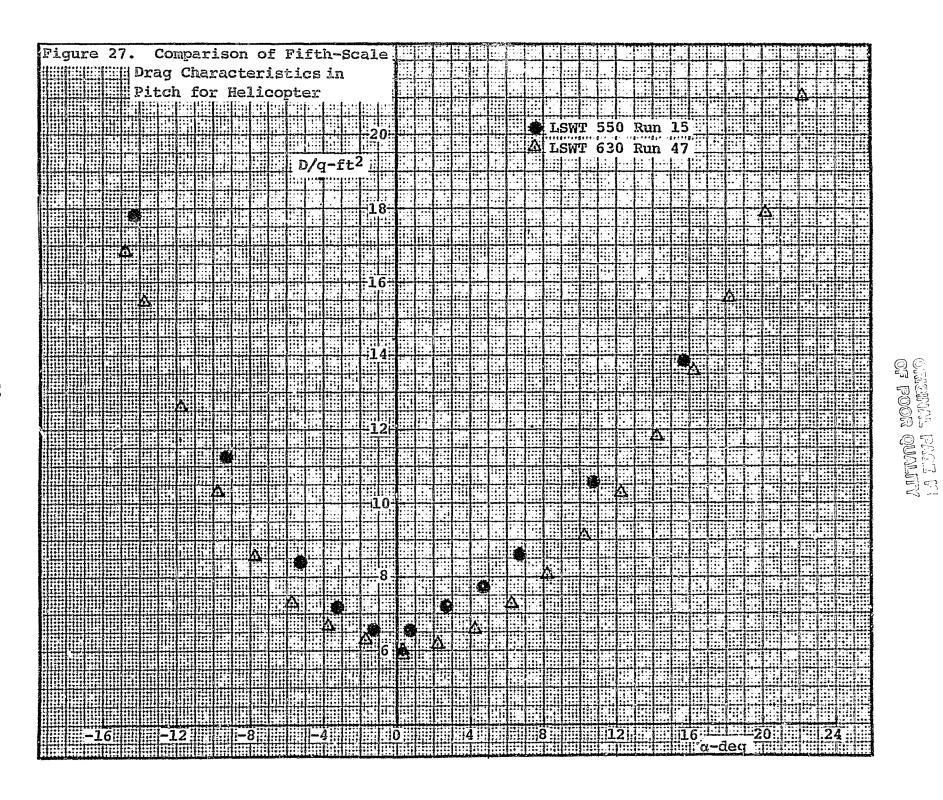


Figure 26. Comparison of Fifth-Scale Lift Characteristics in Pitch for Helicopter





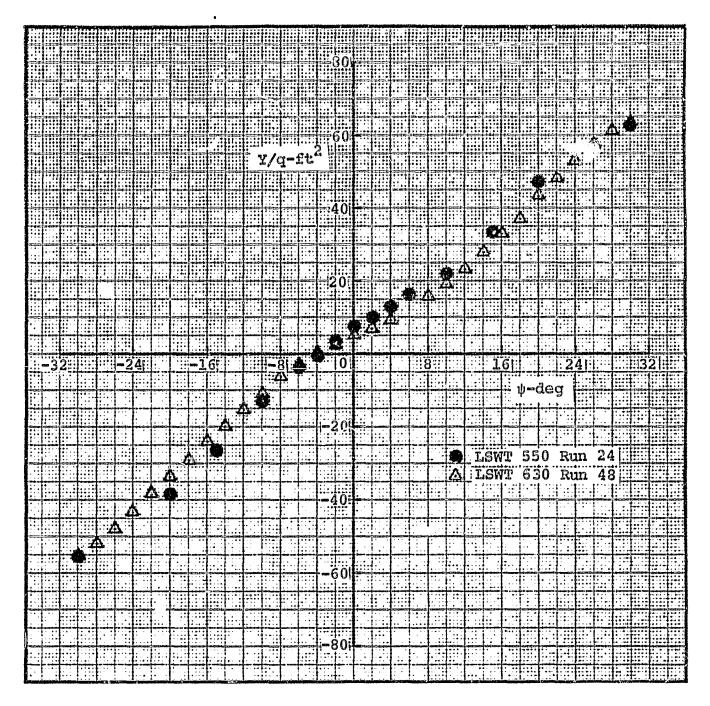


Figure 29. Comparison of Fifth-Scale Side Force Characteristics in Yaw for Helicopter

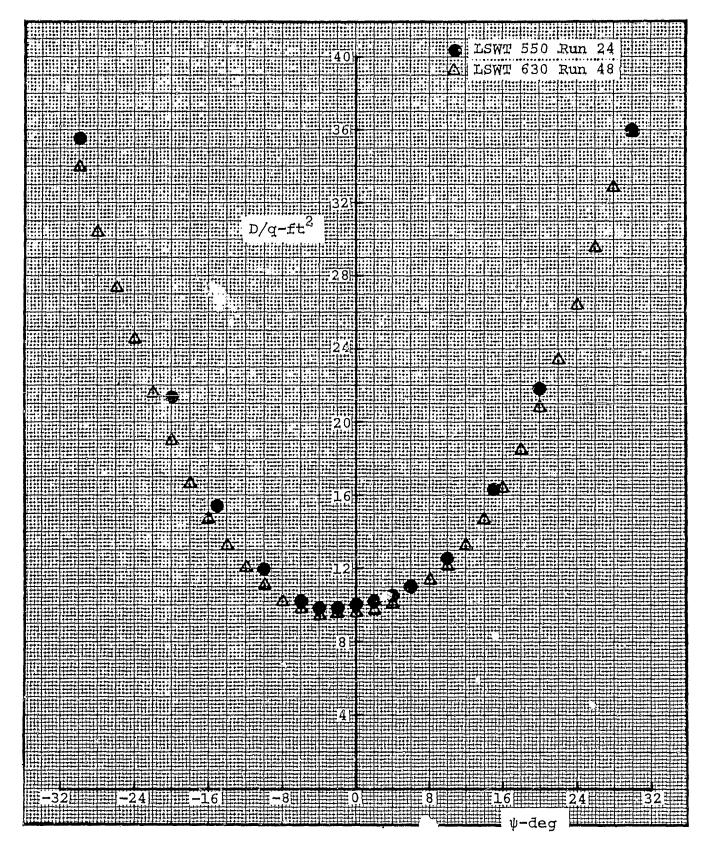


Figure 30. Comparison of Fifth-Scale Drag Characteristics in Yaw for Helicopter



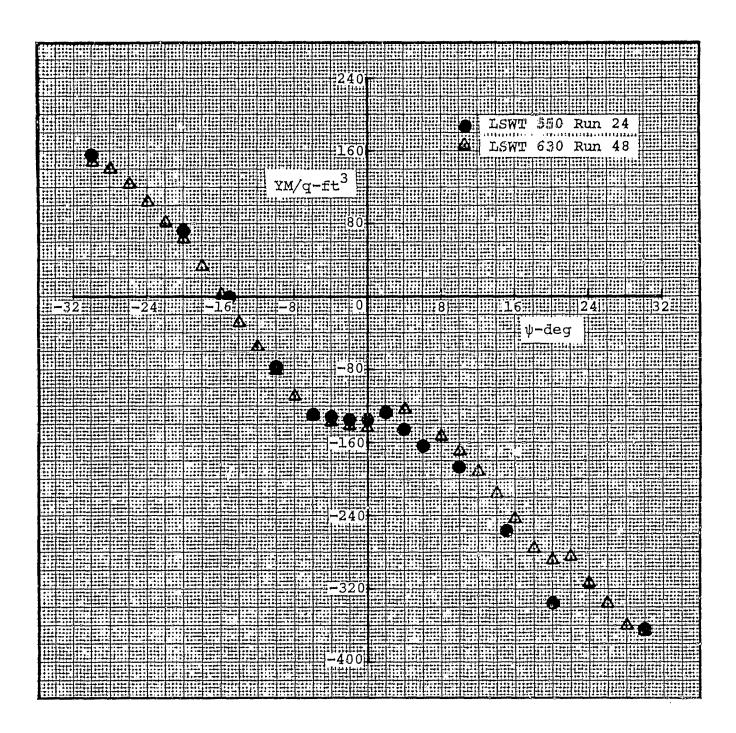


Figure 31. Comparison of Fifth-Scale Yawing Moment Characteristics in Yaw for Helicopter

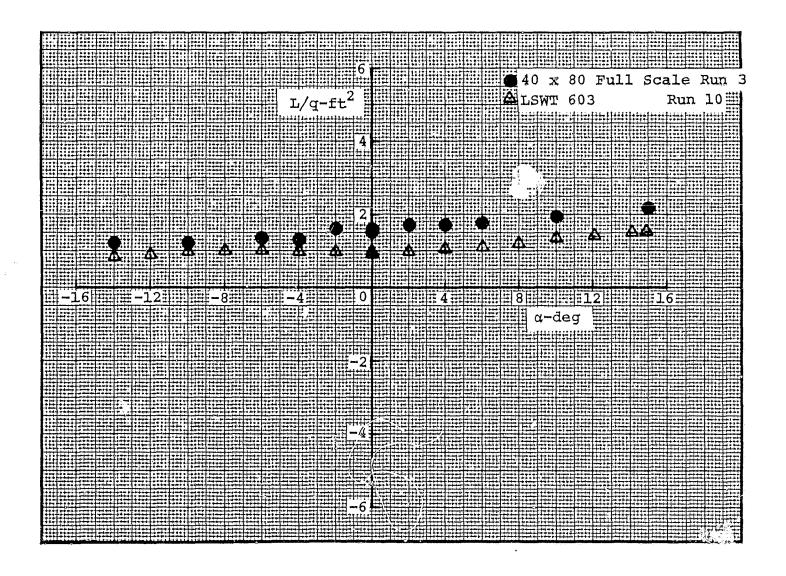


Figure 32. Comparison of Tare Lift Characteristics in Pitch for Three-Point Mount

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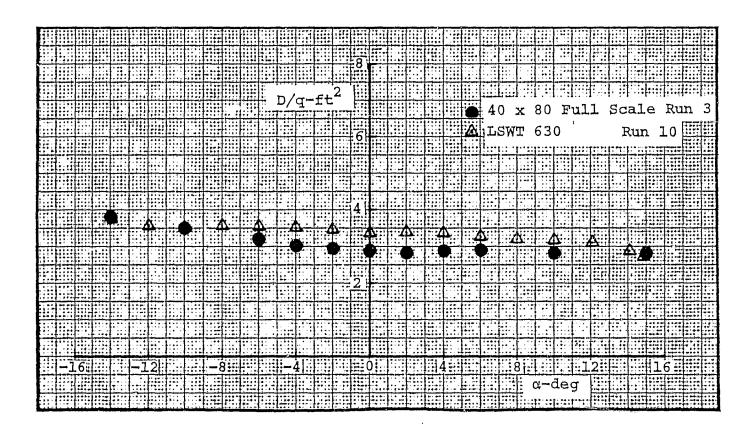


Figure 33. Comparison of Tare Drag Characteristics in Pitch for Three-Point Mount

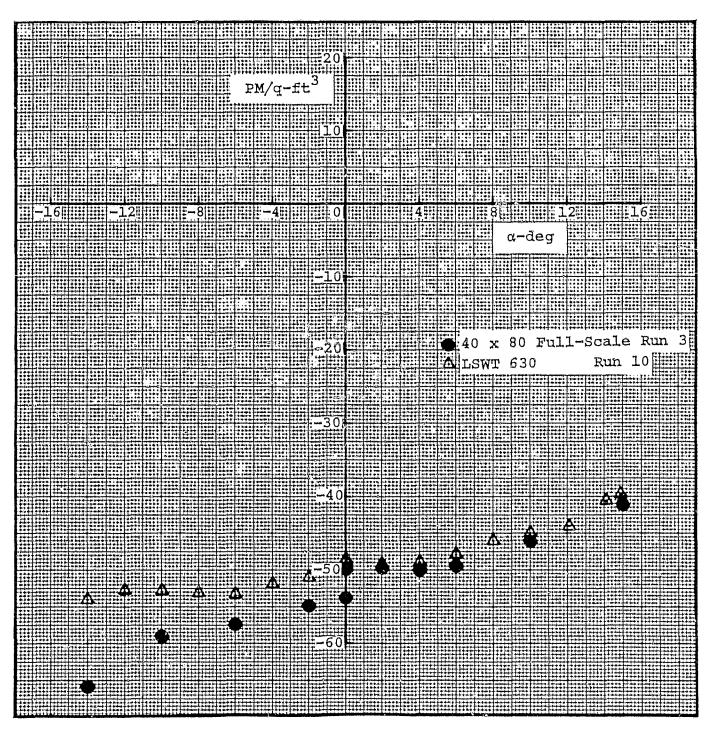


Figure 34. Comparison of Tare Pitching Moment Characteristics in Pitch for Three-Point Mount

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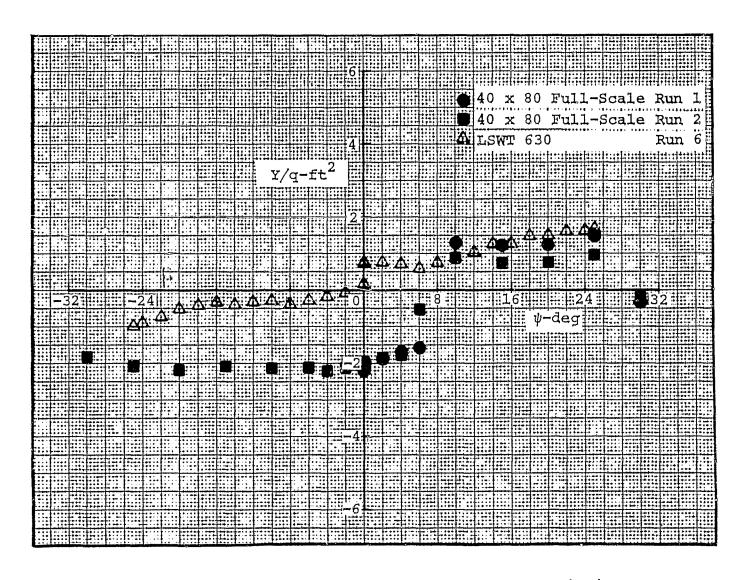


Figure 35. Comparison of Tare Side Force Characteristics in Yaw for Three-Point Mount

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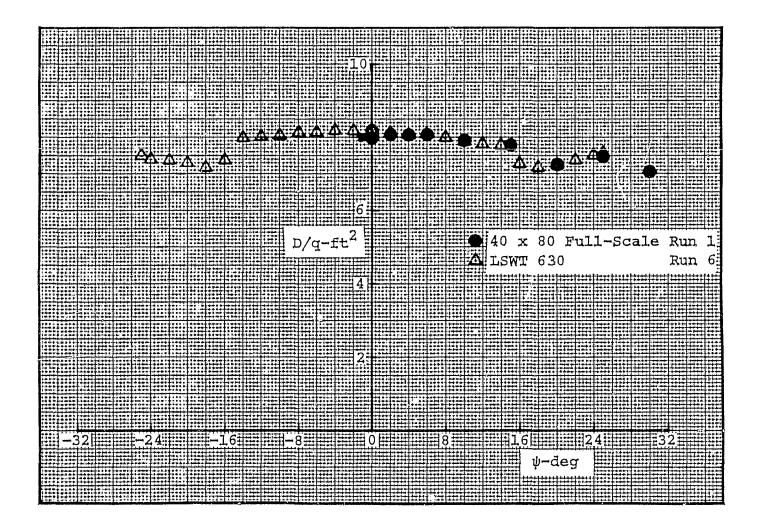


Figure 36. Comparison of Tare Drag Characteristics in Yaw for Three-Point Mount

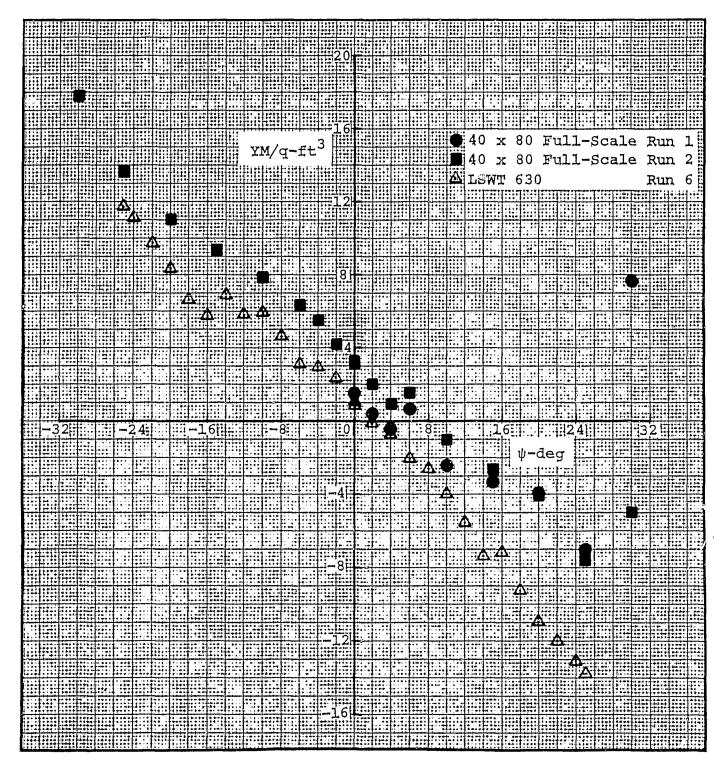


Figure 37. Comparison of Tare Yawing Moment Characteristics in Yaw for Three-Point Mount

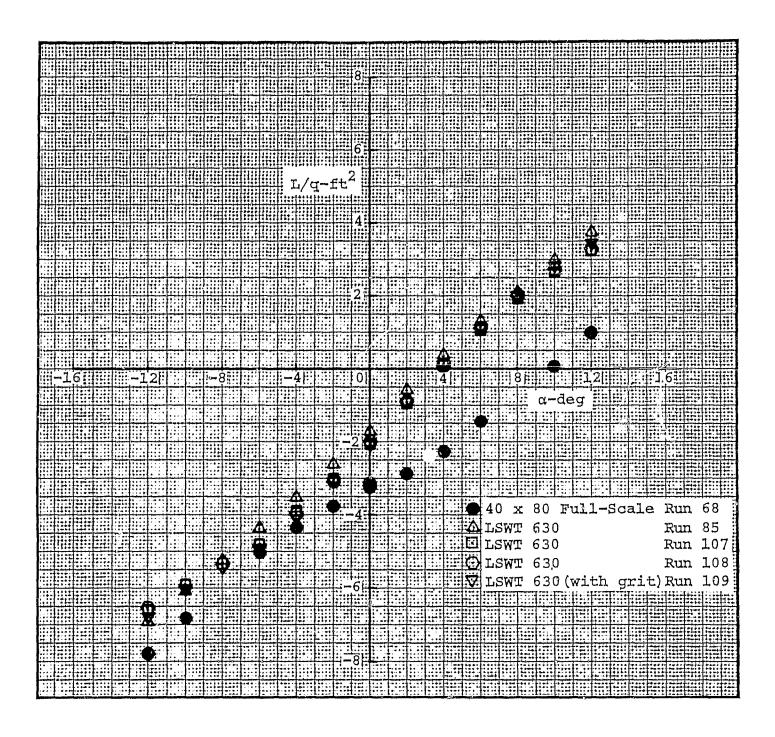


Figure 38. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Basic Fuselage

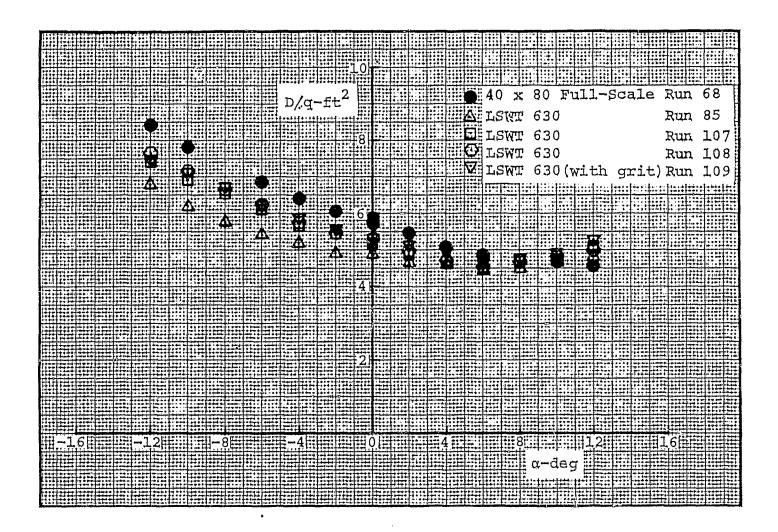


Figure 39. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Basic Fuselage

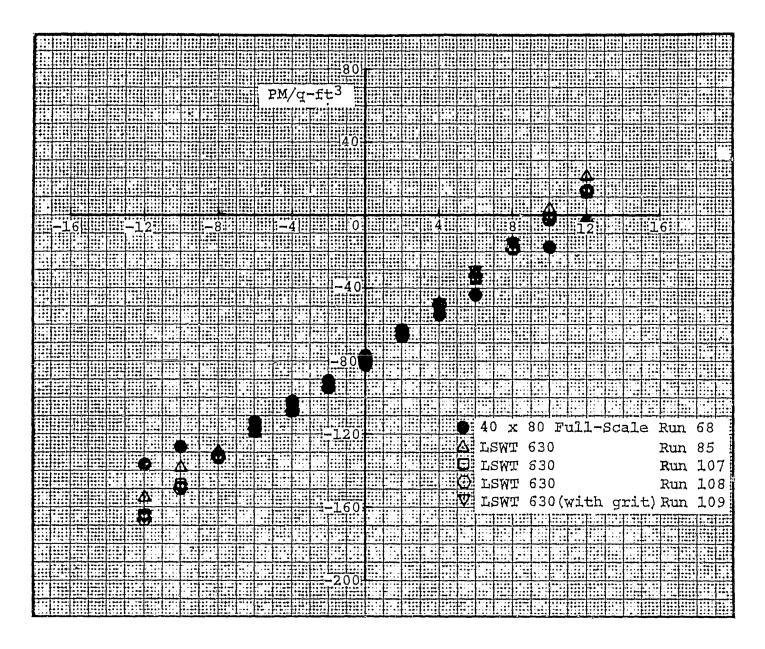


Figure 40. Full/Fifth-Scale Comparison of Pitching Moment Characteristics in Pitch for Basic Fuselage



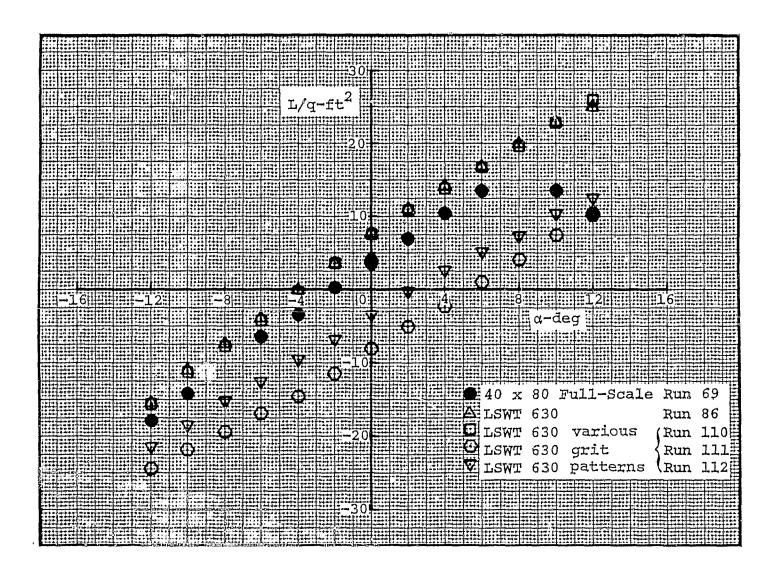


Figure 41. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Basic Fuselage with Wings

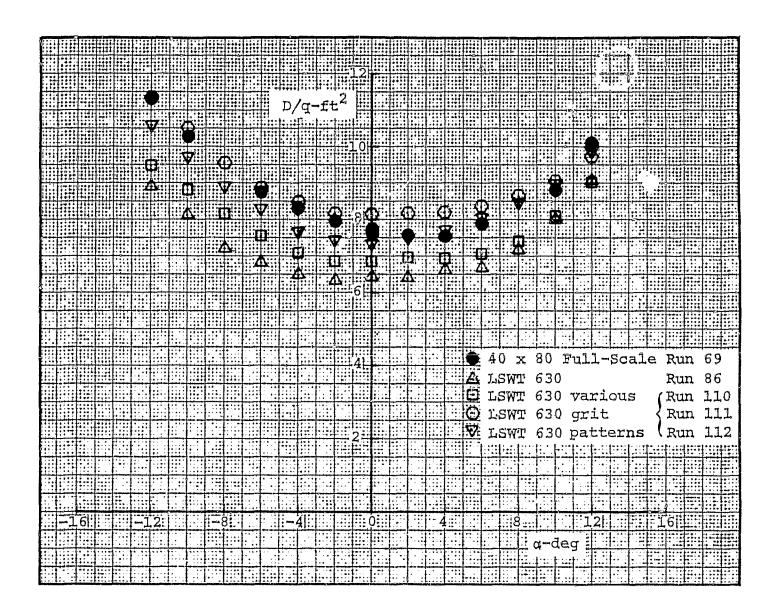


Figure 42. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Basic Fuselage with Wings

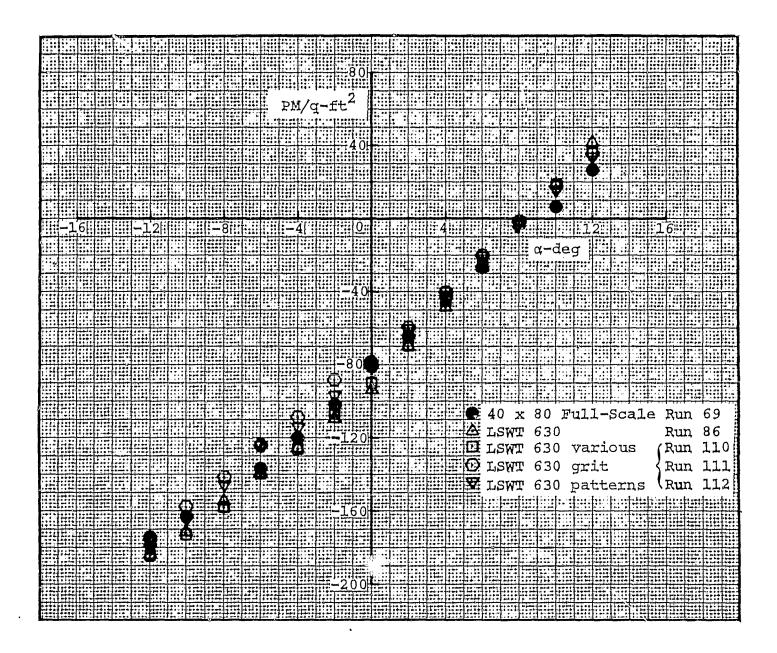


Figure 43. Full/Fifth-Scale Comparison of Pitching Moment Characteristics in Pitch for Basic Fuselage with Wings



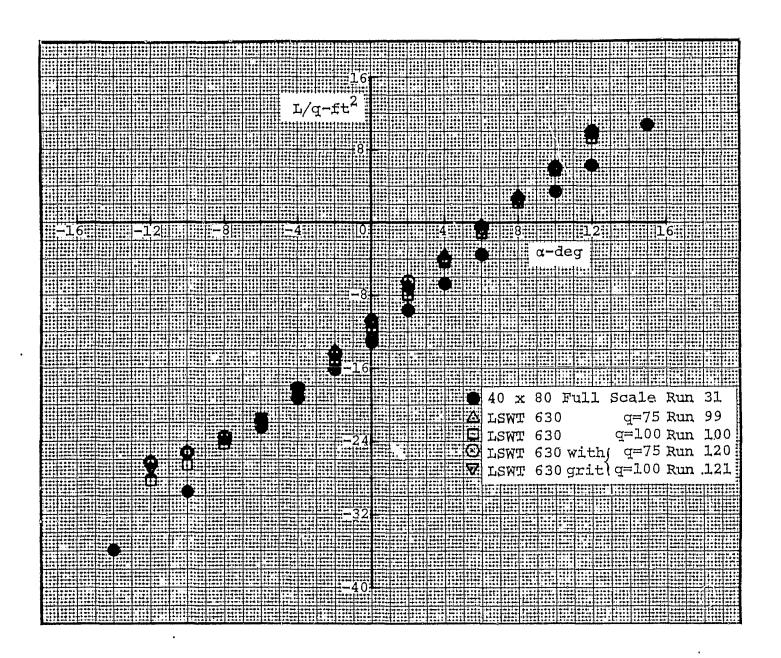


Figure 44. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Helicopter without Wings

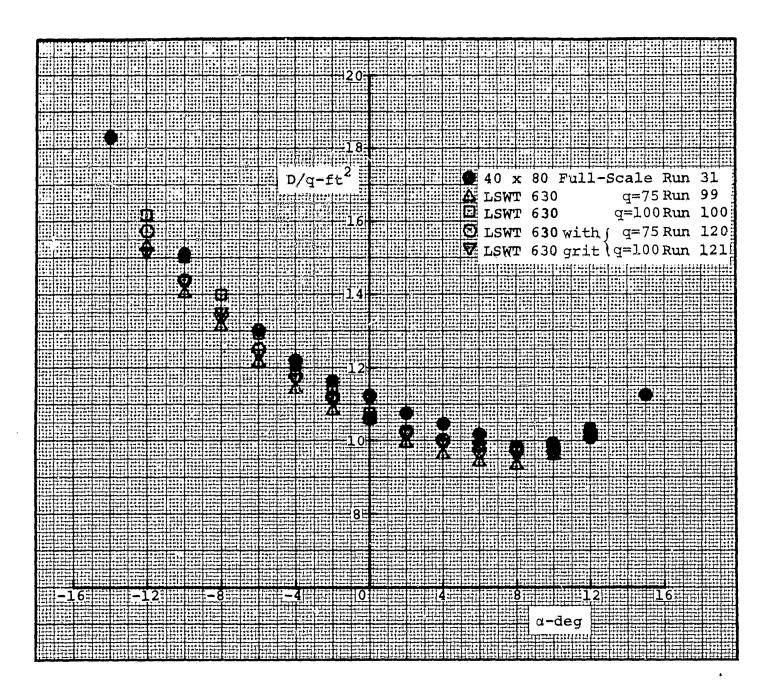


Figure 45. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Helicopter without Wings



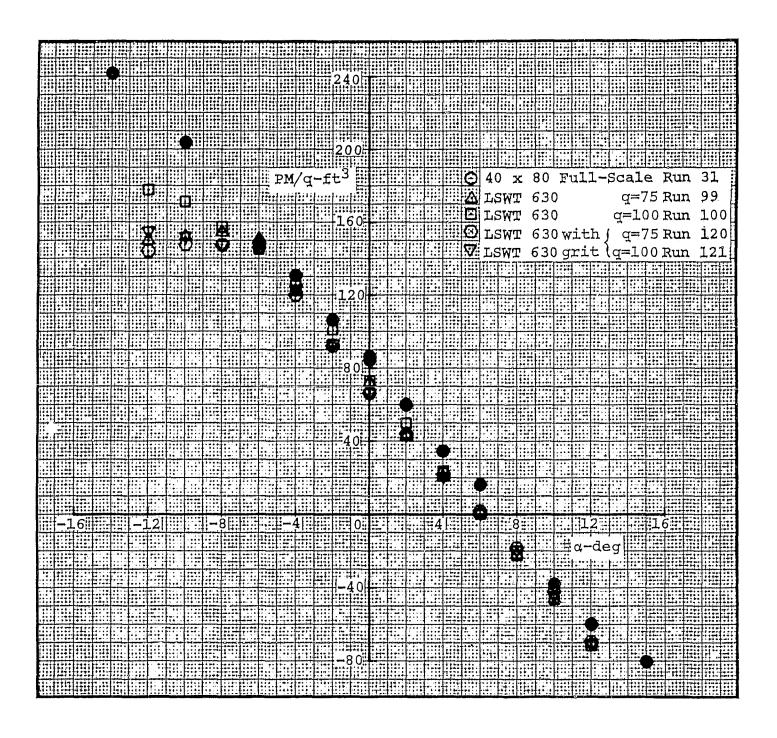


Figure 46. Full/Fifth-Scale Comparison of Pitching Moment Characteristics in Pitch for Helicopter without Wings

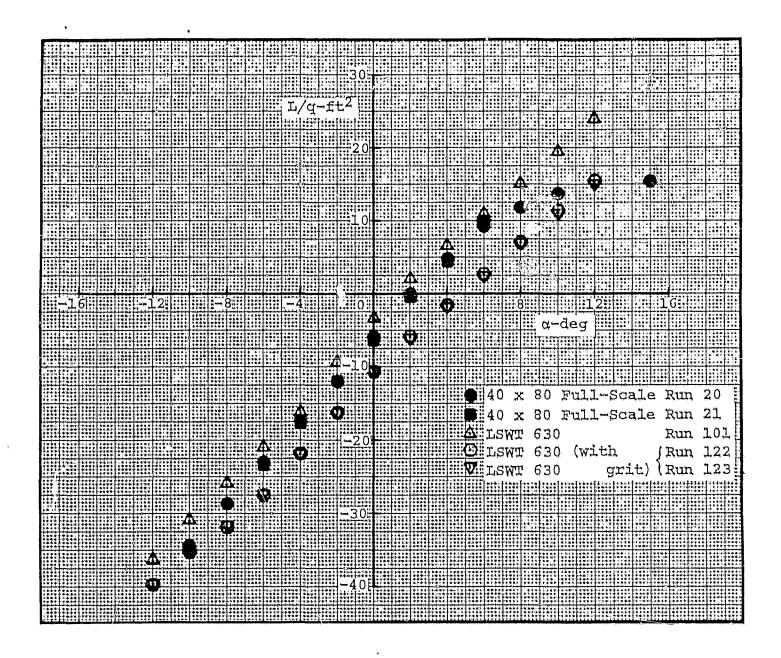


Figure 47. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Helicopter

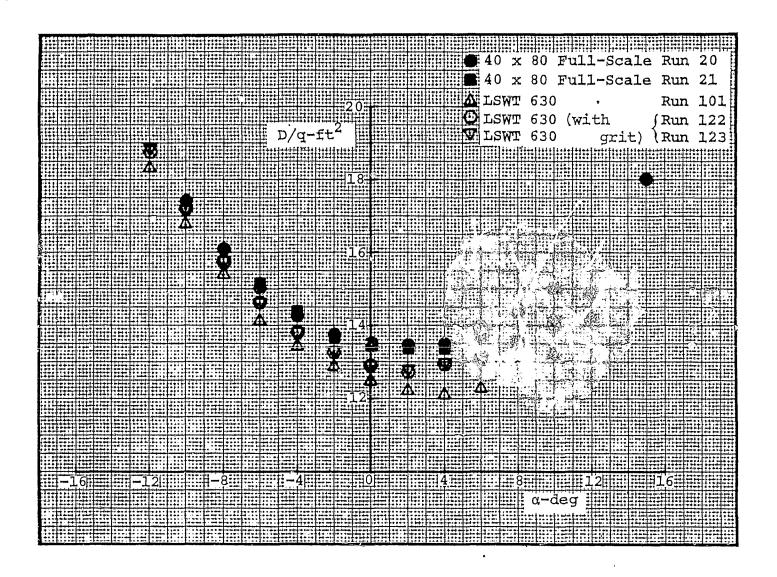


Figure 48. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Helicopter

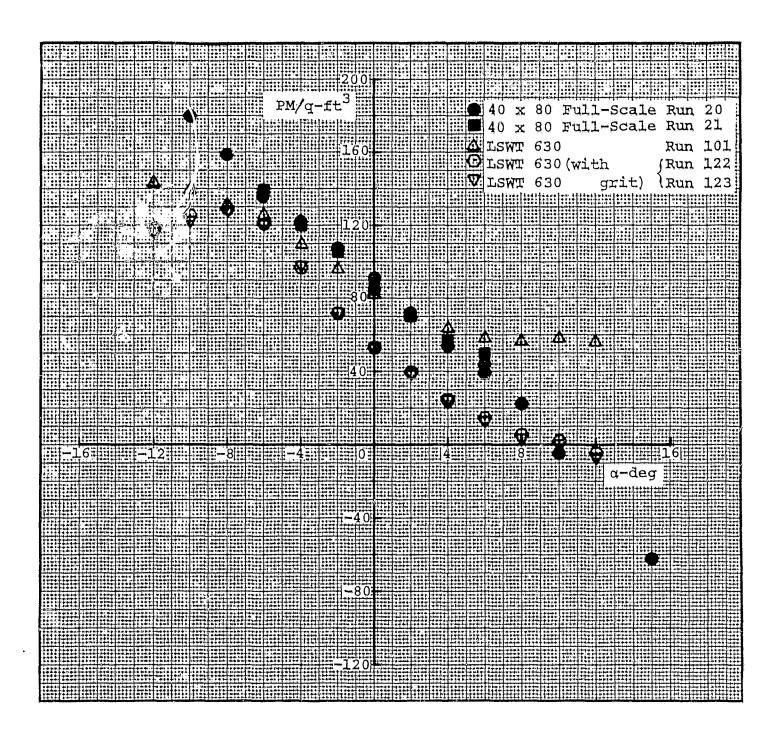


Figure 49. Full/Fifth-Scale Comparison of Pitching Moment Characteristics in Pitch for Helicopter

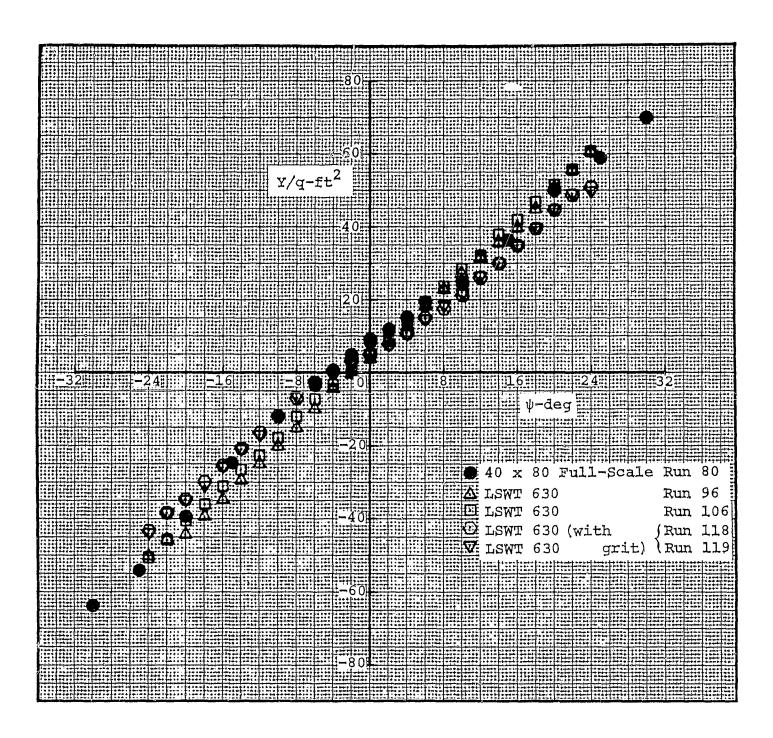


Figure 50. Full/Fifth-Scale Comparison of Side Force Characteristics in Yaw for Helicopter

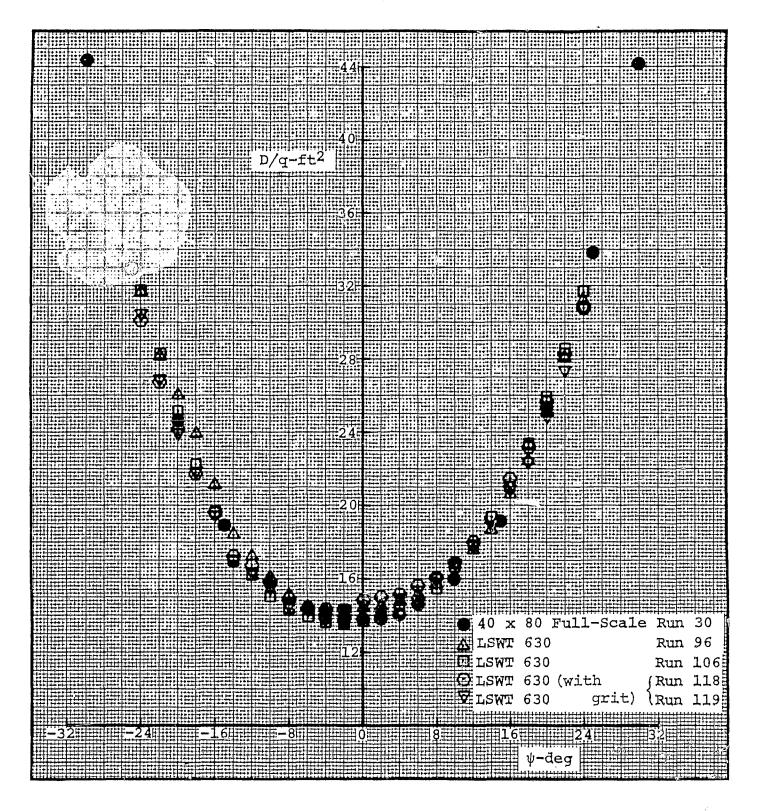


Figure 51. Full/Fifth-Scale Comparison of Drag Characteristics in Yaw for Helicopter



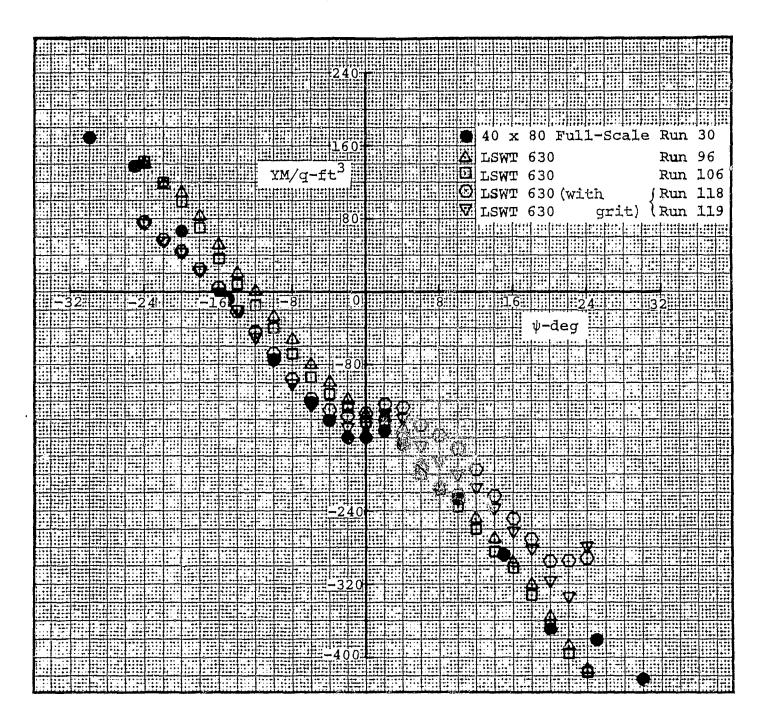


Figure 52. Full/Fifth-Scale Comparison of Yawing Moment Characteristics in Yaw for Helicopter

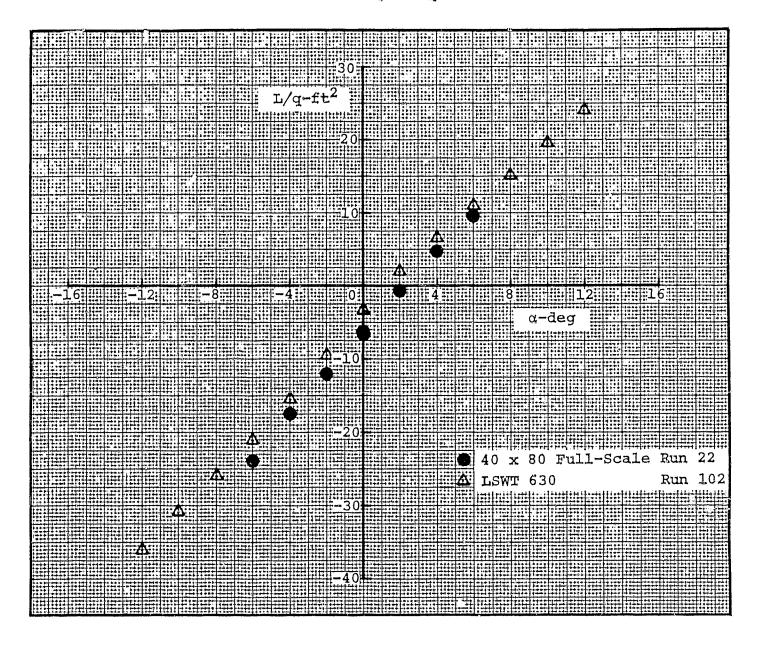


Figure 53. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Helicopter without Tail Rotor

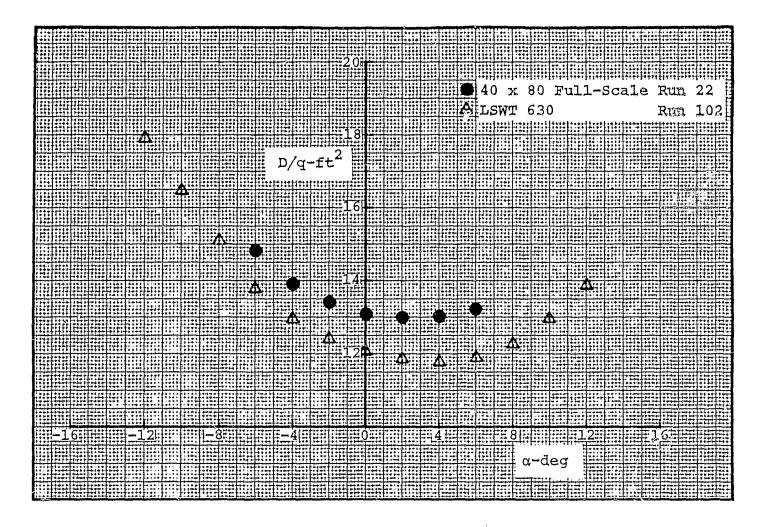


Figure 54. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Helicopter without Tail Rotor

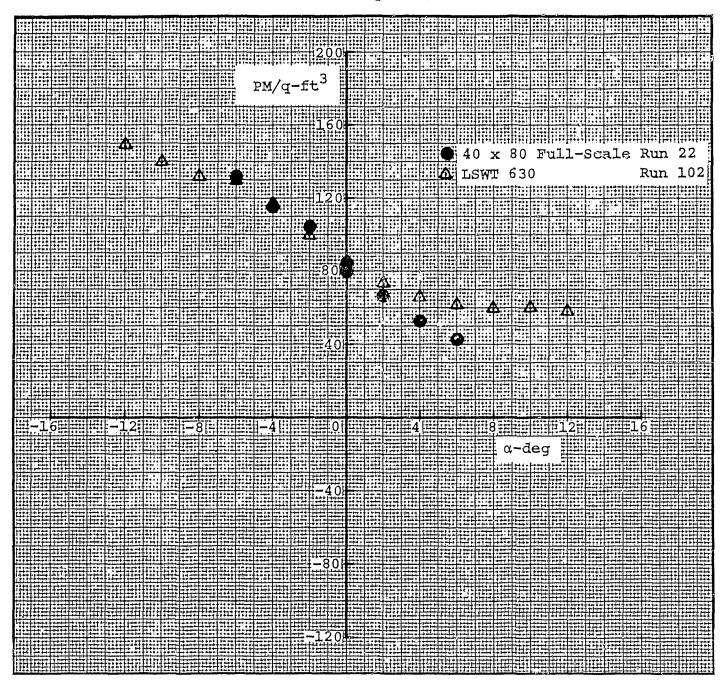


Figure 55. Full/Fifth-Scale Comparison of Pitching Moment Characteristics in Pitch for Helicopter without Tail Rotor

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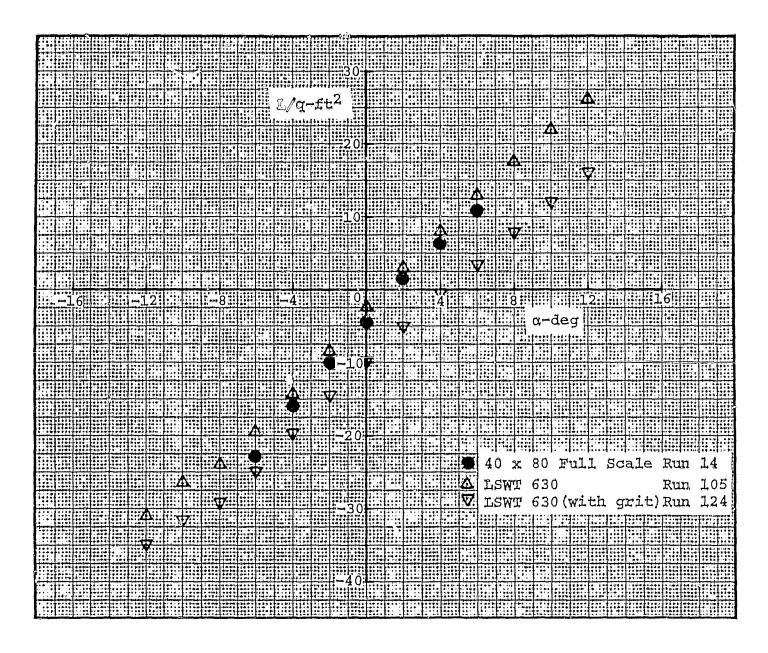


Figure 56. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Helicopter with Landing Gear Doors Open

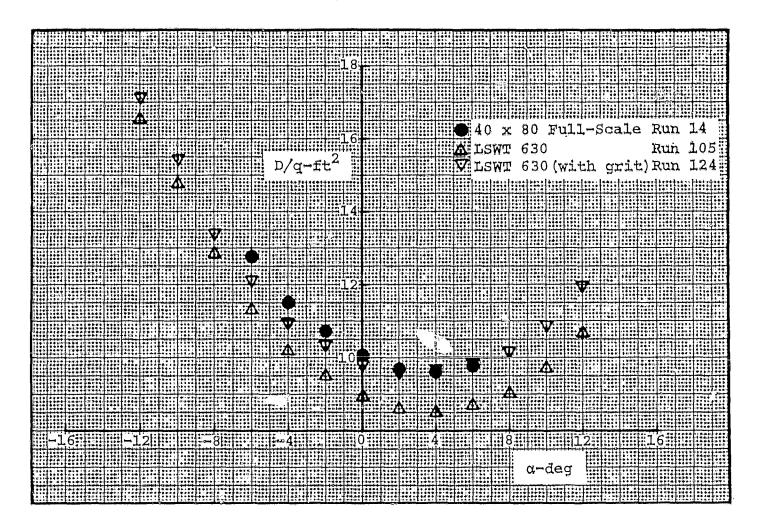


Figure 57. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Helicopter with Landing Gear Doors Open

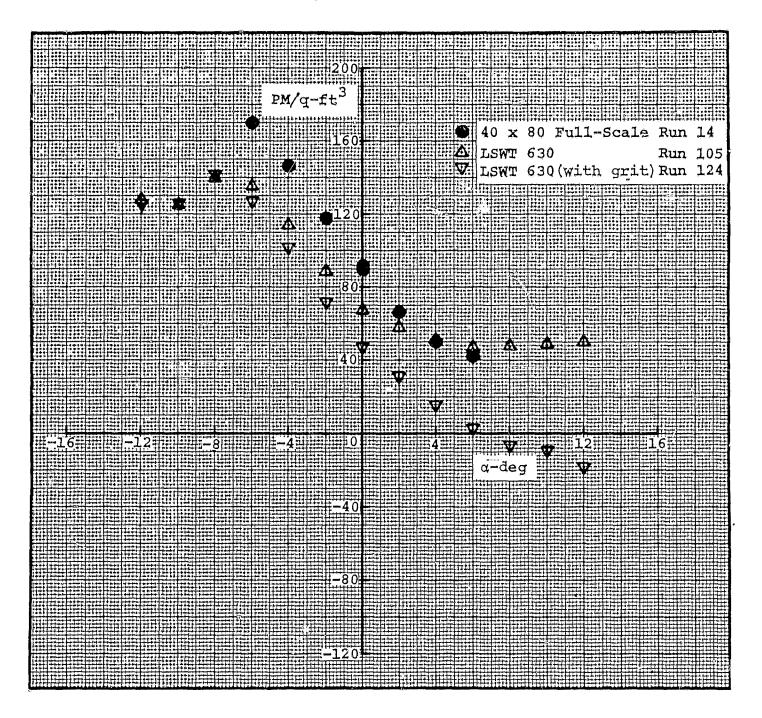


Figure 58. Full/Fifth-Scale Comparison of Pitching Moment Characteristics in Pitch for Helicopter with Landing Gear Doors Open

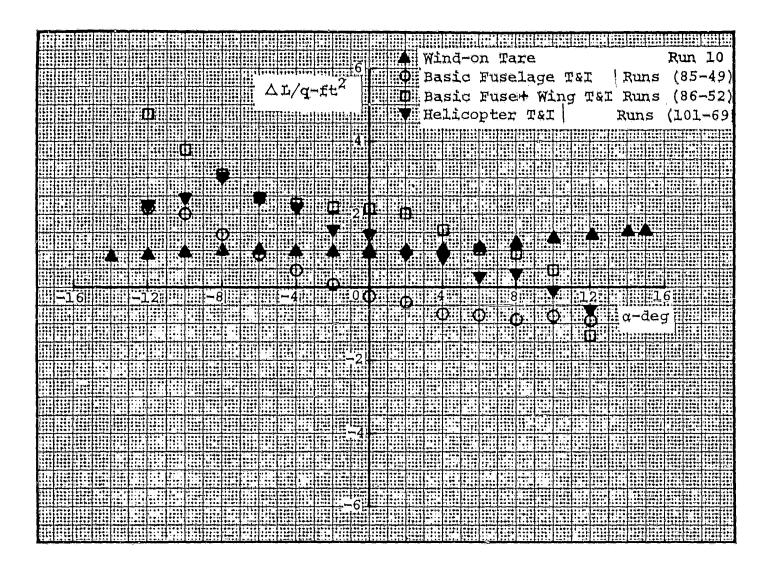


Figure 59. Tare and Interference Corrections to Lift Characteristics in Pitch for Three-Point Mount

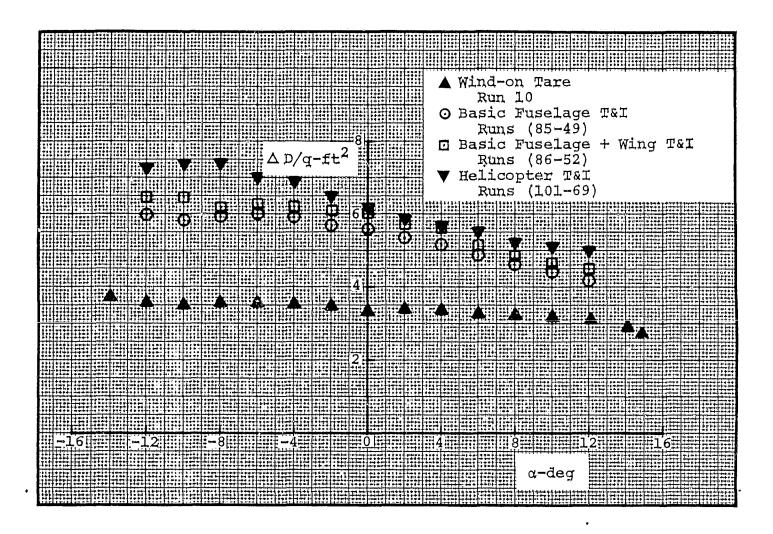


Figure 60. Tare and Interference Corrections to Drag Characteristics in Pitch for Three-Point Mount

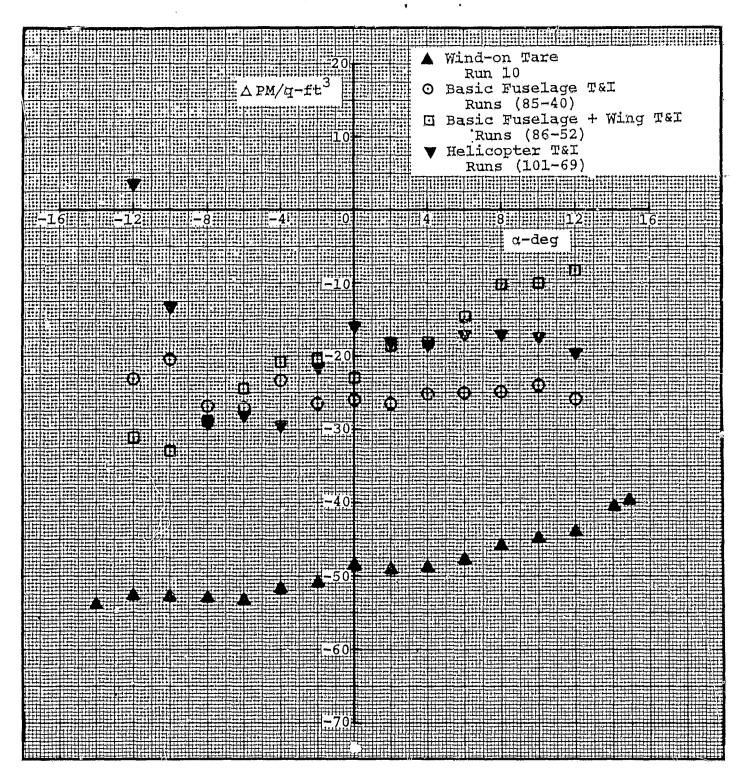


Figure 61. Tare and Interference Corrections to Pitching Moment Characteristics in Pitch for Three-Point Mount

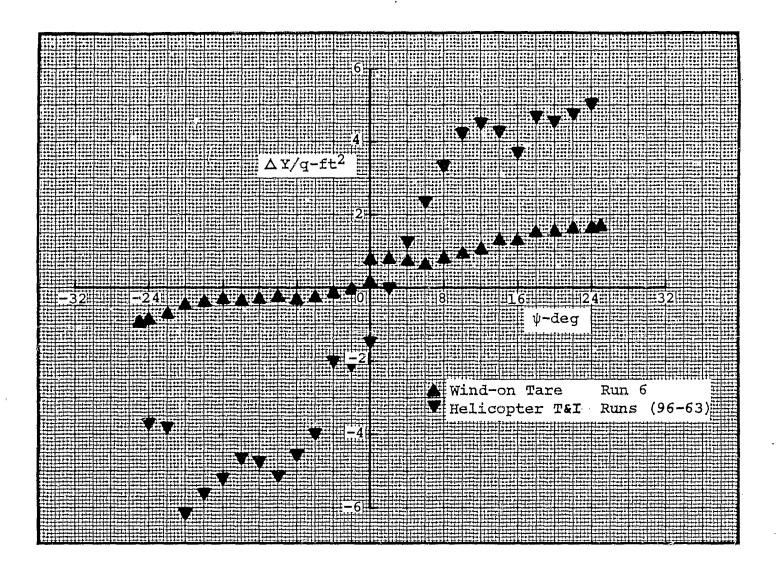


Figure 62. Tare and Interference Corrections to Side Force Characteristics in Yaw for Three-Point Mount

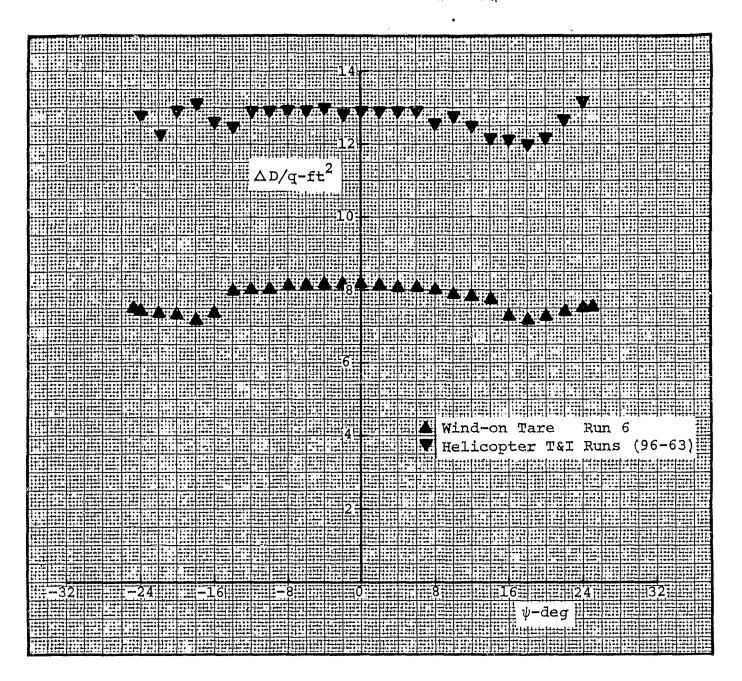


Figure 63. Tare and Interference Corrections to Drag Characteristics in Yaw for Three-Point Mount

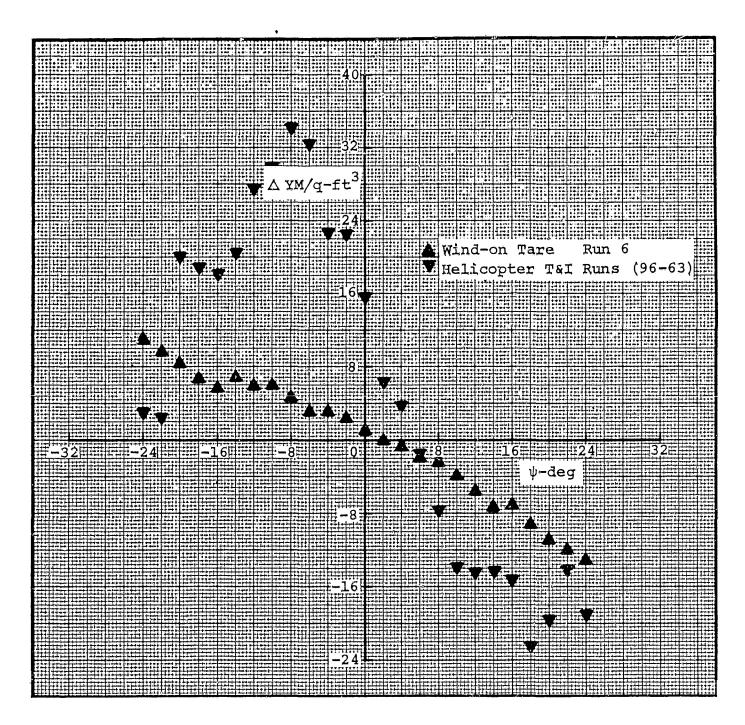
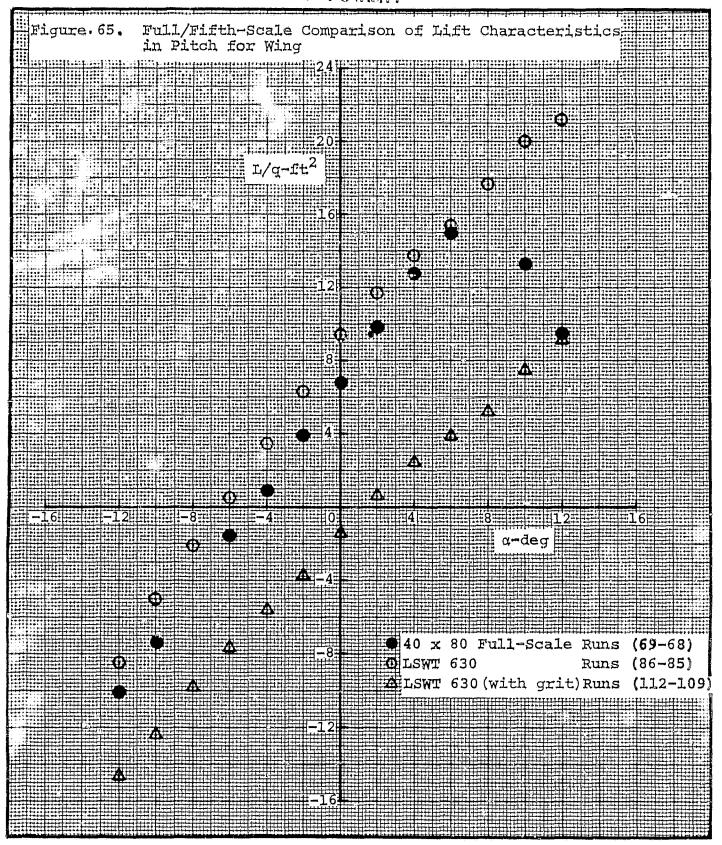
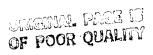


Figure 64. Tare and Interference Corrections to Yawing Moment Characteristics in Yaw for Three-Point Mount





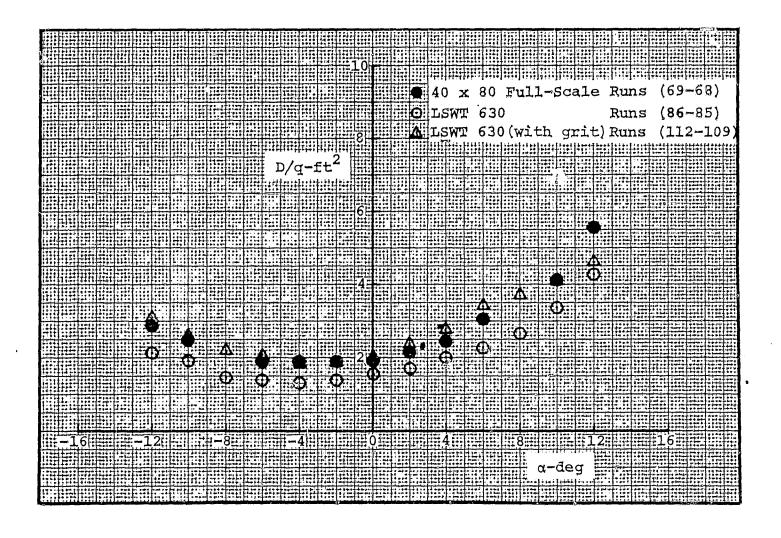
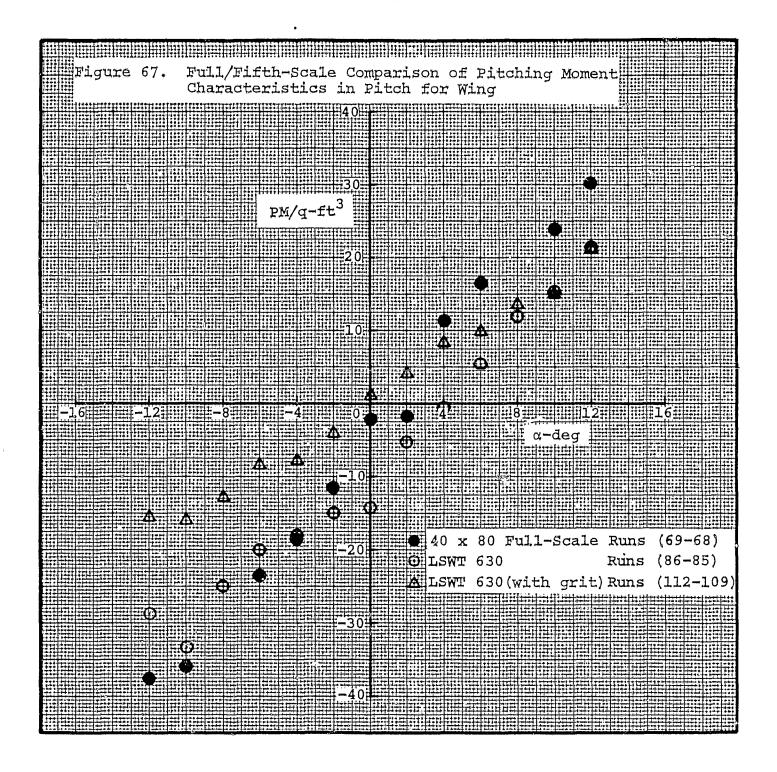


Figure 66. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Wing



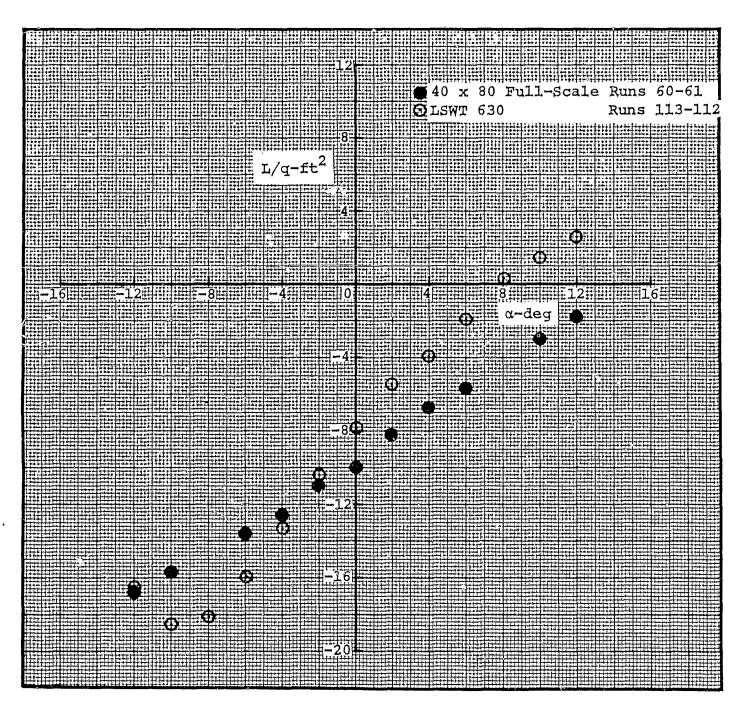


Figure 68. Full/Fifth-Scale Comparison of Lift Characteristics in Pitch for Horizontal Stabilizer

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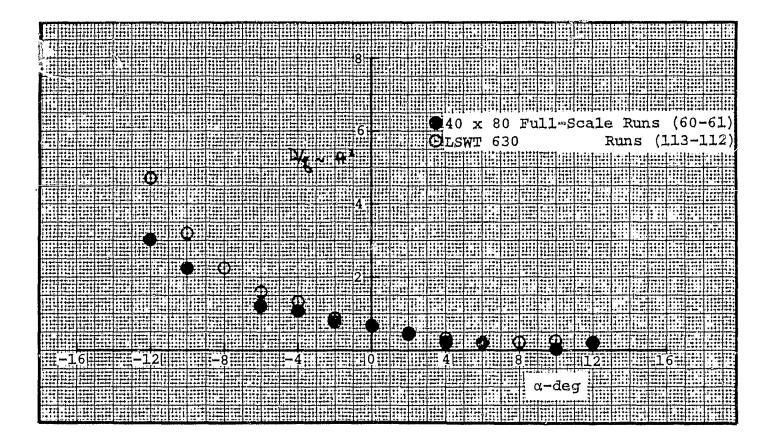
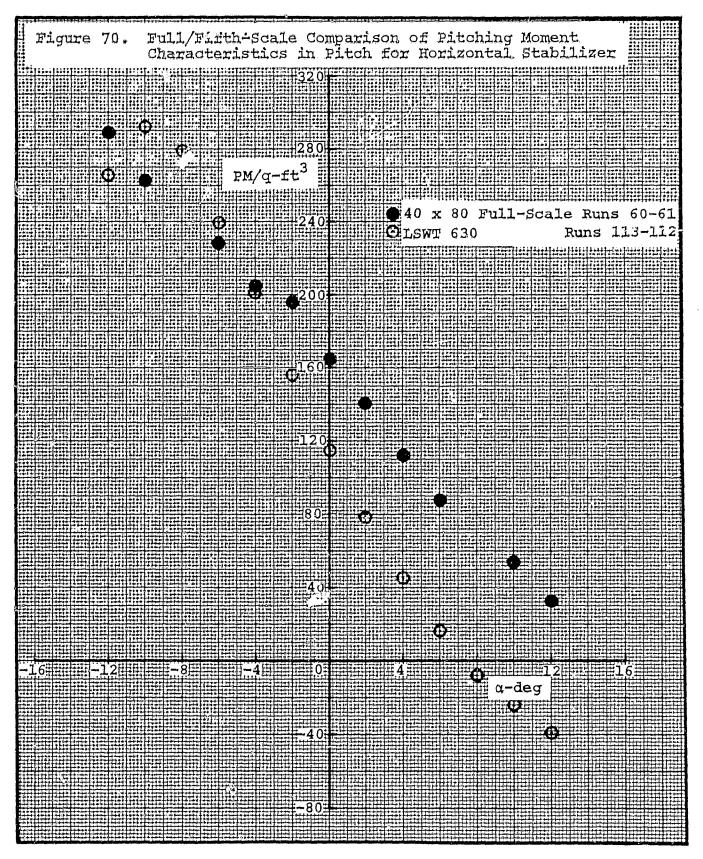
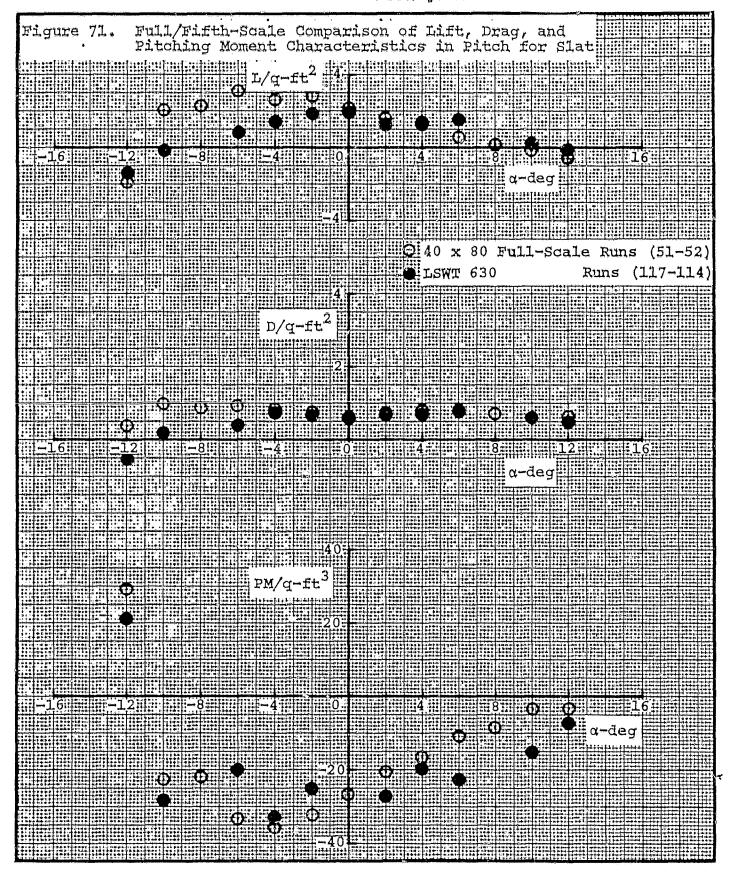
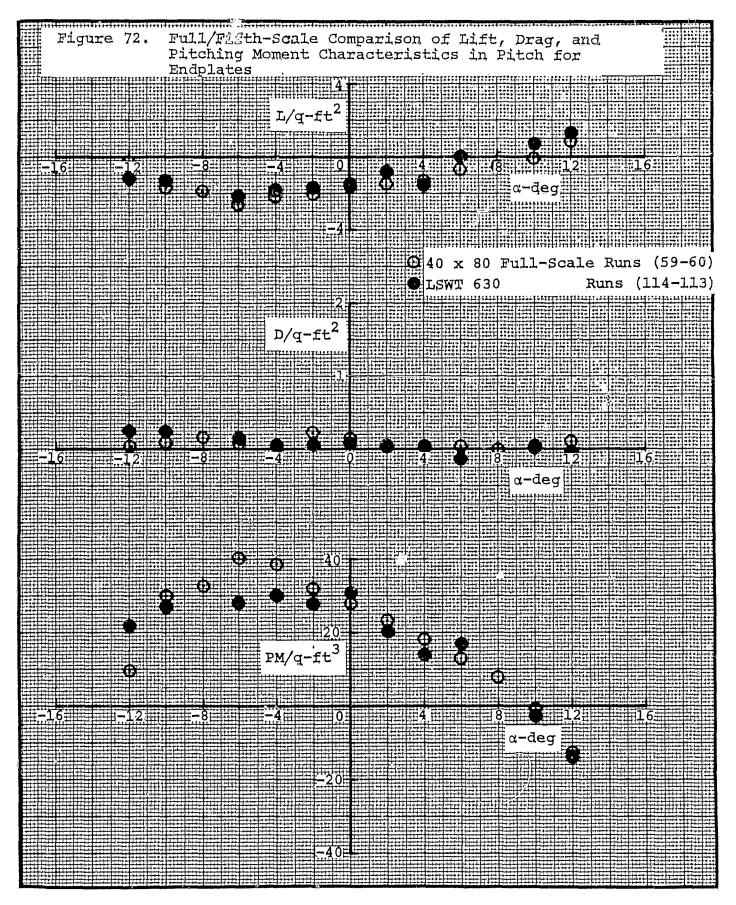


Figure 69. Full/Fifth-Scale Comparison of Drag Characteristics in Pitch for Horizontal Stabilizer

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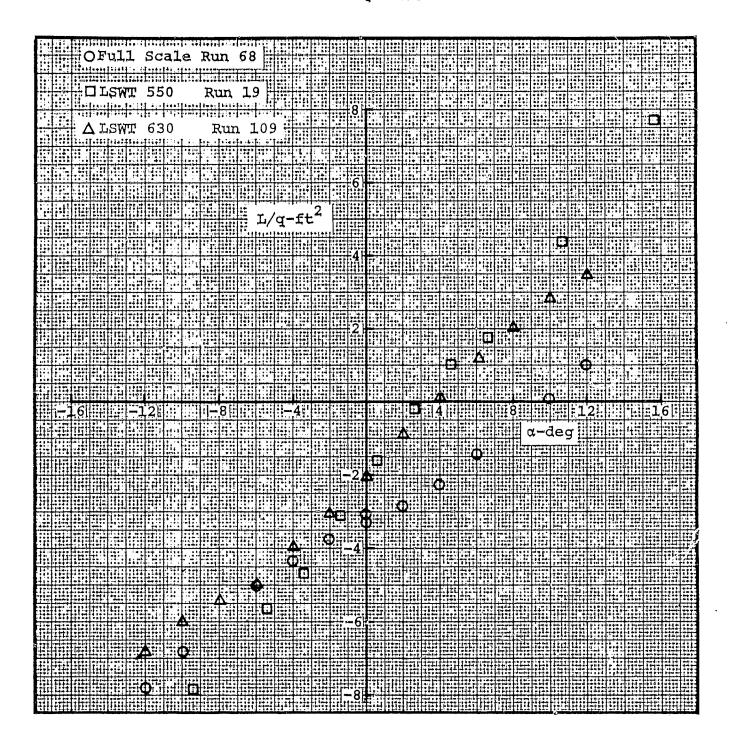


Figure 73. Summary Comparison of Lift Characteristics in Pitch for Basic Fuselage

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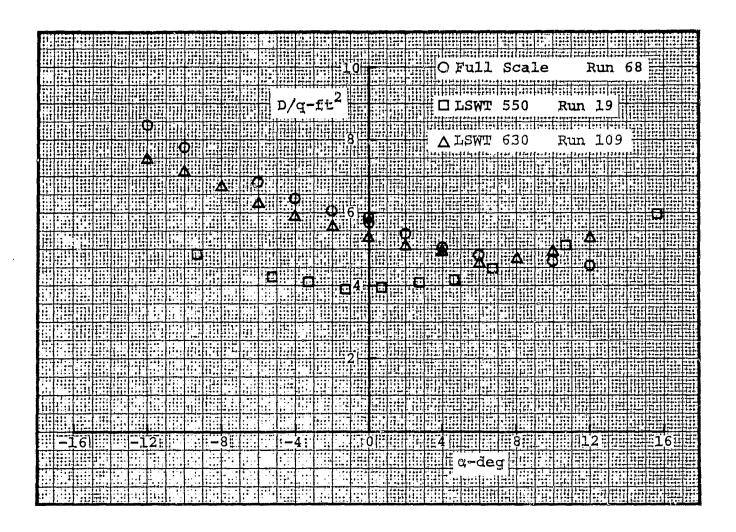


Figure 74. Summary Comparison of Drag Characteristics in Pitch for Basic Fuselage

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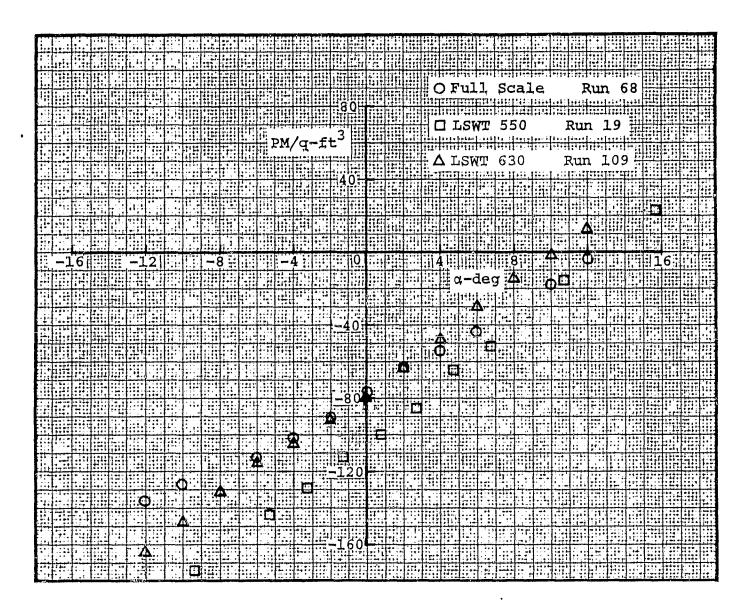


Figure 75. Summary Comparison of Pitching Moment Characteristics in Pitch for Basic Fuselage

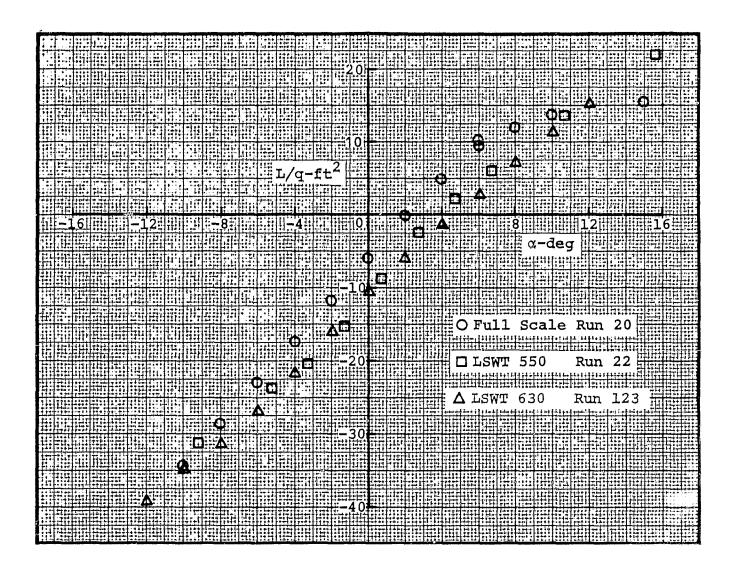


Figure 76. Summary Comparison of Lift Characteristics in Pitch for Helicopter

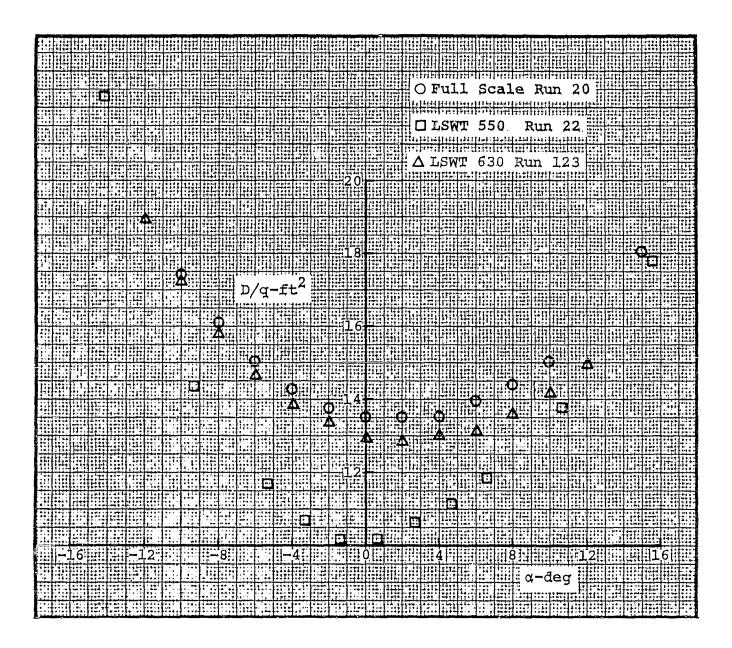


Figure 77. Summary Comparison of Drag Characteristics in Pitch for Helicopter

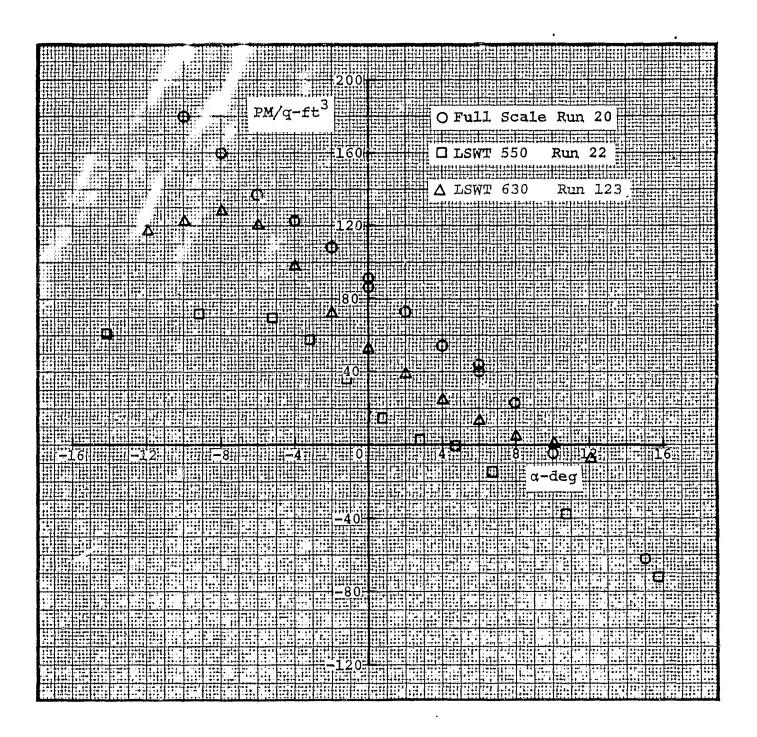


Figure 78. Summary Comparison of Pitching Moment Characteristics in Pitch for Helicopter

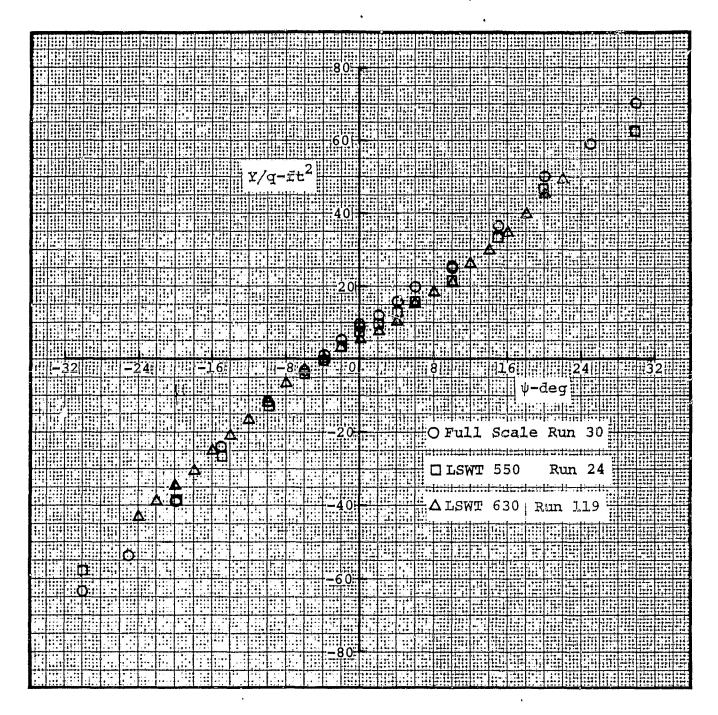


Figure 79. Summary Comparison of Side Force Characteristics in Yaw for Helicopter

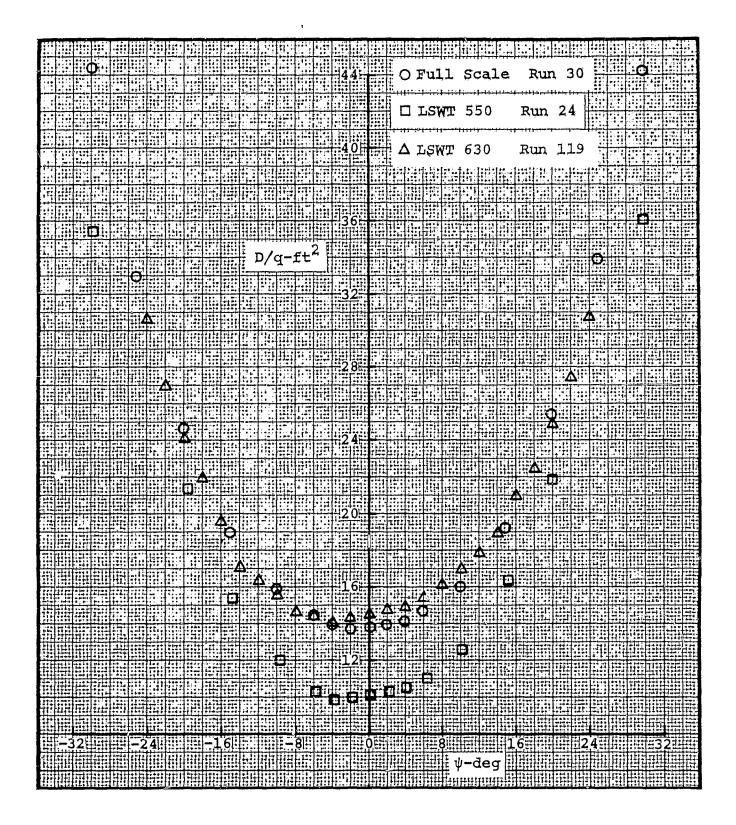


Figure 80. Summary Comparison of Drag Characteristics in Yaw for Helicopter

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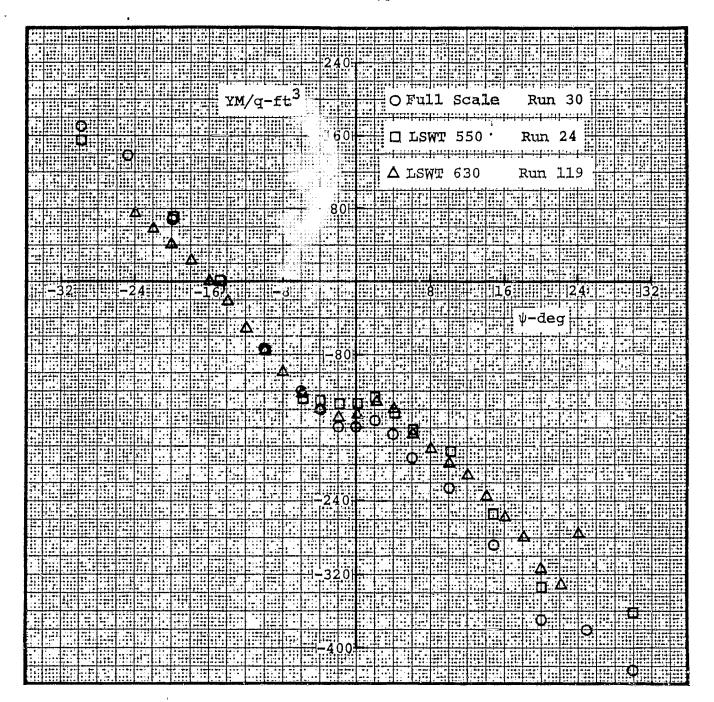


Figure 81. Summary Comparison of Yawing Moment Characteristics in Yaw for Helicopter

TABLE I. COMPARISON OF REYNOLDS NUMBERS FOR FULL-SCALE AND FIFTH SCALE TESTS

		Reynolds Number - Millions									
Run No.		Reynolds No/ft		Wing		Horizon Stabili		Fi	.n	Mounting Strut	
Full Scale	LSWT 630	Full Scale	LSWT 630	Full .Scale	LSWT 630	Full Scale	LSWT 630	Full Scale	LSWT 630	Full Scale	LSWT 630
14	124	1.25	.31	6.13	1.52	2.81	.70	2.95	. 73	2.25	.56
20	123	1.25	.31	6.13	1.52	2.81	.70	2.95	.73	2.25	.56
31	120	1.28	.31	6.27	1.52	2.88	.70	3.02	.73	2.30	.56
68	109	1.29	.30	6.32	1.47	2.90	.68	3.04	.71	2.32	.54
69	112	1.29	.30	6.32	1.47	2.90	.68	3.04	.71	2.32	.54
30	119	.65	.32	3,19	1.57	1.46	.72	1.53	.76	.38	.1.9

Notes:

- 1. Pitch runs were made at q=62.5 psf full-scale and q=75 psf fifth-scale corresponding to velocities of approximately 236 fps and 252 fps respectively.
- 2. Yaw runs (30 and 119) were made at q=16.2 psf and q=83 psf corresponding to V=118 fps and V=272 fps.
- 3. Reference lengths used to calculate these Reynolds Numbers:

•	Full Scale	Fifth Scale
RN/ft Wing chord Horizontal Stabilizer chord Fin chord Mounting strut fairing chord (pitch) Mounting Strut diameter (yaw)	1.0 ft 4.9 ft 2.25 ft 2.36 ft 1.8 ft .58 ft	.2 ft .98 ft .45 ft .472 ft .36 ft

Remove fin horiz

stab & endplates

TEST T&I STATIC α RUN CONFIGURATION RANGE RANGE TARE REMARKS RUN NO. (PSF) (DEG) (DEG) 0 -25/+25 83 1 Model Strut Fouling After Data Pt. 4 1* x_3 8 = 83 psf(TS) 1 . No. 36 Grit on Upper Fwd Support & 2 Rear Strut Remove grit and modify front of hor-izontal fairing exposing horiz beam. 3 -10/10 x₃² Increase dia of pitch strut to simu-4 -6/46 late telescoping NASA system x₃ 5 Simulate gusseted joint at base of dummy strut. x_3^4 -25/25 Modify gusseted joint simulation 6 (matches drag of 40x80#) 7 75 Repeat Run #6 @ q = 75 psf -15/15 Pitch run with same configuration as 8* Runs #6 & #7 q = 75 psf $\mathbf{x_4}$ -14/14 Add large vert fairing & remove 9 dummy strut (40 x 80 #4) Add dummy strut with fairing 10 x_5 (40 × 80 #3) BCN1QO4P3Y1V2W1M1HTE MODEL IMAGE Complete A/c smooth -51/25 75 11 11* INV. OUT 0 -30/30 12 Add 15" fin cap 12* V. 12 Repeat 12 @ g=83 psf -30/30 13 0 83 -15/25 75 11 Remove fin 14 11 Remove endplates 15 Remove horizontal 16* 16 stabilizer Add fin with 10" cap 11 17 V2 Remove wing 18 18* Add horizontal and 18 1,9 H⁺E endplates

18

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TABLE II. RUN SCHEDULE FOR LOW SPEED WIND TUNNEL TEST 630

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tion of LSWT 550 Run #20
Add fin with 15" cap & transition

of LSWT 550 Run #18

550 Run #17

strips to match LSWT 550 Run #19

Add T/R quard to match configuration

Add horizontal stab to match LSWT

TEST STATIC T&I α RUN REMARKS CONFIGURATION RANGE RANGE TARE RUN (PSF) NO: (DEG) (DEG) 21 BCN1QO4P3Y1 -15/25 75 18 20 MODEL IMAGE Repeat Run #20 INV. ΤÑ 22 H⁺E 18 1,9 Add short fin horiz stab & endplates 23 18 Add short fin horiz 18 stab & endplates Add wings with 24 11 17 retracted gear $BCN_1QO_4P_3Y_1V_2W_1M_1H^{\dagger}E$ Remove fin 16 25 16 $\mathtt{BCN_1QO_4P_3Y_1V_2W_1M_1H}^+\mathtt{E}$ MODEL IMAGE Add horiz stab -15/25 26 75 11 15 INV II 14 Add endplates 27 Add fin with 10" cap 11 11 28 Add 15" fin cap q = 83 psf 29 -30/30 83 12 13 Repeat #29 with 12 12 30 75 q = 75 psf(ALIGN 31* -15/25 32 28 MODEL Add fin v_2 UPRIGHT w/10" cap RUN) 32 T+I 32* BEGIN DATA RUNS Repeat #31 w/o 11 image Add fin with 15" cap -30/30 12 33* 33 12 Repeat #33 with g = 83 psf 34 83 33 Remove fin 14 -15/25 75 32 35 32 15 Remove endplates 36 Remove horizontal stab 37 16 37* Add fin with 10" cap 38 32 17 Va 18 Remove wing 39 75 39 1.9 Add horiz stab and endplates HE 39 40 20 Remove fin, horizontal stab # 39 41 endplates (TS)₂ Add transition strips in configura-20 39 42

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39

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TABLE II. CONTINUED.

ſ			α	ψ	T ==== T	071710	~0.	
	RUN NO. CONFIGURATION		RANGE (DEG)	RANGE (DEG)	TEST Q (PSF)	STATIC TARE	T&I RUN	REMARKS
	46	ECN ₁ QO ₄ P ₃ Y _P V ₂ H ⁺ E(TS) ₂ G	-15/25	ō I	75	39	19	Add endplates with transition strips to match LSWT 550 Run 16
	47	W ₁ M ₁				32	11	Add wings with retracted gear with trans strips to match LSWT 550 #15
	48	TF1R1		-30/30		48	12	Add T/R hub, M/R hub & exhaust ejector fairing to match LSWT 550 #24
	49	v ₂	-15/25	0	75	39	18	Remove wings horiz stab, endplates M/R grit, T/R guard, change to 1 10" fin cap
	50	BCN ₁ QO ₄ P ₃ Y _P V ₂ W ₁ M ₁ H ⁺ E(TS) ₂ GTF ₁ R ₁ ⁶⁰				39	18	Modify T/R gearbox fairing to pro- duction configuration (compares to 40x80 Run #68)
	51	BCN ₁ QO ₄ P ₃ Y _P V ₂ W ₁ M ₁ H [†] E T F ₁	0	-30/30	83	51	13	Yaw run with configuration of #50 @ 8 = 83 psf
	52	W ₁ M ₁	-15/25	. 1	75	32	17	Add wing with retracted gear (compares to 40x80 Run #69)
126	53	Y				32	17	Remove production T/R gearbox fairing
1	54	H ⁺				32	1.5	Remove fin, add horiz stab
i	55	R ₁ 60				32	15 (Add M/R 8 60°
	56	E I				32	14	Add end plates
1	57					32	1.4	Remove M/R
	58	V ₂				32	11	Add fin with 10" cap
1	59*					59	1.1	Add M/R @ 60°
	60	G				59	11	Add T/R guard antenna
	61	V-1		•		51	1.1	Add 15" fin cap
	62		0	-30/30 	83	48	13	Yaw run with configuration of Run #61 @ 9 = 83 psf
	63					4.8	1,3	Remove exhaust ejector fairing
	64				75	48	1.2	Repeat 63 @ q = 75 psf (compares to 40x80 Run #30)
	65		-15/25	0		59	11	Pitch run with configuration of Runs 63 & 64
- 1	66	V ₂				59	11	Add 10" fin cap
	67*					67	19	Remove wings (compares to 40x80 Run #31)
	68		-12/+12		100	67	1.9	Repeat: #67 @ q = 100 psf
	69	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-15/25		75	59	11	Add wings and open fuel sump re- cesses (compares to 40x80 Runs #20 & #21)

TABLE II. CONTINUED.

α TEST STATIC T&I RUN RANGE (DEG) q (PSF) CONFIGURATION RANGE TARE REMARKS RUN No. (DEG) -15/25 59 59 Remove T/R hub (compares to 40x80 70 BCN1QO4P4YPV2W1M1H+E Run #22) 71 11 59 Open main gear door, add T/R hub 72 59 11 Open nose gear door N. 73* 32 Remove M/R hub (compares to 40x80 11 Run #14) SIMULATED AMES 40x80 same SUPPORT 75 74 **♦ 74*** P₃ M_1 $\mathbf{x_2}$ -1.2/12SYSTEM config as #32) ◊ 75* Remove fin, same config as #35 75 BCN, QO, P, Y, V, W, M, H+ $\mathbf{x_2}$ -12/12 75 75 Remove endplates. Same config as ♦76 0 10 77* 77 Remove horiz stab. Same config as 75 REPEAT OF RUN 76. #36 78 ORIGINAL PAGE IS 75 79 REPEAT OF RUN 75 v₂ REPEAT OF RUN 74 80 74 ¥32 81* Remove horiz stab. Same config as 81 #38 127 82* Remove wing. Same config as #39 82 83 Add horizontal stab & endplates. .83* Same config as #40 84* 84 Remove fin, horiz stab & endplates Same config as #41 Add fin with 10" cap & T/R hub.
Compare with 40x80 #68 LSWT 630 v_2 82 85 #49 Add wings with retracted gear. 81 86 W_1M_1 Compare with 40x80 #69 LSWT 630 H+ Remove fin add horiz stab. Compare 75 87 with #54 R-60 Add M/R hub @ 60°. Compare with #55 88* 88 Add endplates. Compare with \$56 89 88 E Remove M/R hub. Compare with \$57 75 90 91 v_2 74 Add fin with 10" cap. Compare with **#**58 _R60 92* 92 Add M/R hub @ 60°. Compare with #59 92 Add T/R quard antenna. Compare with 93 **#**66 Add 15" fin cap. Compare with \$65 92 94 ٧,

TABLE II. CONTINUED.

TABLE II. CONTINUED.

				α	ψ	TEST	STATIC	T&I	
1	RUN No.	CONFIGURATION			RANGE (DEG)	q (PSF)	TARE	RUN	REMARKS
	95*	BCN ₁ QO ₄ P ₃ Y _P V ₂ W ₁ M ₁ H ⁺ E GT R ⁶⁰ X ₁		0	-28/28 I	83	95	6	Yaw run @ q:= 83 psf. Compare with 40x80 #30, LSWT 630 #63
	96	. x		•	V	•	95		*REMOVE BUBBLE WIRES #63
	97	X		-12/12	Ô	75 .	92	10 1	Pitch run @ 1 = 75 psf. Compare wi with #65
[98	V ₂					92		Add 10" fin cap. Compare with #66
	99						83	ł	Remoye wing. Compare with 40x80 #31 LSWT 630 #67
	100	BCN ₁ QO ₄ P ₃ Y _P V ₂ W ₁ M ₁ H ⁺ E GT R ₁ ⁶⁰ X ₂				100	100	83	Repeat 99 @ q = 100 psf. Compare with 40x80 #31 LSWT 630 #68
	101	BCN ₁ QO ₄ P ₃ Y _P V ₂ W ₁ M ₁ H ⁺ E R ₁ ⁶⁰	GXŽ	-12/12	0	75	92	10	Add wings with retracted gear open sump. Compare 40x80 \(\frac{2}{2}\)0 \(\varepsilon\) 21 LSWT 630 \(\frac{4}{6}\)9.
	102						92		Remove T/R hub. Compare to 40x80 #22 LSWT 630 #70
ы	103	M ₂	3				92		Add T/R hub @ 60° open main gear door Compare to LSWT 630 #71
128	104	N ₂					92		Open nose gear door. Compare to LSWT 630 #72
	105						74	•	Remove M/R hub 40x80 #14. Compare to LSWT 630 #73
	106	N ₁ P ₃ V ₁ M ₁ R ₁ ⁶⁰	. ***	0	-28/28	83	95	6	Repeat of LSWT 630 #96. Compare to 40x80 #30 LSWT 630 #63
	107	v ₂	-x‡	-12/12	0	75 	82	10	Repeat of LSWT 630 #85. Compare to 40x80 #68 LSWT 630 #49
	108						82		ADD NO. 50 GRIT TO REAR STRUT (TO PIPE & HOSE)
	109		TS) *2						REMOVED GRIT FROM REAR STRUT. Add grit to fuselage
	110	W ₁ M ₁	·				81.		Add wing with gear retracted. Com- pare to 40x80 #69
	1.1.1		TS) 3				81.		Add 80 grit sandpaper wingwalks. Compare to 40x80 #69
	112		TS) ₄				81		Add li0 grit sandpaper wingwalks. Compare to 40x80 #69
1	113	H H					74		Add horizontal w/o slat
r	114	E					74		Add endplates. NO GRIT ON ENDPLATES.
	115	E*	TS) ₅		•		74		E* = GRIT ON ENDPLATES

	RUN NO.	CONFIGURATION	α RANGE (DEG)	ψ RANGE (DEG)	TEST Q (PSF)	STATIC TARE	T&I RUN	REMARKS
Ī	116	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-12/12	0	75 	74	10	Remove endplates. GRIT ON HORIZ TAIL (lower 1.e.)
	117	H ¹ E (TS) ₅				74	, i	Remove grit from horiz stab. Add slat and endplates.
1	118	V ₁ R ₁ ⁶⁰ GX*	0	-28/28	83	95	6	Add 15" fin cap, M/R @ 60°, T/R guard yaw run @ q=83. Compare to 40x80 #30
	119	(TS) 7		•		95		Remove grit from l.e. of fin. Compare to 40x80 #30
	120	v_2	-12/_1	2 , 0 ·]	75	83	10	Remove wing, add fin with 10" cap Compare to 40x80 \\$31
; [121				100	-83		Repeat 120 @ 1=100 psf. Compare to :
	122	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$			7 5	92		Add wing, open fuel sumps. Compare to 40x80 \$20 & \$21
	123	P ₂				92		Add pitot tubes, windshield wipers, pilot's sliding glass window. Com- pare to 40x80 #20 & #21
	124	M_2		y		74		Open main and nose gear doors. Com- pare to 40x80 #14

 $[\]Diamond$ These runs were in error because yaw angle was not zero (actually -.79°)

^{*} Static tare measured on this run

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TABLE III. CONFIGURATION NOMENCLATURE COMPARISON

	Symbol		
LSWT 630 Test	Full Scale Test	LSWT 550 Test	Explanation
В	В	В	Smooth fuselage and tail boom
CQ 04	CQ 0 ₄	С	Prototype cowling with plugged inlets and ejectors (Q) and no screens (0_4)
E	E	E	Endplates canted 3° nose right
Fl	F ₁	Fl	Exhaust ejector fairing
G	G	G	T/R guard antenna
H	Ħ	н	NACA 0015 horizontal stabilizer (with T.E. tab) set at -7° inci-dence
H+	H+	н _ф	H plus L.E. slat
MI	. M _{I.}	MI	Main landing gear retracted with doors closed
M ₂	м ₂	M ₂	Main landing gear retracted with no doors
N _l	иТ	N _l	Nose gear retracted with doors closed
N ₂	N ₂	N ₂	Nose gear retracted with no doors
04	04		All screens closed
P ₂	^P 2	P ₂	Production protuberances: pitot tubes temp probes, windshield wipers, rotating beacons, steps, jack points, misc drain lines
P ₃	P ₃	-	Fuel sump recesses covered
P ₄	P ₄		Fuel sump recesses open
Ω	Q	Q	Fairings to cover engine inlet and plug exhaust ejectors

TABLE III. CONFIGURATION NOMENCLATURE COMPARISON (contid)

	Symbol		
LSWT 630 Test	Full Scale Test	LSWT 550 Test	Explanation
R ₁ 60	R ₁ 60	R ₁ 60	Main rotor hub, mast, controls set at 60° azimuth (fore and aft is 0°)
T.	т	T	Tail rotor hub, mast, controls set at 60° azimuth
through (TS) 7			Transition strip configurations used for 603 test. See Pictoral Configuration Nomenclature (Figure 20) for details.
v ₁	v _l	V.	Vertical fin with stinger and 15" cap (extends to WL 156)
v_2	v ₂	f.i.—	Vertical fin with stinger and 10" cap (extends to WL 151)
W ₁	W ₁	w _l	Prototype NACA 0035 wing with standard tip
x ₁	x ₁	- -	40 x 80 mount with no fairings on vertical support strut
x ₂	x ₂	1004	40 x 80 mount with both fairings
x ₃	Name		40 x 80 mount with dummy strut and no fairings
x ₃ through x ₃			Modifications to X3. See Pictoral Configuration Nomenclature (Figure 20) for details.
x ₄	-		. 40 x 80 mount with dummy strut and no fairings
x ₅	-		40 x 80 mount with dummy strut and both vertical fairings
Yı	Y ₁	-	Original prototype T/R gearbox fairing
g.	Чp	Yl	Preliminary "production" tail rotor gearbox fairing

APPENDICES

APPENDIX A - LSWT 630 Tabulated Data

This appendix contains all tabulated wind axis computer data from the LSWT 630 test. It is included in the interest of completeness and to give the report a "stand-alone" capability. There are four blocks of tabulated data. First is a set of data for all runs with all corrections except wind-on T&I's (pp A-3 to A-126). Next is a set of data for Runs 32 through 73 on the single strut mounting with all T&Is applied (pp A-127 to A-168). The third data set contains Runs 75 through 124 for the model mounted on the three-point system with wind-on support tares removed (pp A-169 to A-218). Finally, a set of data for Runs 74 through 107 is provided from which the "model alone" data of the appropriate configuration in Runs 32 through 73 is subtracted yielding T&I values for the three-point system (pp A-219 to A-252).

While most of the designations used on these forms are selfexplanatory, the following nomenclature, in order of occurrence, is provided for clarity.

TEMP	temperature, °F
PO	pressure, lb/in ²
QPSF	dynamic pressure, lb/ft2
VFPS	velocity, ft/s
RNFT	Reynolds number per foot of length, 1/ft
MACH	Mach number
TOL)	
thru }	data reduction code identifiers
T20)	• •
PNT	data point number
ALPHA	angle of attack (positive nose up), deg
PSI	yaw angle (positive nose right), deg
L/Q	lift/q (positive up), ft2
D/Q	drag/q (positive aft), ft ²
PM/Q	pitching moment/q (positive nose up), ft3
Y/Q	side force/q (positive right), ft2
RM/Q	rolling moment/q (positive right), ft3
YM/Q	yawing moment/q (positive nose right), ft3

VAUGHT LEW SPEED WIND TUNNEL TEST 630

WIND (AXES

FUN 1 1/19/81 0907 RUN 1

TEMP 84. PØ 14.4696

QPSF: \$3.00 VFPS 272.81 RNFT 1588728, MACH 0.2386

101 T02 T03 T08 T05 T06 T07 T08 T09 T10

701 0 1 0 0 0 0 0 0 0

T11: T12 T13 T14 T15 T16 T17 T18 T19 T20

PNT	.ALPHA	PSI	に/ロ	D/Q	PM/Q	YYD	RM/Q	. AW\ð
		0.01	1.566	7.229	-81.48	0.090	*2.38	+ #0.61
		2.03	1.566	7 • 169	-81+04	0.151	-1+70	0.31
		. =4.00	1.446	7.139	-79.96	-0.241	1.26	1.89
. 4		- ≖6+00	1.416	7 • 199	=79.30	.=1:193	9+04	3.38
5	7	• =8 ∗00	1.325	7 • 078	=78 + 81	≈1.428	11.59	4 * 25
<u> </u>		<u>=10.01</u>	1.325	7.048		=1.446	12.62	5.33
		.=12.00	1,325	7.018	J+79	.=1 + 657	14.68	6.22
	0.06	.=14.02	1.355	. 6.958	-72.53	-1.867	16.93	7.77
	0.06	-16-00	1.355	6.566	#66.59	-2.078	19,49	
10	1 0.06	=18+04	1.386	4 295	■61+65	=2.771	23.61	7+74
11	0+06	:=20 k02	1.506	6 • 265	=61,49	#3 · 072	25 . 82	9.75
12	0.06	=22.00	1.506	6.355	=62.73	-2.530	25.67	11.07
13	0.06	-24 -05	1.446	6.476	-63,48	.=20711	. 27.98	
	0.06	:-25.00	1.446	6.506		:=2:651	27.77	12.48
11 25	0.06	-0:01	1.717	6.747	-72.72	.=4.229	71 .03	
16	0.06	2,01	1, 596	6 * 687	#72.09	=5 · Q60	94+03	=1.87
17	0+06	3 499	1.476	6.717	=72.40	-5.452	108 87	=1.85
18	0.06	6.04	1.506	6 • 687	-70.54	=6.295	123.73	: =1 +64
19	0.06	E0.8	1,386	6 . 657	-69.45	-6,588	139.81	-0.68
20	0.06	10.00	1.536	6.175	-61.43	-5.542	117.58	-2.97
21:	0.06		1.446	6.114	-58.70	-5.422		3.22
	. 0.06	14+00	1,446	6.084	=58 • 03	-5.181	117:32	-3.52
23.	0.06	16+03	1.446	5.271	=46.98	-5.241	122.63	-0.80
24	0.05	18.00	1.446	5.392	<u>=46.22</u>	=5.482	.127 -89	1 - 47
25:	0.06		1.386	5.422	-48.75	-5 - 723	133:42	0.24
26	0.04		1.657	7.711	=78.01	-0.783	€0.95	=14.07
27	0.04		1.355	5.482	-/0:01 -47.54	-5.072	123.57	-0.18
28	0.06	25.03	1.325	5.633	=49.50	-5.271	132 • 45	1.20
29	0+06	0.01	1.596	7.018	=78.32	=3·193	49.41	=1.63

VOUGHT LOW SPEED WIND TUNNEL TEST :630

WIND AXES

FUN 2 11/19/81 0907 RUN 2

TEMP 64.

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	AMES	TYPE S	UPPORTS	BNLY	DATA'A	T C.G.	FULU	CALE D	TA
	FNT	ALPHA	PSI	٢/٩	۵\a	₽M/@	YZQ	RM/Q	. AW\d
	1	0.12	0.00	1.536	. 5,994	-67.36	=0.271	1.72	-0.88
	5	0.12		1.536	5.934	=66,62	-0.211	1.38	=0.56
	3_	- 0-12		1.476	5.964	-66.02	-0-151	0.91	-0-25
	• 4	0.12		1.416	6.054	=65+84	=0.211	1+24	0,38
	. 5	0.12	-7.98	1,355	6 • 084	=65 €62	-0:151	1.01	0.70
		4 . 11 41, 11	=10.00	1.355:	6.114	=65+94	-C.181	2.23	1.63
	. 7		-11.99	1.386	6.175	-66+09	-0.151	2.11	2.85
	8		-13.98	1,355	6 * 205	-66.55	-C.181	2.45	4.08
			=15.90	1.295	5.5994	-62.66	=C.211	2,99	4.76
	10		. =18+ 00	1.265	6+084	-64 -17	·=0.271	4.23	6 • 23
	11	0.12	.=19+95	1.265	6 . 024	≠63 ∗04	-0:181	3 - 35	6 *39
	12	. 0.12	:=22.00	1.265	6.145	=63.89	=0.060	2.02	7.46
	.13	0.12	-23.99	1.235	6.235	-65.40	0.000	2.05	8.23
	1.4	0.12	-25100	1.205	6.265	-65:97	0.030	1.72	8 • 5 4
	15	0.12	0.01	1.536	E.783	#64.50	-0.241	0+74	1.33
	16	0.12	1 +99	1.536	5.783	=64.76	=G.241	1.04	· =1 ::80
	17	0.12	4 + 00	1.506	5 • 8 4 3	F64+49	=0.301	1.75	=2.72
	18	0.12	6.00	1.506	5.873	#64.55	-0.301	1.88	-3.34
	19	. 0+12	8.00	1,416	5.964	-65.23	=0.271	1.50	-4.57
	20.		10.00	1.416	5.994	-64.93	-0.241	1+10	-5.20
기계에 되는 것이 되었다.	21	0.12	12.00	1.386	6.024	-64.96	=C.151	0.45	
ati and a state of the state of	.22.	. 0.12	13.99	1,355	6+084	=65.11	=0.090	-0.66	=7.21
	:23	0.12	15.99	1.355				-0.51	
	24	0.12	17.99		6 • 145	·=65+83	-0:120	0.56	=8+23
				1.355		-60+86	-0.241	halo bears and a man	-7.38
	25	0-12		1.325	5.843	-60.30	-0.241	0.43	. =8.00
and the second second	95		. 22.00	1.295	5 873	=59+74	-0.395	1.51	-8.31
ساوا أشتنت ومساور ومشاور والمساور والمس	27	0.12	24.02	1.205	5.873	=60.10	*0.455	2.13	-8.78
	28	0.12	24.99	1.205	5.934	-60.29	-0.482	2.64	-9.24
*	29	0.12	0.02	1.596	5 • 783	=64:57	=0.229	0.71	-1:48

		·	= Control Fo	SH SPEED		1113 mm = 15m 97	, 		
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	1	0.16	0.02	0.512	7.530	-86.48	-0.211	3.23	85.0
	, : 2		-2.00	0.512		-86.78	-0.361	5 - 25	0+54
	. i . i . 4	0.13	-5.99	0.452	7.530 7.524		=0.572 =0.594	6 *19 9*70	1.30 2.27
	5	0.16		0.392	7.410	-82+04	-1.145	11+30	3.05
	6	0.16		0.455.	7.380	w81.93	=1.295	12.30	4.45
	7			0.512	7 - 560		-0.271	3 + 53	-0.43
	8	0.16		0.512	7.560		=0+241	3.74 3.86	-0.91
	10			0.452	7.620		=0.241 =0.151	3 482	=1.98
	.11			0.512	7.590	=84+41	0.452	-0.09	-3.45
	12			0.542	7.440	■82.72	0.542	-2.69	-4.23
	13	0.16	-0.01	0.512	7.560	=86+84	=0.271	3,53	0.13
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	, , , ,		WIND:		MPE TEE			
\$	RUN . I			<u> </u>	1 0907		RUN	· · · · · · · · · · · · · · · · · · ·
		TEMP	81.			P5 14+	5580	
\$	OPSF 4 1	TO1	VFPS 2 702 703 0 1 712 713		TOS TOT 0 . 0 T16 T17	708 709 0 0	o.	2379
AME	ATYPE I	BUEPORT	e ant A	DATA	AT C.6.	FULL	SCALE D	
PNT	ALPHA	PSI	<u>_</u>	.D∖Ø	PM/Q	.A\rd	. RM/Q	. AW\0
1 2 3 · +	0.10 0.10 0.10 0.10 0.10	0.00 -2.00 -4.00 -6.01 0.00	0.452 0.482 0.482 0.422 0.452	7.711 7.681 7.651 7.741 7.801	489:31 -89:45 -89:41 -88:93 -90:10	=0:361 =0:301 =0:301 =0:964 =0:542	6 • 8 8 8 • 4 7 8 • 6 2 11 • 7 6 8 • 6 2	1.54 1.87 3.01 3.79 1.41
6 7 8 9	0.10 0.10 0.10 0.10	2:00 4:02 6:01 0:01	0.452 6.452 0.482 0.512		=89.71 =89.06 =89.10 =89.81	=0.633 -0.723 -0.633	8.95 10.22 10.26 8.90	0:49 -1:34 -1:71 1:27
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Valle	HT LOW SPEED	WIND TUNNEL	TEST 630	<u></u>	<u> </u>
	WIND:	AXES			
		11/19/81 0	907	RUN.	
	71EMP 85.		· PO . 14+	5629	
graf es			T 1590128.	MACH 0.2	378
*	701 0 1 T1# T12 T13	0 0 0	1 4 6 1 4 7 7 8	0	
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· • • • • • • • • • • • • • • • • • • •	PS% 'L/Q		DVY DVH	RM/Q	YM/Q
60.6	0.00 0.482 2.00 0.500 4.01 0.482	: 8.313 =9	4,75 0.000 5.06 =0.512 4.45 =0.602	5.20 7.23 7.74	2.79 2.79
4 0.09 m 5 0.09	6.00 0.361 0.00 0.482	8+313 =9 8+253 =9	3.89 =0.693 4.51 =0.331	8 si 13 4 u 7 1	4 * 0 8 1 * 6 9
7 , 0.09 8 ; 0.09	2.01 0.482 4.00 0.392 6.00 0.392	: 8 • 253 = 9 8 • 253 = 9	3.81 =0.361 3.16 =0.331 3.13 =0.361	4 • 7 4 5 • 7 2 5 • 6 2 5 • 6 2	0.61 . =0.48 . =1.32
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WIND AXES

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TEMP 85.

PO 14.5629

QPSF 83+00 VFPS 272+18 RNFT 1590128+ MACH 0+2378

AHE6	TYPE	WEFORTS	-ONLY	DATA	T-C+8+	FULL	SCALE DA	A
PNT	ALPHA	PSI	L/0	0/0	PM/0	Y/Q	RMOO	· YM/Q
*	0.09	0.00	0.693	8 • 133	*92.43	0.120	2+54	0.77
	0.09	-2+00	0.663	8.163	=54+21	*0+090	3.47	2.30
_ (0.09		-0.633	-8+133-	92-78	C+181		2+91
•	0.09	- m6.01	0.566	8 • 102	-91 +53	-0.301	4.46	3 • 1 0
5	0.09	-8 (02	0.512	8.102	-91.10	-0.422	5 • 25	4 • 5 9
		-10.01	0.482	8-012	-89.59	-C+301	5.37	5.90
	0.09	*11.99	0.512	7.982	#87:14	-0.361	4.99	5.78
- 1 kg - 1. 1 - 1. 1 - 3.1 H 31 H 27	0.09	-13.99	0.542	7.952	#86.28	#Q,392	5.34	6.87
	0.09	#16.00	0.633	7.319	-77.07	-C+361	4524	5.67
10	0.09	-18-00	0.753	7 • 169	=74.88	-0.422	4.71	6+60
11	0.09	-19.99	0.783	7.289	-75.59	-0.542	6 • 40	8+30
12	0.09	=21.99	0.213	7.349	-76.27	-0.253	8 63	9.70
13	0 • 69	-24.C1	0.813	7.380	#77 · 68	-0.5U4	10-19	11.09
		#25:01	0.843	7.470	*78.26	#0.554	10.98	11.72
	0.09	-0.01	0.842	8.133		C.727	¥5.07	82.0
16	0.09	2.01	0.542	8.102	=92.41	0.753	≈ 5∢32	-0-11
17	0.09	3.98	0.542	8.042	=91.57	0.693	=4 • 89	-0.73
1.8	0.09	5.98	0.542	8.072	-91.40-		-3.14	-2.11
15	0.03	7+99	0.602	7.982	#90.05	0.723	=4.91	-2.6G
žŏ	0.09	10.01	C+663	7.861	-36.03 -88.08	0.843	*6 * 36	*3 * 99
) i	0.09	12.00	0.633	7.801	-00+U0	1.094	-8.89	-5 × 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
:22:	0.09	14.00	0.602			• • • • •	-11:72	
		15.99		7.771	≈84 ¢98	1.266		-7-40
)23 49	0.09	18.00	0.572	7.259	-78.00	. 1.265	-12.69	*7. 25
	0.08		-0-663	139	-74+66-	1+476	#16.10	*9 *32
25	0.09	19.98	E44.0	7 • 229	-74.92	\$ 476	*16.96	*10.95
26	0.09		0.572	7.349	₩75 * + 1	1.596	*17+84	#12+04
22	0.03	- PARCI-	0+633	7.500	n76.58	1.627	*18.98	m13.13
28	0.09	24.99	0.633	7.560	₽77•13	1.657	-19.88	-13.77
29	0.09	0.00	0.572	8•133	=92.87	0•693	m4+71	0 •83

1 1	- i - , - , i ;;;; i , - i ; - ; i	نه پر سروان به او	(Bundal C	H SPE	D WIND T	INNEL TES	T-630	
				WIND	(AXES			
ý			4.		· .			
	iy , anang pangang pangang pangang pa	· RUN '	7		11/19/	81 0907	<u> </u>	IN - 7
			· TEMP	94.			P6 14+5629	
	,	QPSF	75.00	VFP8	260.86	RNFT 14	80378 - MACH 0	.5261
			* TO1	T02 T0	13 TO 4 TO	L TOF TOT	708 709 710	
		, , , , , , , ,	7.01 7.11	0	1 0			

AMES	TYPE	SUPPORTO	-ONLY	DATA A	T C+G+	-FULL	SCALE DA	TÁ
PNT	ALPHA	PSI	.r\d	D/Q	PM/Q	Y/Q	RM/Q	. AW\&
. 1			0.000	0.006	0.22	0,000	≈0.¢59	0.00
. 2			0.700	8+167	-=93+8+	0.433		1.29
3_			0.700	8.300	-94+64	C+233	0.79	2.01
· 4			0.733	8 + 200	=94 e20	0.067	2 .38	2 . 72
5	0.09		0,633	8 • 133	=92+34	=0.067	3,03	3 * 13
6_	all and the second second		0,533	8 100	m91.20	-0.300	4.78	4.48
7	0.09	-10.00	0.533	8 • 133	-90,91	-0.633	7.61	5 • 21
8	0.09	-12.00	0.567	8.067	-88.86	-0+633	7 186	6.41
. 9	0.09	=14.01	0.600	8.000	-87.30	-0.593	8-10	6.93
10	0.09	.=15+99	0.667	7.400	=78+25	₩0+440	020	5 ø 8 9
11	0.09	-18:02		7.367		■0 • 467	6 = 40	7.12
12	0.00	#20.00					7.58	8.32
13	0.09	-22.00		All the second of the second o		20,000,000,000,000,000	9*99	9.87
		the state of the s						11.08
15			0.400					11.61
.16								1.28
								-0.12
	, ,	,						-0.49
				the state of the s			1000	-1.99
12 1								-2.53
								-3.16
								-5.20
								-6.98
								-9.36
10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1								-9.37
								-11 · 06
								=12.05
•	7 7 7							
								=12.94
						0.333	0.61	=13.42 1.47
	13 A () Y							
	PNT 1 2 3 4 5 6 7 8 9 10 11 12 13 14	PNT ALPHA 1 0.09 2 0.09 3 0.09 4 0.09 5 0.09 6 0.09 7 0.09 10 0.09 11 0.09 12 0.09 13 0.09 14 0.09 15 0.09 16 0.09 17 0.09 18 0.09 19 0.09 20 0.09 21 0.09 22 0.09 23 0.09 24 0.09 25 0.09 26 0.09 27 0.09 28 0.09 29 0.09	PNT ALPHA PSI 1 0.09 0.02 2 0.09 0.02 3 0.09 0.00 4 0.09 0.00 5 0.09 0.00 6 0.09 0.00 8 0.09 0.00 10 0.09 0.00 11 0.09 0.00 12 0.09 0.00 13 0.09 0.00 14 0.09 0.00 15 0.09 0.00 16 0.09 0.00 17 0.09 0.00 18 0.09 0.00 19 0.09 6.01 20 0.09 8.01 21 0.09 12.01 22 0.09 12.01 23 0.09 12.01 24 0.09 12.01 25 0.09 12.01 25 0.09 12.01 26 0.09 20.01 27 0.09 24.00 28 0.09 24.00 29 0.09 25.00	1 0.09 0.02 0.000 2 0.09 0.02 0.700 3 0.09 =2.00 0.700 4 0.09 =4.03 0.733 5 0.09 =6.00 0.633 6 0.09 =3.01 0.533 7 0.09 =10.00 0.533 8 0.09 =12.00 0.567 9 0.09 =14.01 0.600 10 0.09 =15.99 0.667 11 0.09 =18.02 0.767 12 0.09 =20.00 0.833 14 0.09 =20.00 0.833 15 0.09 =24.01 0.833 16 0.09 =24.01 0.633 17 0.09 2.01 0.633 18 0.09 =25.00 0.900 16 0.09 0.00 0.633 17 0.09 2.01 0.633 20 0.09 8.01 0.733 21 0.09 10.00 0.733 22 0.09 12.01 0.633 23 0.09 14.01 0.600 24 0.09 10.00 0.733 26 0.09 20.01 0.667 27 0.09 22.02 0.600 28 0.09 24.00 0.600 29 0.09 25.00 0.600	PNT ALPHA PSI L/Q D/Q 1 0.09 0.02 0.000 0.006 2 0.09 0.02 0.700 8.200 4 0.09 2.00 0.733 8.200 5 0.09 6.00 0.633 8.133 6 0.09 10.00 0.533 8.133 8 0.09 12.00 0.567 8.067 9 0.09 14.01 0.600 8.000 10 0.09 18.02 0.767 7.367 12 0.09 18.02 0.767 7.367 12 0.09 20.00 0.833 7.467 14 0.09 22.00 0.833 7.467 15 0.09 22.00 0.833 7.467 16 0.09 0.00 0.633 8.167 17 0.09 2.01 0.633 8.200 18 0.09 25.00 0.667 8.200 20 0.09 8.01 0.633 8.200 22 0.09 12.01 0.633 8.233 21 0.09 12.01 0.633 7.867 23 0.09 12.01 0.633 7.867 24 0.09 12.01 0.633 7.867 25 0.09 12.01 0.633 7.867 26 0.09 12.01 0.633 7.867 27 0.09 24.00 0.733 8.233 28 0.09 24.00 0.600 7.533 28 0.09 24.00 0.600 7.533 28 0.09 24.00 0.600 7.533	PNT ALPHA PSI L/Q D/Q PM/Q 1 0.09 0.02 0.000 0.006 0.22 2 0.09 0.02 0.700 8.200 94.64 3 0.09 2.00 0.700 8.200 94.20 5 0.09 6.00 0.633 8.133 92.34 6 0.09 10.00 0.533 8.133 990.91 8 0.09 12.00 0.567 8.067 88.86 9 0.09 14.01 0.600 8.000 87.30 10 0.09 15.99 0.667 7.400 978.25 11 0.09 18.02 0.767 7.367 976.66 12 0.09 22.00 0.833 7.467 978.09 14 0.09 22.00 0.833 7.467 978.36 15 0.09 22.00 0.833 7.467 978.36 16 0.09 22.00 0.833 7.467 978.36 17 0.09 20.00 0.633 8.167 993.56 17 0.09 20.00 0.633 8.167 993.56 17 0.09 2.01 0.633 8.200 994.03 18 0.09 4.00 0.600 8.167 994.54 19 0.09 6.01 0.633 8.200 994.03 18 0.09 4.00 0.600 8.167 994.54 19 0.09 6.01 0.633 8.200 994.03 20 0.09 14.01 0.607 7.867 87.54 21 0.09 10.00 0.733 8.200 994.03 22 0.09 12.01 0.633 7.867 87.54 23 0.09 14.01 0.600 7.800 88.71 22 0.09 12.01 0.633 7.867 87.54 23 0.09 14.01 0.600 7.800 88.606 24 0.09 16.01 0.633 7.867 87.54 25 0.09 18.00 0.733 8.000 88.71 26 0.09 20.01 0.667 7.333 976.38 27 0.09 22.02 0.600 7.533 97.600 97.11	PNT ALPHA PSI L/Q D/Q PM/Q Y/Q 1 0.09 0.02 0.000 0.006 0.22 0.000 2 0.09 0.02 0.700 8.167 #93.84 0.433 3 0.09 =2.00 0.700 8.200 #94.64 0.233 4 0.09 =4.03 0.733 8.200 #94.20 0.067 5 0.09 =6.00 0.633 8.133 #90.91 =0.633 8 0.09 =12.00 0.567 8.067 #88.86 =0.633 8 0.09 =12.00 0.567 8.067 #88.86 =0.633 9 0.09 =14.01 0.600 8.000 #87.20 #0.459 10 0.09 =15.99 0.667 7.400 #78.25 #0.440 11 0.09 =18.02 0.767 7.367 #76.66 #0.467 12 0.09 =20.00 0.833 7.467 #78.96 =1.000 14 0.09 =22.00 0.833 7.467 #78.96 =1.000 15 0.09 =25.00 0.633 8.167 #94.54 0.567 18 0.09 \$2.01 0.633 8.200 #94.03 0.567 18 0.09 \$2.01 0.633 8.200 #94.03 0.567 18 0.09 \$2.01 0.633 8.200 #94.03 0.567 19 0.09 \$6.01 0.667 8.200 #94.03 0.567 20 0.09 \$6.01 0.667 8.200 #94.03 0.567 21 0.09 \$6.01 0.633 8.200 #94.03 0.567 22 0.09 \$6.01 0.633 8.200 #94.03 0.567 23 0.09 \$6.01 0.667 8.200 #94.03 0.567 24 0.09 \$6.01 0.667 8.200 #94.03 0.567 25 0.09 \$6.01 0.667 8.200 #94.03 0.567 26 0.09 \$6.01 0.667 8.200 #94.03 0.567 27 0.09 \$6.01 0.633 \$7.867 #87.54 0.933 28 0.09 \$14.01 0.600 7.800 #86.06 \$1.233 28 0.09 \$14.01 0.600 7.800 #86.06 \$1.233 28 0.09 \$2.001 0.667 7.333 #76.38 \$1.332 26 0.09 \$2.001 0.667 7.333 #77.16 \$1.253 27 0.003 \$2.202 0.600 7.533 #77.16 \$1.253 28 0.09 \$2.400 0.600 7.533 #77.16 \$1.253 29 0.09 \$2.000 0.633 7.600 #77.11 0.933	PNT ALPHA PSI L/Q D/Q PM/Q Y/Q RM/Q 1 0.09 0.02 0.000 0.000 0.22 0.000 m0.659 2 0.09 0.02 0.700 8.167 m93.84 0.433 m1.69 3 0.09 m2.00 0.700 8.200 m94.64 0.233 0.23 4 0.09 m4.03 0.733 8.200 m94.20 0.067 2.38 5 0.09 m3.01 0.533 8.133 m92.34 m0.067 3.03 6 0.09 m3.01 0.533 8.133 m92.34 m0.067 3.03 6 0.09 m10.00 0.567 8.067 m88.86 m0.633 7.61 8 0.09 m12.00 0.567 8.067 m88.86 m0.633 7.666 9 0.09 m15.99 0.667 7.400 m78.25 m0.440 6.10 11 0.09 m18.02 0.767 7.367 m76.66 m0.467 6.40 12 0.09 m20.00 0.800 7.367 m77.05 m0.593 8.13 0 m09 m22.00 0.833 7.467 m78.05 m0.593 9.99 14 0.09 m24.01 0.833 7.467 m78.96 m1.00 11.95 15 0.09 m25.00 0.633 8.167 m93.56 0.467 m2.41 17 0.09 2.01 0.633 8.167 m93.56 0.467 m2.41 17 0.09 2.01 0.633 8.200 m94.03 0.567 m2.41 18 0.09 6.01 0.633 8.167 m93.56 0.467 m2.41 19 0.09 6.01 0.633 8.200 m94.03 0.567 m2.41 10 0.09 12.01 0.633 8.200 m94.03 0.567 m2.49 21 0.09 6.01 0.667 8.200 m93.76 0.667 m2.41 22 0.09 8.01 0.733 8.133 m92.07 0.747 m3.94 21 0.09 12.01 0.633 7.867 m87.54 0.933 m7.08 23 0.09 12.01 0.633 7.867 m87.54 0.933 m7.08 23 0.09 12.01 0.667 8.200 m93.76 0.667 m2.79 21 0.09 18.00 0.733 8.200 m94.03 0.567 m2.79 21 0.09 18.00 0.733 8.200 m93.76 0.667 m2.79 21 0.09 18.00 0.733 8.200 m94.03 0.567 m2.79 21 0.09 18.00 0.733 8.200 m94.71 0.500 m2.10 22 0.09 18.00 0.733 8.200 m93.76 0.867 m2.79 21 0.09 18.00 0.733 8.200 m94.68 1.333 m13.92 24 0.09 16.01 0.667 7.333 m76.38 1.333 m13.92 25 0.09 26.00 0.600 7.533 m77.16 1.253 m13.92 27 0.09 22.00 0.600 7.533 m77.16 1.253 m13.92 27 0.09 24.00 0.600 7.533 m77.16 1.253 m14.00 29 0.09 25.00 0.663 7.600 m77.11 0.933 m12.76

WIND :AXES	oka 1980 Ausa milimus ayan iyo Musaka a 1995aan iyo ayaan 1900 ausa ayayaan — ayiyayad Asahii ina galaasadan qoolaasada 1900aan ahada 1900 I
<i>*</i>	
RUN : 8	19/81 0907 RUN : 8
TEMP 80.	P8 14.5629
QPSF - 75.00 VFPS 257.5	4 RNFT 1525353+ MACH 042261
QPSF - 75.00 VFP8 257.5	

موسوق و المعهد شده مي م همد بين و دين موه مدين بيده و المعارف بين بين موه أنت بين بينا ود			OF FOR I &	ONL, Y	DAIA A	T-0+0+		-	
	PNT	.ALPHA	PSI	.r\a	0/0	PM/Q	'Y/9	RM/Q	YM/Q
	: 2	0.11 -2.00		0.633 0.767	8:133 8:233 8:267	-93.90 -94.82 -94.76	0.433	-0.76 1.90 3.55	1.52 1.93 2.53
	* 5	-6.05 -7.98 -9.93	-0.02	1.200 1.500 1.733	8.500 8.500	#98 • 12 #98 • 36 #98 • 15	0.000 005.0=	4 + 60 6 + 67 9 + 67	2:37 3:56 5:52
	7 8	-12.01 -14.06	-0.05	1.933 : 2.267 : 2.367	8 · 433 8 · 400 8 · 433	=97.71 =98.54	0.000 =0.600	5 • 9 6 10 • 7 0 12 • 00	2.51 5.06 7.76
	10 11 12	2.00	-0402	0.633 0.533	8 • 167 8 • 233 8 • 167	-94+37 -94+37 -93+77	0.467	=0.83 =3.43	1 • 62 0 • 45 1 • 20
e e e	13 14		#0.02 \$0.0	0,267 0,267 0,200	8 · 133 , 8 · 100 - 5 · 033	=94.04 =93.46	0.773 0.500	. =5.88 =7.67 =5.94	1.47 0.95
		:12 • 10 · -14 • 10	*0.02 *0.02	0.167 0.133	8 • 0 6 7 7 • 8 6 7	=92 • 40 =89 • 22 =88 • 87	0.993 0000 0000	=10 ∉59 =9 €60 =8 €95	· =1 •10 · =0 •46 =0 •18
·	19	0.09		0.633	8 • 167	#93 *9 0	0+467	-0.93	1.45

YOUGHT LOW SPEED HIND TUNNEL TEST 630

WIND AXES

RUN 19 11/19/81 0907 RUN 19 ...
TEMP 77. PO. 14.5580

	PNT	ALPHA	PSI	٦.٢٧٥	D/D.	· PM/Q	.A\o	: RM/Q	. AW\O
	1	0.10	~0.02	0.767	2.600	#44×00	-C,273	4+75	1.86
	2	-1.99	=0.02	0.733	2.700	-44+84	=0.307	5 • 15 7 • 26	2.38 2.55
	. 4	-6.06	=0 <02	0.700	2.800	47 9 3	=0.407	6+34	2+84
	· 5	00.8= 30.96=		0.700 0.667	: 2.833	#47+60 #48+54	=0.467 =0.613	7+90 10+18	4 + 23 5 • 58
	7,	412.02	-0.02	0.567	2.967	-47+80	-0.5 27	7 • 80	4 * 65
		-14+07		0.500	3.067	=48,40 = -44.60	=0.740 =0.307	11.28	7.71
	10	. 1.98	=0.02	0.800	2 • 633	=44+34	=0.273	4+08	1.35
•	11. 12		=0.02 =0.02	0.867	2.533	=44+52 =42+52	=0.240 =0.167	3+84 2+38_	0.98 0.50
	13	7.94	-0.02	1.067	: 2.500	-42.47	-0.140	1.79	0.43
	14	12.10	=0.02	1.267	2 · 400	39.74 39.86	-0.107	1.88 <u>-3.37</u>	=0.06 =1.99
	. 16	.14,10	-0.02	1.267	: 2.400	:#38 • 71	0.127	=3.06	-1.45
	17 18	-14:87:		1.300	: 2.333 : 2.600	=37.78 =44.60	0:060 =0:307	=1 • 77 4 • 82	2.03

	Ok 1	ook goar		; i	;	A-12	
*		•					-
Annual transfer and the second	YSUBHT LE	W SPEED	HIND TUN	Nel Tegt	·-630		
	,	WIND:		e e e e e e e e e e e e e e e e e e e			
				····	· · · · · · · · · · · · · · · · · · ·		
	RUN 10	×	!1/19/8 1	0907		- PUN	.10
	# * * * * * * * * * * * * * * * * * * *	•	AAF SEF VA				,
	, TEMP	77.			PO 14:5	5580	
j j	QPSF 75.00	VFP8 2	56 • 87	RNFT 155	9942	MACH 0 42	261
and the second s	· 701	TO2 TO3	TO4 TOB	TO6 TO7	708 TCS	710	
	107	0 8	0.0	0 0	0 0	0	
	7 T11	712 713	T14 T15	T16 T17	718 T19	T20	
						·····	· · · · · · · · · · · · · · · · · · ·
entre più de la companie de la comp La companie de la co		e de la companya de La companya de la co	,		files and		
ADE	S-TYPE SUPPORTS	DHLY	DATA A	7 C+G+	FULL	SCALE DA	TA
FAT	'.ALPHA PSI	L/Q	'ō∕Q	PM/Q	Y/Q	. RM/Q	· YM/@
	0.11 -0.02	0.967	3.367	=45+66	-1.600	12.76	1.99
		0.967	3.433	-51+04	×1.533	12.76	2.88
		1.000	3.500 3.533	=51.81 =53.44	-1.460 -1.220	13.90	4.50 3.72
. 5		1.000	3,533	=53 +21	.=1.067	11.47	3 • 87
6	±9.93 ±0.02	0.967	3.500	-52+91	-0.933	12.90	6.29
		C.867	3.567	-52.79	-0.633	8+49	3.78
그 함께 고객들은 공기를 통 🛎	-14.03 +0.02	EE8.0	3.733	-54:07	-0.967	13.00	7.31
	0.10 -0.02	0.967	3.333	-49.09	-1.633	13.00	2.00
10		0.967	. 3∙367	49 23	≈1, •667	12.70	1 413
11		1,033	: 3.333	F0. 64 m	=1.4633	12.29	0 • 82
		1.100		=47+88	-1.600	11.00	=0.28
	7.94 -0.02	1.200	3.200	-46.07	-1+400	8 • 28	* *1 • 59
	9.94 =0.02	1.333	3.133	-45.01	-1,333		-0.97
	1211 -0.02	1.400		****	-1-000	2.88	2.75
	14:09 =0:02	1.500	: 2.867	=40+65	=1 • 167	4 462	-2.86
	14.87 =0.02	1.533	: 2.700	=39+69	=1.000	4.08	=2.53
18	0.11 -0.02	0.900	3,333	=48.75	-1.633	13.10	2.03
		•		i is fije i			

VOUGHT LOW SPEED HIND TUNNEL TEST 630

WIND :AXES

TEMP 86, PS 14.5187

OPSF 75.00 VFP8 259.36 RNFT 1505745. MACH 0.2264

0 0 11 0 0 0 0 0 0 0 0 0 0 T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

	PNT	AHPHA	PSI	「一」の	.D\0	PM/Q	ō/Y.	RM/Q	. AWA
	1	-0.03	0.01	2.200	8.033	=36,90	≖5 •700	: 29.58	:137+54
	. 2	2.01	0.01	8.167 13.233	8+100	-56+84 -74+83	-6.467	37.84	×142+29
	4	6.00	0.01	18.467	8 • 700	≈ 86 • 76	-6:300	49 173	147 .62
North Control of the	: 5	8.03	0.01	24.300	9+433	=97.40	-6.167	54.71	143+66
	6_	9.97	0.01	30.333		-119+15	-6.233	63.28	156 97
	7	12,02	0.01	36.133	11.707		.=6+847	72.29	163.15
	. 8	13.99	0.01	41.833	13.453		=6,867	78.97	-165+56
	: 9		0.01	44.620	14.413	-138+46	-6.700		158-33
	10	-0-01	0.01	1.767	8 + 100	=36+64	·=5 • 767	30.02	138+04
	11	:=2.02	0.01	:=2.900	8.200	=24.32	·=5+367	23 + 89	:132.01
	_13	#6.03	0.01	-11,967	8+567	-8.74	-4.533	7.92	:129.49
	14	-8.03	0.01	-16-167	9.067	-6.08	·# . 867	2:07	130.68
		-10.00	0.01	-20.600	.10 . 133	-4 -3-15	=5.767	-2.74	:132-49
	16	#12.03	0.01	-25.600	11.500	5+05	-6.453	-6.32	133-08
	17	=13.99	0.01	=29,633	13.013	: 20+74	=6.753	=13+14	134 • 12
	18	-15,98	0.01	#31.460	14.600	26,33	·=7.+233	=19.81	133.77
	19	=18.02	0.01	34.787	17.880	61+05	-3.567	=27:62	:123.24
	20	-20.02	0.01	-36.813	20.120	101.11	:=2.433	-29.09	121.16
	21.	10.55	0.01	-40.700	55.600	129.95	:=2.800	-32:87	:126.08
	23	-23.99	0.01	m43.680	25.820		-3.133	-39.60	124.71
	23	-25.01	0.01	=46.427	27 • 487	172.35	3-3.700	=43+36	:124+33
	24	=0.03	0.01	2.300	8 • 067	=37 . 87	i=5 • 767	30 475	:138+14
	24	-0.02	=13.98	#1.325	12.620	22.29	-34.940	131.31	271.26

VOUGHT LEW SPEED WIND TUNNEL TEST 630

WIND AXES

	. TEMP	90.		4	PO 14.5	5983	
gPSF	75+00	VFPS 2	60+14	RNFT 145	32840+	MACH 0.2263	*****
	ም ስ ቀ	****	****	106 707	mad man	" 45	

PNT ALPHA PSI L/Q D/Q PM/Q Y/Q RM/Q YM/Q	el minale
	A SHARAGES
1 0.03 0.00 1.500 8.000 m36.79 m5.967 32.94 147.66	
*2 0.03 2.02 1.733 8.033 #36.50 #2.167 27.06 135.16	,
3 0.03 4.00 1.900 8.067 -37.71 1.567 18:95 118.70	-
(4 0.03 6.08 2.000 8.467 =37.07 5.633 8.97 96.84	
5 0.03 8.00 1.633 8.600 =29.84 9.667 =1.25 71.78	
6 0.03 10.00 0.467 9.400 -15.90 13.200 -9.75 35.01	Transfer of the last
7 0.03 12.00 m0.300 10.433 m8.47 17.700 m22.54 2.42	
8 0.02 14.00 =0.833 12.000 =8.49 22.367 =34.33 =33.48	3 1
9 0.02 15.99 =0.933 13.867 =8.58 27.167 =44.53 =65.38	ويتشكوسها
10 0.02 18.00 =0.967 15.900 =8.96 38.567 =58.51 =93.14	
11 0.02 19.99 -1.667 18.100 -9.43 37.900 -69.81 -122.64	
12 0.02 22.00 -2.167 20.767 -5.36 41.300 -76.37 -145.47	
13 0.02: 23.98 0.813 25.167 49.91 46.967 480.82 4154.07	
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16 0.02 30.00 6.313 36.080 -65.78 58.133 -69.35 -206.12	
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26 0.02 -18.01 -2.733 16.667 42.40 -44.967 141.38 337.60	
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28 0.02 -22 02 -3.467 21.633 37.17 -54.367 163.50 405.46	
29 0.02 -24.01 -2.833 24.433 26.31 +58.467 168.18 438.33	
30 0.02 -26.02 -1.733 28.533 -14.89 -59.133 134.98 380.46	
31 0:02 =28:01 =1:413 32:900 =28:05 =65:433 144:05 404:05	
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VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND .AXES

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7 0.03 12.99 = 0.211 10.452 = 9.08 18:108 = 24.09 1.58 8 0.03 13.99 = 0.512 12.078 = 10.32 22.801 = 35.83 = 93.98 9					1.717		#28 · 69	10.090	-3.97		
8 0.03 13.99			0.03		0.542	9.530	-17-13	13.584	-12.32	35.56	C-SEP
9		7	0.03	1:499	*0.211	10.452	*9.08	18:108	W24+09	1.58	
10 0.03 17.99		8	0.03	13.99	WO.512	12.078	#10+32	:22.801	*35*83	**33.98	'
11 0.02 19.99		9	EO.O	15.99	-0.482	13.976	-10.87	27.771		#4.S	-
12		10	0.03	17.99	#O.663	15.910	-10.71	33.012	-59•77	-92+80	
13		11	0.02	19•99	-1.506	18.102	#9+85	37.801	=69+93	≈121·30	
14	-	12	0.05	55.05	-2,018	20.699		41.506	77.87	*144.52	No.
14		13	0 - 02	23.99	1.211	25 . 416	#17+49	47+CU6	-79.82	*152+29	
16 0.02 30.00 6.307 36.114		14	0.02	26.01		28 . 795	#24.94	51.355	-83.33	*172.58	1.
17 =0.02 =0.01		15	0.08	28-00		33+506	36.98	55,090	_82.8A	=186+77	223
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21 *0.02 *8.01 1.807 9.488 *18.76 *21.536 71.97 199.95 22 *0.02 *9.99 0.693 10.361 *4.63 *25.482 82.31 219.87 23 *0.02 *12.01 *0.470 11.536 10.96 *29.825 94.78 244.36 24 *0.02 *13.98 *1.325 12.620 26.68 *34.940 111.79 271.26 25 *0.02 *16.01 *2.229 14.367 37.58 *39.819 125.98 302.10 26 *0.02 *18.01 *2.892 16.596 42.63 *44.518 139.33 335.99 27 *0.02 *19.99 *3.795 18.795 44.86 *48.916 150.68 373.32 28 *0.02 *21.98 *3.801 21.446 38.40 *53.765 161.08 408.47 29 *0.02 *24.00 *3.102 24.247 27.53 *57.831 165.33 437.06 31 *0.02 *27.99 *1.416 32.705 *27.08 *64.789 143.32 397.94 32 *0.02 *30.00 0.392 36.301 *51.51 *67.910 135.83 415.11 33 *0.02 0.02 1.958 8.012 *38.12 *5.904 31.49 149.61		20	*0.0Z	*5,99					58 * 58	178 * 84	e.e.
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29 =0.02 =24.00 =3.102 24.247 27.53 =57.831 165.33 :437.06 31 =0.02 =27.93 =1.416 32.705 =27.08 =64.789 143.32 397.54 32 =0.02 =30.00 0.392 36.301 =51.51 =67.910 135.83 415.11 33 =0.02 0.02 1.958 8.012 =38.12 =5.504 31.49 149.61		27	=0.02	-19.99	*3.795	18.795			150.68	373.32	
29 -0.02 -24.00 -3.102 24.247 27.53 #57.831 165.33 #437.06 31 -0.02 -27.99 -1.416 32.705 -27.08 *64.789 143.32 397.94 32 -0.02 -30.00 0.392 36.301 *51.51 *67.910 135.83 415.11 33 -0.02 0.02 1.958 8.012 *38.12 *5.904 31.49 149.61		28:	=0.02	-21.98	-3.801	21.446	38.40	×53.765	161.08	408 • 47	
32 -0.02 -30.00 0.392 36.301 -51.51 -67.910 135.83 415.11 33 -0.02 0.02 1.958 8.012 -38.12 -5.904 31.49 149.61		29	-0.02	-24.00	=3.102	24.247	27.53	#57 ·831	165+33	437+06	
32 -0.02 -30.00 0.392 36.301 -51.51 -67.910 135.83 415.11 33 -0.02 0.02 1.958 8.012 -38.12 -5.904 31.49.61	P8199	31	-0.02	=27.99	-				143:32		nga.
33 -0.02 0.02 1.958 8.012 -38.12 -5.504 31.49 149.61		32	#0+02	-30.00	0.392	36.301			135 * 83	415:11	
		33	m0+02	0.02	1.958	8.012					
	****	33	0.02	0.00			140 100 770	#5 # 8 67	32.00		raes

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	ORIGIN OF PO	ial page is or quality			A-1	5]
	YEUGHT	Law SPEED	WIND TUN	INEL TEST	630		
		WIND '	AXES			•	
	UN 4		<u> *1/19/8</u> 1	- 0907		RUN.	14
	· T	EMP 91.			P5 14.5	187	
	2PSF / 75.00	VFPS 2	60+55	RNFT 148	8385•	MACH 0 42	26♠
		0 702 703 0 0 11 11 712 713	0 0	0 : 0	: 0 1 Q	O	
	RUNS DV	TA AT UPRE	GHT TRUN	VIEN-	#ULL 6¢A	LE DATA	
FNT	ALPHA PS	SI L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/@
	: 2.00 O:	01 2.233 01 7.800 01 13.400	7.733 7.700 7.973	-35,11 -53,34	-1:067 -0:900 -1:033	3 • 88 3 • 73 4 • 90	9.60 8.11 7.74
. 4	7.97	01 18.333 01 23.867 01 20.133	8 • 400 9 • 033	=82 • 72 =91 • 91	=0.867 =0.333 =0.233	4 • 65 2 • 02 1 • 71	5+24 -=0+28
7 8 8	11.99 0	01 36.267 01 41.833	11.347 13.067	#118 • 14 #125 • 68	-0.733 -0.567	3.01 3.01 3.00	6.56 6.99 6.58
11	:=2:01 0	01 2.267 01 =3.267	7 • 693 7 • 867	:=34,44	=1:067 =1:067 =0:500	3.91 3.08 1.56	. 11+10 . 12+40 - 13+28
	-6.03 O	01 =12,500 01 =16,800 01 =21.467	8.300 8.867	-5.12 2.74	=0.567 =0.967	=1.90 =3.78 =3.56	14.61 15.91 13.60
16 17	=12:03 0: =13:99 0:	01 =25.467 01 =29.933 01 =32.327	11.033 12.553	10.01 25,22	=1.893 =2.133	=3+54 =4+06 =5+53	8 • 1 1 4 • 0 6 2 • 0 2
	-18.02 0	·01 •35.013 ·01 •37.213	17.0367	60.64	-0.067	=9.90°	=0.13 0.60

24 -- 0+01

7.767 -34.28 -1.133

أك دغ معرض المنافة القوراء الشاطوة المراجعة بالغام بغورين المنافعة ويدام ستبهاجه

≈5 • 50 · **≈3 •** 76 · #6+04 · #3+21

ವರ್ಷ-೧೯ ನಿರ್ವದ ರ ಈಗ ನಿರ್ವ ಧರಕ್ಕಗಳು (೧೯೫೪) ಕರ್ನು ೧೯ ಕರ್ನಾಟಕನ್ನು ಕಂಡುಗಳು ಕು

	14		11	3 L	1.	*	ł		_	• 1					- 1	-	•	ŧ.	ı,	٠.	L,	-	نسا	۳.	1		N.		L.	 i i	۳.	•	ď.	کرن.		Ľ	ì
٠,	-	۳	•	٠,	۲	•••	٠,	•		w	_	О	7	٠.	-		-	-7	•	۲,	7	U		т	ס	T	77	Е		 \mathbf{T}	ς.	J	Г		Ţ		,

WIND AXES

TEMP 91. #5 14.5187

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DATA AT UPRIGHT TRUNNION FULL SCALE DATA TAL RUNS PNT ALPHA PSI PM/Q 'Y/Q RM/Q . AWA .F\@ D/Q 7.500 =15,96 -0+600 0+04 0:13 1 0.01 0.01 1 . 167 -0.13 -0.86 0.01 7.467 4-31.23 -0.500 2 , 1,99 6.580 0.34 0+06 0.01 -0+620 4.02 11.767 ---5-31 7.767 0 19 · =4 .07 5.98 --0・40で 0.01 17.067 8 . 167 =55 ± 67 -2.11 7.98 0 . 187 · =4 • 02 . 5 0.01 21.867 8 + 700 ×62+98 28,780 -2.34 0.033 -3+66 10.01 0:01 -86 + 45 9+633 -1.33 -1.57 -0.267 12.02 0.01 35.367 11.000 4104.08 41.800 12.933 -119.30 -2.34 14.00 0.01 0.967 · #3*70 -4.01 15.00 0.01 0.200 -0.97 **.753 -13-987 -123.72 0.01 0.440 -=0·433 -0 -27 1 . 77 10 -0.01 7,500 -12 - 89 7.733 **=0.21** 0.69 **#4.600** --O,3UÖ 11 :=2 + 05 0.01 · =2 933 -0.31 0.01 -8.000 -C+167 7+800 5.21 -1-19 0.45 9.30 -0.100 15 #6+0\$ 0.01 -13.000 8 . 133 0.98 -2030 -0.593 .14 -7.99 0.01 -17,533 8.767 11.40 **#3.62** 1+64 -10.01 0.01 -21.700 9-667 9+47 -1-100 · ≈3.18 1.57 16 412:00 0.01 -25.133 10.900 -1 - 16 #1:7:20 =3 +80 -1.833 **=0.77** 17 =14 + 02 C . 01 = 27 . 627 12.520 **≈12** #89 -3-90 -14-31 -2.063 18 -15,99 0.01 -29.440 10+833 **-7** €50 0.433 -10.34 19. -18.04 0.01 -34.133 17.000 36 . 89 : 2 . 167 -5,49 0.01 -36.320 85.52 19.440 20 -20 -01 -3.71 118+55 21 -22 -02 3.500 0.01 -10.367 21.933 · =3∗8Q · #8 +98 :22: =24.00 0:01 =44,240 : 2:067 25 - 167 153,00 m4.51 23 -25.01 1.700 0.01 -47.013 26 . 767 169 #40 --0.01 0.467 7.500

YOUGHT LOW SPEED WIND TUNNEL TEST	

WIND AXES

RUN 16 11/19/81 0907 RUN 16

TEMP 81.

PE. 14.5187

	PNT	.ALPHA	PSI	.F\d	.D/0	PM/Q	Y/Q	RM/Q	· YM/Q
	1	-0.01	0.02	-6.633	. 6,267	111+65	-0.460	.0∗03	· =0.53
	5	. 5.00	50.02	-2.900	6+000	124.81	=0+467	0.03	2.13
	3_	4.00	0.05		5.933	-137+32	-0.833	0.56	-1.57
No. of	• 🐐	6.00	0.02	· 4.400	6.000	150+23	-0.500	0+53	=2.29
	. 5	8.01	0.02	8,600	6.333	161.27	0.100	=3.51	=5+44
		10.03	0.02	13.033	6+500	169.31	-0.100	-3. 50	-5+83
	7	.11.99	0.02	18,333	7.067	175+55	-0.500	-1 ⊮65	, =1.95
	8	-14:01	0.02	23,300	7.933	183,92	-0.167	-3.17	· *3+14
	9	15.01	0.05		8+467	- 185+86	-0.067	-4.54	*4.56
	10	: 0 * 0 Z	0.02	=6 • 667	6.333	111#47	≈0.433	0 • 53	-0.17
	11.			=10.267	6 • 6 6 7	96+06	-0.400	0 + 70	0+19
	15	-4.05		-13-467	7+033	78.32	-C+167	0.51	
	13			#16,600	₹•440°	61.80	0.000	=1.50	-2.17
	14	-8.05		-19,967	: 8+067	** 46,09	-0.300	-2.99	0 . 81
		-10-02		₩23+380	9.067	29+93	-0.587	-3.79	-0.53
•		: 412 € 00	0.02		10.300	16+60	=1:700	=3 0 31	. 1.03
		=14+03		-28.433	11+787	0 • 6 9	=1.933	≈5 ∗10	=4.90
		-15.03		*38.30C	13.560	-7 • 1 1	-2.013	*6.51	<u> </u>
		-16.00	0.05		13.320	-13.15	:-2.107	-7.00	=10.66
	20	-18.07	0.02		16.113	=32.56	1.093	-11.32	=12.08
	21			-28.800	17+333	-+++75	1+967		-10.61
		H22+00	0.02		119,000	⊨55 ∗19	. 1:900	=4 +86	=8.51
		. =24 +03	0 . 02		20.767	. ≈ 65.≥25	1,500	=4 i95	-8.42
	24	-25.00	20.02	-34-227	22+347	64+61	1.767	■5 ∗67	
	25	-0.01	0.02	-6.733	6.333	110.65	-0.500	0.50	0.33
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WEUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

RUN 17 11/19/81 0907 RUN 17

. TEMP 814

: PC 14.5187

	PNT	ALPHA	PSI	. 170	D/O.	PM/Q	D\A.	RM/Q	. AW\@
	1	0.01	0.02	-6.200	6.613	109.50	;=5+633	28.08	:130+30
	,2	4 1.97	.0.02	-2.g33	6.400	119.66	-6 -100	34.44	1139 • 42
	3	3.97	0.02	0.967	6:267	134+26	-6+767	42+80	-147+33-
	. 4	6.02	0.02	4.900	6 • 400	145.55	-6+467	49407	·148 ·42
No.	5	8 + 01	0 .02	8.567	6 • 6 6 7	154,84	= 6	53.01	152 - 14
	6	9.97	20.0	13.400	7.067	162+64	-6.720	62+27	154.38
	7	:12.03	0.02	18.767	7.467	168+26	*=7 +167	70:57	161.22
	8	-14+03	0.02	23,767	8.433	175.92	-6.800	73.56	154.55
	. 9	15.04	0.02	26,000	9.013	179.81	-6.500	73.74	148+35
	10	-0.01	0.02	-6.800	6.733	106+03	i=5 . 613	27 + 28	:132+00
	-11	:=2.02	0.02	=9,900	7 + 047	93.77	=5 : 100	22.47	:124+76
	12	-4.01	0.02		7.393	76-15	-4.660	16.32	-117-25
	13	-6-00	0.02		7.800	. 59 . 81	4.387	10.11	.116 • 62
	-14			w19,400	8.500		-4+767	4.40	118.02
		-10.01		~22.933	9.500	26+52	-5.567	0.25	118.63
	16.	-11:99	0.02		10.833	10 643	=6.400	-4.79	122.98
		=14+00		=28.967	:12.433	≈5 • 45	=6.733	=12.71	:124*75
		-16.00		-29.500	13.967	-20.66	-6.520	.=20.81	122.41
	19	-18.01		=29,780	16,367	-32.36	-3.58C	-58453	113.88
		-20.00	0.02		18.033	-48-13	:-2,733	-28+20	118+04
	51	46+15+	5.00	-30.667	19.500	-55+64	-2.800	=32.83	122.84
	:22		0 1.02		21.567	=65 · 40	:=3:167	=38.33	:123.27
	:23	1.4	0.02		22.767	=65 + 45	:=3:373	-42-13	122.52
	24	-0.02	0.02		6.700	106+30	:=5.480	27.80	131.67

0.33

0.20

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	in in				i i	*****************		<u> </u>	e gan erroritation applicate
	w.t		ع شوريخوريد						4
era - marine de la marine della			GUGHT L	A SPEED	HIND TU	NNEL TES	7 (630		
				MIND.	AXES				
						× 4	Program		
									• * * *
and the state of t		RUN 1	<u> </u>	•	11/19/8	1 0907		RUN	:18
•		,	. TEM	79,		•	PO. 14+	5187	
		GPSF .	75+00	VFPS 2	57•70	RNFT 15	30627•	MACH -0 42	264
			. 701	T02 T03			708 TOS	erania de la composición dela composición de la composición de la composición de la composición dela composición dela composición dela composición de la composición de la composición dela composición de la composición dela composición d	
		<u> </u>	. 0	0 18	0 0	T06 T07	0 0	0	
			T11	· · · · · · · · · · · · · · · · · · ·	-	T16 T17		T20	
B				0 11	11 0	0 1	0 0		······································
	747	RUNS	DATA	AT MEDT	GHT TRUN		KULL:SC	ALE DATA	
والمستخط المستخط المستخطع المستخطع المستخطع		HOHO		A COMPANY	uni inon	N. O.			
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	: RM/Q	' YM/Q
	1	0.00	0.02	1.033	5.467	86 49	i=5.080	: 28.67	:130 • 50
		2.01	0.02	2.000		100,67	-5,513	34.90	:137.99
	3.			2.933		112+74	-6 - 147	43.35	145-79
	• *	6.00		4,133	5 • 400	125 • 43	-6.507	49.91	156 • 18
		10.00		6.767	5 • 6 6 7	145 • 41	=7.•353 =7. 443	71.50	1177 + 18
	. 8			8,200 9,560	a facility of the control of the con	155.93 164.46	<u>- #7.613</u> '=7.4373	77.76 81.68	179.20 174.00
	. 9	16.00		10,900	6.860	173.72	-/	82.12	157.95
	10	18.02		12.300		181.91	-6.827	83.33	-149-32
	11	0.01		0,933	5 • 467	85 • 73	=5.080	: 27.77	:129 - 40
	.12	:=2.02	0.02	£.033	5.567	71.55	4:780	. 23 • 11	125.40
	13	-4400		-0.940		<u>58+80</u>	=4+667	18+45	125.85
	14	-5.99		-1.733		41.52	·= 4 • 447	11.28	:125.60
		*8.02		.=2.500	5.767		and the second of the second o		:129 • 49
		-10-08							1135.54
		=12.03		=4,193			=5.813	×1+64	144+44
		=14+04 =16+00					≈5.800		149+12
		-18.02							<u>148 85</u> :127 38
		=20.02						A CANADA TO THE STATE OF THE ST	124+70
		-55.01			The state of the first of the first of the state of the s		The state of the s		124.98
		=24+00							:122.71
		≓25 +04							
		-0.04							

0.02 -6.733 6.333 110.40 -0.500

25 -0.01

Se de la companya de	· · · · · · · · · · · · · · · · · · ·	V8L	IGHT L	W SPEED	WIND TU	INEL TEST	· 630	other with the state of the sta	or and the second s
				WIND:		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
									And the second s
	, ,	RUN 119	<u></u>		11/19/81	0907	a a Carolina de la Carolina de	RUN	119
			TEMP	79,			PD 14.5	5187	
		GPSF 75	5.00	VFP8 25	57.70	RNFT 153	0627+	MACH OVE	264
		W	TOL	702 703	TON TOB	TO6 TO7	105 TOT	T10	Text And the second
			Ö	0 18	0 0	1 0	0 0	0	
			T11	T12 T13	节1年 〒15	The Time	T18 T19	T20	
		-7							
		#"							
	7+1.	AUNS	DATA	AT UPRIC	HT TRUM	AI ON	FULL SC	LE DATA	
	PNŢ	.ALPHA	PSI	L/Q	.D\d	PM/Q	'Y/@	RM/Q	' YM/Q
	1	-0.03	0.02	8,700	6.867	-44.22	-5.627	→ 30.58	1136.97
		2 2.00	0.02	11.833	7.4200	-67+54	-5.793	: 38.98.	
	3_	3.97	0.02	14.867	7+5+7		6.173	. 44.59	144-23
Sam o	5	6 • 02 5 • 6 • 6	0 * 02 0 * 02	18 233	7 • 867 8 • 300		.₩6±627 .₩6±987	55 • 58 . 63 • 55	.156 #39 .169 •42
	, 5	10.01	0.02	20,680		=144.68	=7.527	75 • 44	174.26
	. 7	12.03	0.02	25.927		-149+24	:=8.040	83.73	180.40
	. 8	113,99	0.02	28:347		-158.98	-7,593	91.35	.180 * 64
	. 9	15.00	0.02	29.747		=165.91	*=7.760	. 35.55	178:34
	10	;=0+0 <u>1</u>	0.02	8.567	6.933	=44+05	i=5.660	30401	:197 • 20
	11.		0 * 02	5 + 667	6.767	=21:82	=5.327	24 • 82	134 433
	12	=4.03	0.05	5.300	6+600	2+55	-5.160	16.45	132.65
	.13	-5.99	0.02	#0.580	6.500	23,16	4,987	11.25	:134+23
	14	-8.00	0.02	-4.400		-: 51.95	:=5,193	4 4 62	;139·33
		-10.01		-7.733					145-35
		-12.01		m11.600	7.533	115.67	=6+293	=3.16	151 • 11
		.=13.98		=14 - 167	8 • 400	129.76	=6 193	=10.78	155.61
		=16.01 =18.02		=16.167	9.567	134+69		=17.38 =35.77	152.31
		-20.01		#17.807 #19.400	11.567	144.15	:=2+493 =1+960		
		10.02		-50-200 -13-400	12.693 13.833	147.11			
<u></u>		=23.99		=21.773	15:207	137+94	=1.960		
		=25·05		#22,480	15.913	137 • 54	⇒1:860	=41 *55	109 • 17
		0.00	0.05						136.00

V3 0= 1		··· /	ح رثنا <u>حروج حين نشيط "ويوجي.</u>					om selver framer – Nie agent – Gyger Andre Sanflake Amstellake – 1938 (1987 – 1988)	
(·	Y8	UGHT Le	H SPEED	WIND TU	NEL TEST	4.630		
		• **		WIND A)	•		
والمستونة المستوان والمراب المستوانة المستوانة المستوانة والمستوانة والمستوانة والمستوانة والمستوانة				utus V	N 16 4	····			
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District Constitution of the Constitution of 	<u></u> - <u></u>	AUN BO	 		11/15/8				-50
			. TEMP	79+		,	PO. 14+	5187	
*.	vi. 1-19-1-10-10-10-1	QPSF ' 7	5+00	VFP8 20	7.70	RNFT 153	10627•	MACH OFE	264
			701		-			* *	
<u></u>			101	702 703 0 18	707 TOS	T06 T07	0 0	T10	*************************************
			Tir	1.0	T14 T15	T .	718 719	T20	
Harrista and Maria and Landing and Arriva a		~	g , 		-11	- 0 - 1 ·			1-1-1-14
and the second s	40.00	d tikkak	2 D	3.4	i Lisale sala 14. H	en de la companya de La companya de la co	المراجع المراج	ونسوي سوائد وال	
ىيە چى <u>ڭ سىدېلىنى سىزىكى سازىلىنىد</u> ىس ئ ىلىنىڭىنى	7+1	PUNIT	DATA	AT GPRIC	HT TRUN	NION	FULL SC	ALE DATA	
	PNT	ALPHA	PSI	L/Q	୍ ଏସ	PM/Q	Y/Q	RM/Q	YM/Q
	1	-0.03		0.833	5.067	88 • 26	-Q:167	1.35	-1.57
	. 2	: 2.03	0.02	1.867	5 100	102+85	-0,133	1+34	## # # # #
(. 4	6.05	0.02	3,933 3,933	5+133 5+167	130+26	=0.467 =0.500	2.90	3.66 3.57
Marie .	, 5	8.04	0.02	4.967	5.367	143.79	=0.433	2.96	5.43
Market Comments of the Comment of th	6	9,99	0.02	EEC.A.	5.467	155+11	-0.500	3.52	3.11
	7	:12.00	0.02	7.533	5 • 600	165+53	-0.433	· ·	-1+29
ing and the second sec	. 8	14.01	0.02	9.133	6.000	176.49	-0.133	=1.83	=3.59
	9	15.01	0.02	9,833	6.267	181-50	-0-100	m2.00	-3.71
	10 11	1 0 • 0 <u>1</u> = 1 • 9 9	0 * 02	0.900	5 100	88+09	=0+167 =0+133	1 ±35 1 +24	#0+40 =1+80
	12	3.56	20.02	=0.100 	5 • 160 5 • 167	72+48	-01133	1+00	* *1 *83 **1 *39
	13		0.02	-2.000	5 4 147	43,29	0.267	70.18	· =1 • 75
A Company	18	-8.02	0.02	-2.800	5.367		0.300		-2.58
-		-10.01	0.02	-3,633	5.633		0.000	0.33	-2.00
	-16	m11.99	0.02	=4:300	6 . 133	=9.52	₩Ø•533	2 • 28	· =0+04
		=14.01	Q •.02	=5.193	. 6 . 433	=26,58	40.500	2 • 58	1 • 45
		-16.01	0.05	-5.800	6.833		-(+167	2 • 67	0.01
A second		-18.01	0.02		8.033	-57.42	2.833		=10.90
		-20.00	0.02	-7,253	8.333		: 2.7.33		-7.71
<u> </u>		22.03	0.03	-8,233 _	8.833		2.333		1 =8.94
		. =24.03 . =25.05	0 + 02	#8.767 ~8.767	9.567		2.600	-3:12 -3:10	=9.67
	24		20.02	-9. 300 1.000	9.800		: 3.593 	=3+09 1±51	- =9.14 - =3.30
		V L	- Univ.		- 5.06/	38+09 -			
		48			¥.				
and the second and the second are the second and the second						نتريت والمستحد والمستحد والمستحد والمستحد والمستحدد والمستحدد والمستحدد والمستحد والمستحد والمستحد والمستحدد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحدد والمستحدد والمستحد والمستحد والمستحد والمس			العام والمراور والمراكز والمراور والمراور والمراور والمراور والمراور والمراور والمراور

	yazza Sanda Tapoka (1 kadan 1921-19 194 daka 1921-1944). Usak hakakat tiribi hakakat tana daka si	BEXA. GNIW	in the state of th	After the Control of
	2004 ATOMANDO BANCO DE PARTIL PARA MARIO DE PARTIL DE CONTRACTOR DE CONTRACTOR DE CONTRACTOR DE CONTRACTOR DE C	and the second s) /81 • 0907 — —	RUN 21
	TEM	es el	PO 14	++5580
The second secon	QPSF 75:00	VFPS 258.06	RNFT 1521935.	MACH 0+2261
			F 08 T06 T07 T08 T \	
and the second seco	T11	722 713 714	715 T16 T17 T18 T1	.9 T20
et anderson ger alle transit og til graden en skriver fikkel				

	PNT	ALPHA	PSI	L/Q	0/0	PM/Q	YVQ	RM/Q	YM/Q
The second secon	1	MO.05	0.01	1.500	7 . 867	81 - 18	*C:100	0+34	**+53
	2	5.03	0.01	1.933	7 • 833	94+83	#01733	0+34	*******
42 CT - 44				-2.500	7.800	107+58 -		0.30	
\. • '	4	: 5.96	-0.01	3,800	7 • 867	119.50	00000	0.90	· #3#69
	5	8•03	0.00	4.733	8 • 167	131.80	₩0•100	0+34	· #6.26
Capacita Control of the Control of t		9.99_	0.00	- 5 - 8 - 7 -	8+167	142.48-		0+59_	
	ッ	11.99	0.00	7.067	8.367	152.72	C+287	- w1+0+	· #5.39
	- 8	14.00	0.00	8.033	8.567	162.76	1.253	· #2+49	· #4+69
	<u> </u>		0.01	8.800	-8+8 <u>+</u> 7	- 167+33	1+207	×5.68	****
	10	0.00	9.01	1.200	7.867	81 608	0.113	0•49	4.50
	11	1•97	0.00	0.333	7 • 833	68.06	G•127	1 •82	= 1.94
******************************	12		0.00	-0.600	7.769		-C+C07	0.67	-1 ·27
	13	#6+04	U- 00	*1.30 0	7.800	37.46	0 + 440	#0.03	· #1.85
	14	#8 * O 1	0.00	M1.967	7 . 833		0.200	0.16	*2 * 72
C-17555-1755-175-175-175-175-175-175-175-	15.		0.00		8.067	5+45	0.162	1.99	m1.22
	16	-12.00	0+00	-3.567	8.367	-11.96	-0.300	3+34	0.51
	17	-14.01	0.02	-4.233	8.667	-26.71	*0.167	3.40	0.90
CACCOMMENTAL SECTION OF THE SECTION	18.	-15.00	0.02	-m5.033-	8.933			3,50	n0.133
	19	-18.02	0.01	~5,300	10.033	-57.98	2:720	-1.13	m11.94
	50	-19.59	0.01	-5.933	10.320	-72.29	2.767	*2.57	₩10 · 80
THE PERSON NAMED OF TAXABLE	21	REALSM	0.01			-85,58		#2.49	7.24
	:22	m24.01	0.03	-7.400	11.133	*98.66	: 2.793	*0.77	m6.37
	.23	m25.01	0.02	-8.033	11.233	-104-47	2 . 833	m1.07	. =6.98
	24	0.00	0.02	1,233	7.767	21.54.	=0.167	0.41	×1.27

A series	v		IBUGHT Le	SH SPEED	WIND TU	\\\\\\	* 630		No.	
				MIND:						
The state of the s	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				araga persak kerangkan di dan seberak keran				<u> </u>	
And the second s	и 	RUN :	12		11/19/8	1 0907		RUN	:55	
			. TEMP	90.			PO. 14+	5580		
		QP3F	75.00	VPPS 2	59.96	RNFT 14	93849•	MACH O+2	2261	
	N.		701	702 703	TO# TO5	T06 T07	TOS TUS	710		
			711	81 0 E1T 21T	0 · 0 T1# T15	0 0 T16 T17	718 T15	0 T20		
	187 187								yan ka angan yang manaka at angan yang manaka Manaka da manaka da m Manaka da manaka da m	
<u> </u>	+ I	RUNS	DATA	AT UPRI	GHT TRUN	NION .	RULL :SC.	ALE DATA		
	PNT	ALPHA	PSI	'L/Q	D/Q	PM/Q	YZQ	RMZQ	YMZQ	
	1 2	2.01 2.01	0.02	9.300	10.100	-81.58	-5 · 133	28:01 36:22 43:05	131 *33 136 • 66	
	5	8.00	E0#03	18.233 20.680	10.800 11.520	=137+39	-5.700 -5.700	50+09 58+49	137 • 20 138 • 55	
	6 7 8	14.02	0.03	23.567 25.353 27.367	13.467	=159+34 =164+75 =174+91	-5.433 -5.980 -5.433	64.58 74.653 76.57	137+31 -142+47 -147+34	
•	10 11	0.00 =1.99	E080	8.967 6.233	9 + 867	=54+83	i=5.467	28+33 : 28+34	141.20 1132.37 1127.36	
	12 13		0.03	3.167 0.067	9.433		-5.100 -4.560	16.08 9.48	125.84 127.56 132.74	
	16	=12.00 =14.00	0.03		9.367	* 71÷47 104 • 59	-5.567 -5.733	1.55 =2.34	135.03	
	18 19	-16.01 -18.00	0.05	+14.800 +16.267	13.567	125:17 130:92	EE0.5=:	=14.98 =22.70	111.62	
	21 :22	. =19:9 5 ==22:01 ==24:01	0.02	-17.433 -18.567 -19.820	16.733	127+78	-2.120	=32.13 =37.68	112.25 116.09 116.06	
May represent the second of th		. =24.96 . =0.01		-20.900 -20.300	17.367		:=2:067 -5:260		114 • 72 	

MALIGHT		L. VAID TIME	1 TEAT 420
	war die erwa	WIND TUNNE	F 1521 000
•			

WIND AXES

RUN 23 11/19/81 0907 RUN 23

TEMP 87.

Pd 14.5187

	RUNS	DATA	AT UPRIO	HT TRUN	RULL SCALE DATA			
PNT	.ALPHA	PSI	.F\d	D/Q	PM/Q	.A\đ	RM/Q	YM/Q
	0.02	.0.00	1.433	8.267	79,92	-5.100	24.71	126.10
	1.97	0.00	2.167	8 • 233	91.94	:=5.400	30+39	:128+13
- (3.98	-0.01	3.067	8+400	104+45	-5+613	38.82	130.90
4	6.01	0.01	. 4.033	8.500	114:99	· = 5 • 467	43.91	1132.77
; 5	7.98	0.01	4 - 867	8 • 7.73	126 81	=6.087	51+74	137 = 75
<u> </u>	9,99	0.01	6.100	8+800	136 + 92	-6 - 107	60.75	140.37
다른데 가는 아니일 소개를 깨길이 보다. 70	:12.00	0.01	7.133	8.933	143.80	6,233	63.88	4136 × 58
2 이 항상 10 명 - 보다 10 15 15 15 15 15 15 15 15 15 15 15 15 15	14.00	0.01	8.400	9.100	153,34	-6.700	73.90	138.53
	14.99	0.01	9,000	9.400	158-09	-6+467	75.24	1136-50
10	. 0.01	0.01	1.500	8.333	77 - 55	=5.587	26 • 67	:126 • 10
11	.=2.00	0.01	0.680	8.260	65.58	-5.300	20.45	119+10
12	#3.98 ·		-0.267	8+367	52.60	=4.733	15.19	.118.46
i i i i i i i i i i i i i i i i i i i	-6.00	0.00	-0,900	8.333	34+74	-4.613	10:12	118.93
	-7.99	0.00	-1.567	8 + 433	and the second s	-4.733	5•76	118.85
	-9.98	0.01	-2,300	8+700	0.73	-5.013	2.80	122.86
•	=11.98	0.01	=3,033	9.033	=13.27		=1.66	:126 + 07
	=14.01	0.01	-3,833 : = 3,833	9.267	=28±00	- 5.080	=6 +43	124.70
	-16.00	0.01	-4.500	9.600		-4.800	=10×68	126.50
	-18-00	0.01			-+4+05		and the same of th	T 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
and the control of th			-4.800	10.847	-58 • 16	-1.667	-20.59	
The state of the s	-19.99	0.01	-5.300	11.113	-71.91	-1.587	:=24 (72	108+04
	-23-01	0.01	-6.093	11+680	-87+07	-2+227	-30.93	115.13
	=23.98	0.01	-6.800	12.040	≈96 •04	.=2.300	=34:02	116.21
	=24.99	0.01	-7.513	12.127	=105+64	:=2 • 233	=37.68	118 • 49
54	0.05	0.01	1.500	8+467	77+91	-5-100	26.37	:125:13

YOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND :AXES

	TEMP	82	! *					PO	14.	5187		
opsr.	75+00										0.536	
	. 0	. 0	11	T04. 0 T14	· 0	: 0	Ö	0	1 0	0		
			-11	11	0	0-		0		.		

PN	T .	ALPHA	PSI	L/@	D/Q	PM/Q	'YZQ	RM/Q	, AWNO
	1	0.01	0.01	=6.167	9,633	98,58	-6.260	: 26+86	:131 •50
	2.	1.98	.0.01	-2.833	9.400	109.71	-6:460	33.10	1135.77
	3	A+05	0.01	0.900_	9 • 267	122+22	-7-127	41.82	-144+30-
	4.	6.00	0.01	4,567	9.367	:132 • 43	: =6+7 00	47 • 92	144,41
	5	8.01	0.01	8.233	9 • 7 9 3	142 + 02	-7.193	55.23	140.57
	6	10.01	0.01	13.267	10.133	148.89	=7+353	62.84	150.96
	7 .:	12.03	0.01	18.000	10.567	155.57	·=6 .773	67.66	147+40
(2) - (1) - (3) (1) - (3) - (4) - (8 -	14.00	0.01	22.367	11.467	161.14	'-7.093	74.47	141.93
	9	15.01	0.01	24.433	12+033	164+10	-7.000	76.08	141+22
1	ο .	0.02	0.01	=6.933	9 • 667	94.91	=6.007	27+94	:127 • 90
i	1 .	-2.02	0.01	=10.300	9 • 947	83,52	=5 ,493	21,439	119 435
1	2	3.98	0.02	-13.033	1C-267	66.75	4.093	15.84	114.29
	4	-8.01		#18,467	11.153	34.86	.=5.060	5,21	112+93
		10.00		-21.700	11.967	18.78	:=5,640	0.06	113.69
		11-98		-24,013	13.233	4.35		#4.78	114+83
		13.98	0.01		14.367	=11+83	=6.793	-11:07	113.81
		16.00	0.01	-27.367	15.567	=26.15	-6.993	=19.31	112.42
		17.99		-25.807	17.873	-41.49	-2.70C	m24.21	104+96
		19,99		-27,367	19.260	-52.29	-2.527	-25+06	105.65
and the second of the second o		55.03		-27.973	20.713	=62+65	-2.507	29.42	113.22
		24.01		-29.507	22.340	-70.01	-3.460	=34.71	
;2		25.00	0.00	=31,433	23.433	-71.92	-2.953	-41.55	116.87
		-0.01	0.00	=6.467	9.633	98.12	*6.013	27+94	:128+00
	4	0.02	0.01	1.500	8.467	77.90	-5.100	26.37	125.13

YOUGHT LOW SPEED WIND JUNNEY TEST 630

WIND :AXES

RUN 25 11/19/81 0907 RUN 21

TEMP 82.

· 85. 14.5089

QPSF 75.00 VFP8 258.50 RNFT 1519366. MACH 0.2265

TO1 702 703 704 705 705 707 708 709 710

O 0 16 0 0 0 0 0 0

T11 712 713 714 715 716 717 718 715 720

			•				·		
	PNT	ALPHA	PSI	.F\ d	D/Q	PM/Q	Y/Q	. RM/Q	· YM/@
	1	-0.01	0.00	~6.533	9.333	99•86	-1+040	≈0 • 59 Î	2.07
		. 2.00	0.00	-2.733 -0.900	9.033	111.96 125.57	-1.500 -1.560	-0.63 0.93	2.02
	. 4	6,03	0.00	4,600	9.067	135.48	=1.667	0147	3.02
	5	7.98	0.00	7.833	9 • 4 6 7	144+76	=1:700	0 483	-0 •72 -1 • 55
	6	10.02	0.00	12:300 17:567	9.700 10:133	155.13 160,96	-1+193 -1+193	=1416	-1.78
	8	14.00	0.01	22,033	10+900 11+533	167.33	=1.667 =1.300	1.20	*7:12 -7:27
	10	0.00	0.01	=6.867	9.367	98+56	-1.467	=0.13	=1 + 07
	11	:=2.03 :=4.00	0.01	#10.400 #13.267	9+733 10+087	85+45 69+91	=0.993 =0.467	0 (97 1 83	=0+87
	·13	-5.91	0.01	-15,667	10.133	55.46	-0.333	-0.08	. =1.44
	14 15	-8.02		#18,533 #21.933	10.667	38 • 15 22 • 76	-1.133 -1.400	-1.20 -1.37	=0.72 0.40
	16	#12.02	0.01	-24.787	13.067	3∗98	·=2 • 133	=1.020	-1.80
		=14.03 =15.93	0.01	=26.460 =27.187	13.967 15.267	=9.28 =25.97	=2.367 =2.467	=4+39 =6+06	-5.97 -7.26
	19	-18:01	0.01	-26.093	17.500	-43.00	1,353	≈6.25	•9•75
		-50.00	0.01	#26:707 #28:393	18.667	*51 • 13 *63 • 51	1.700	-4.98 -3.76	=10.48 8.78
<u></u>	22	=24.00	0.01	=29.880.	21.867	-72.71	2:007	=2:61	=6.93
	23 24		0.01 0.03		22.833	=73.20 100.42	1.800	=3 × 73 =0 • 40	=10.67 =0.77

							and the second state of the second	and the second s	Špano da ja como
Commence of the second	**			engar S	## ***********************************	* 17 1	g verskriver sær		29 4
and the state of t		YOU	JEHT LA	H-SPEED	HIND TUN	INEL TEST	630		<u> </u>
				WIND :	XES				37
						*			
		DIIN 26			11/19/81	0907		RUN	26
							அரை 4 ந. நீ	<i>,,</i>	
			TEMP	82•			月日 . 14*	0003	
		GPSF 7	5+00	VFPS 25	3 8 • 50	RNFT 15	19366+	MACH ORE	265
			o diversi				MAG TAA		
	<u> </u>		0	702 703	0 0	706 707	0 0	0	
			•	T12 T13	-	T16 T17	718 T19	₹	
			<u> </u>	0 11	11 C	-0-1	<u> </u>		
									i de de la pape 1955. Pagnara
<u> </u>	+1	RUNS	DATA_	AT UPRI	SHT TRUN	HICH.	FULL SC	ALE DATA	
p	NT	ALPHA	PSI	L/Q	.p/6	PM/Q	Y/Q	RM/Q	YM/Q
				•					
	1	0.01	0.03	1,733	10.367	-31,31	-1:667	0 + 19 0 + 45	-0.73 -0.00
	2	1,98	E0.0	7.000	10.467	=46.76 =62.62	-1.693 -2.133	3.28	0.97
	4	5.99	0 03	17.000	11,133	≈72.86	.=1.667	1+54	1.86
	5	8.01	0.03	22.067	11.800	=84.31	=1.807		0.75
	_6.	10.01	0.03	28.800		-106.86	-1:527	1.50.	1.59
	7	:12.00	0.03	35.000	-14.367		-1.333	0.74	-1.23
	8		0.03	41.000	16.200		:-2,067	-0+04	8,39
	9	15.01	0.02	*3.800			-2.007	0.48	7-90
	10	0.00	0 * 0 5	1.233	10.600	=32.32	=1.807	0.13	0 • 83
	11	:=2:01	0.02	=3,833	10.533	F19+43	-1.200	1:42	- =1.±49 4.00 ~
	12	-3.99	0.02	<u>=8,367</u>	10.833	-10+60	-0.800	-0.95	-1.93 -
	13		20.02	#12.400	10.833	그렇게 나는 하는 것도 먹는 것같아.	=0.827	×1+75	-0.32
		-7.97		#16.233	11.333	=2.26	#1.593 -1.760		
		-10.01		-50-300		-2.92 -2.80			=1.36
		-11.99	0.02		13+333				=6.47
		=14.04 =16.02		#25.367 #26.800	14.533 15.800				=3.42
		-18.02		*29.873					-5.13
는 사람이 작용했습니다. 		-20.05		*23.607					-8,18
		-22.03		-37.747					- 8.34
		. =24.01		m41.100					=10:07
		25.02		=43.933					=11+32
		0.00		1,480			-		

ಪ್ರಕರ್ಮ ಸಂಪರ್ಕ ಮೂರ್ತ ಮಾರ್ಡ್ಯ ಮಾರ್ಡ್ಯ ಪ್ರಕರ್ಮ ಪ್ರಕರ್ಮ ಪ್ರಕರ್ಣ ಪ್ರಕರಣ ಪ್ರಕರ್ಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರ್ಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರ್ಣ ಪ್ರಕರ್ಣ ಪ್ರಕರ್ಣ ಪ್ರಕರ್ಣ ಪ್ರಕರಣ ಪ್ರಕ್ಷ ಪ್ರಕ್ಷ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕರಣ ಪ್ರಕ್ಷ ಪ್ರವರ ಪ್ರಕ್ಷ ಪ್ರಕರ್ಣ ಪ್ರವಣ ಪ್ರಕರ್ಣ ಪ್ರಕರ್ಣ ಪ್ರಕರಣ ಪ್ರಕ್ಷ ಪ್ರವಣ ಪ್ರಕ್ಷ ಪ್ರವರ ಪ್ರಕರಣ ಪ್

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VOUGHT LOW SPEED WIND TUNNEL TEST 630	•
WIND :AXES	
HIND WALC	
RUN 27 11/19/81 0907	IN '27
TEMP 82. Pd 14.4990	
QPSF 75.00 VFPS 258.59 RNFT 1518851. MACH	· 8266
TOT TO2 TO3 TO4 TO6 TO5 TO7 TO8 TO9 T10	erin erin erin erin erin erin erin erin
0 0 11 0 0 0 0 0	•
T11 T12 T13 T14 T15 T16 T17 T18 T19 T20	
THE RUNS DATA AT UPREGHT TRUNNESH FULL SCALE DA	***
PNT ALPHA PSI L/Q D/Q PM/Q Y/Q RM/C	. AWNO
1 -0.01 0:02 : 2.667 10.833 -52.14 -1.967 3.	8.80
2 : 2 • 02 0 • 02 8 • 553 10 • 733 = 70 • 67 = 2 • 3 + 7	
4 5.99 0:02 18,833 11:500 =101:21 =2:167 4:	
5 8:01 0:02 23,733 12.080 =110.41 :=2:100 4:0	
6 10.01 0.02 30.600 13.167 -131.66 -1.813 5.	
7 12:01 0:02 35.533 14.547 =135.92 =1.993 4.	
, 8 ·14.06 0.02 +0.980 15.840 =150.75 \=2.467 6.	
9 14.97 0.02 43.500 17.000 -158.57 -2.167 54	
10 0.02 0.04 2.367 10.767 =51.10 =2.167 2.0 11 =2.03 0.05 =2.867 10.800 =37.27 =1.853 3.0	
11 =2.03 0.05 =2.867 10.800 =37.27 =1.853 3 12 =4.03 0.05 =7.200 10.967 =25.66 =1.507 1	
13 -8.01 0.05 -15.667 11.500 -13.86 -1.800 -1.	
-14 =10.02 0.04 =20.033 12.187 - =7.55 (=2.100 =1.	
15 -12-01 0-04 -24-400 13-567 4-50 -2-767 -1-	
16 =14.01 0.04 =27.973 14.800 19.70 =3.127 =2.	
17 =16:03 0:04 =30:227 16:220 25:82 =3:433 =5:	
18 -18 -02 0 -04 -32 -360 19 -067 62 -33 0 -340 -6 -	34 - =1.56
19 -19.92 0.04 -35,580 21.000 93.89 0.800 -5.	
20 -21.99 0.04 -38.713 23.133 118.60 1.167 -5.	
21 -24-02 0.04 -44.787 26.220 144.20 1.480 -44	
22 =24.98 0.04 =43.760 27.260 147.65 1.233 =5.	
23 0.00 0.04 2.833 10.733 =51.83 :=2.187 3.	06 10:73

A-30 "

YOUGHT LOW SPEED WIND TUNNEL TEST 1630

WIND AXES

T+1-	RUNS	DATA	AT UPRIGHT	TRUN	AIGN .	FULL :SCA	LE DATA		
PNT	ALPHA	PSI	"L/9	0/0	PM/Q	Y/•	: RM/Q	. YM/0	
	0.02	0.00	2,767 1	1.053	=53.29	=6,793	. 23.00	132.30	وتنسسنا
· 2	1.95	0.01	84333 .1	1.133	-72 .63	1=7 ± 267	. 36.35	:139 :43	
. 3 نامر	4.00	0.01		1 + 467	=91 #59	=7.633	44.19	144.08	
	6100	0.01	19.167 1	1.840	-104.39	# # ##UU	49463	148.58	
	7.99	0.01	23,533 1	2 . 667	-115.21	'-7a700	57.26	.142 .92	
	10.01	0.01			-138.60	·=7.533	64+84	-145-22	
7	:12:00	0101			m141.9%	=7.357	71+95	:151.82	
. 8	:13.91	0.01	41,200 1	6.693	=159+75	7-7.733	77+49	144:07	
9	-14-98	0,01	44.100 1	7 . 7.53	=168.44	₩7.133	77.58	-144 -00	
10	-0.01	0101	2.567	1.033	#55 · 85	1=6 , 793	29.06	134.44	
	-1,99	0.02		1.167	-40.39	-6.133	. 22.01	128.75	
	4-01	0.02		1.233	=30.29	-5.667	15.55	:125.01	* [™] × ?
. 13	=6+03	0102		0.953	=23,00	145 9667	9+28	:124.40	
14	=8.02	0 * 0 2		1.500	-=18+52	=£ . 233	3.91	:124 . 26	
15	=10:01	E0#03		2.567	=13.07	=6.767	=1.36	:126 . 87	
14	412103	-0.03		3.933	0.12	=7:167	#6+13	:123.97	
17	-13.99			5 . 167	15.64	· 7.467	-12473	124.06	
and the control of th	-16.00	0.03		6.400	20.28	-7.613	-18.21	:122 -72	Jan 18
	=18.01	0.03	and the second second second second	9.200	53,06	-4.133	.=25.60	111075	
	=22.00	0+04		23.600	117 + 44	!=2.727	-30.97	114 • 89	
.22		0+04		26 • 487	139.58	1=3 -167	=36.91	.117.73	
	-25+01	0+04		7.820	147 (27	-3.333	-41.57	119+84	
24	0.00	0.04		1 -067	-63-12	-6,467	: 28.67	132.03	81.7
24		0.01		5.200	=101.50	3,400	H42.98	=121.96	e dyr e dyr

			QF.	POOR QU	ALITY		,	7	
·	-49				· · · · · · · · · · · · · · · · · · ·	**************************************	na a sanda ng palamana a d arah sana na manganan at manna	,	; <u>1995</u>
	7					# 1			
		Y6	NGHT FE	W SPEED	WIND TUN	NEL TES	1:630	<u> </u>	
				WIND (A	VEC				
				MTHD 16	1729	4,000,000			
,			*			ė.		· •	
	É		No. 479al						
- Alice Communication of the C	<u> </u>	HUN 29			11/19/81	0907		RUN	-29
•			. TEMP	82.		•	PG 14+	990	
	***************************************		•						
		CPSF . 8	3.00	VPPS 27	72.03	RNFT 15	7805	MACH ON	2384
			704	*02 TO3	TOK TOR	T06 T07	705 Tog	. T.170	n Talendaria. Santa managan menganan
			· · · · · · · · · · · · · · · · · · ·	0 :12	0 0	0 0	0 0	Ö	
			· 111	T12 T13	T	T16 T17	Ŧ		
			<u> </u>	011-	-11 0	- 0 1	<u> </u>		
					in the second second Second Second Second	ngi disebua Maseur di Malasa		antina da Maria da Salaharan da Maria da Salaharan da Maria da Salaharan da Salaharan da Salaharan da Salahara Salaharan da Salaharan da Salaha	
	→	GUNS	DATA		in and the second		FULL 18C	ATA DATA	
and the second of the second o		HURS		AT UPRIC	HT TRUNK	12011	P. U	HE ONIA	<u> </u>
•	PNT	.ALPHA	PSI	.F\@	'D/Q	PM/Q	'Y/Q	RM/Q	' YM/Q
					_ · _				
		0.01		2.982	10.964	-52,85	-6.867	. 29.86	-144+97
		0.01	2+00	2,952	11.024	=53,26	=2.530	23+20	:129+94
		0.04		2,741	-14-235	-51.35	2-139	13.85	109-64
	- T	0.01	6.01 8.02	2,259	11.566	=46 *13	7.108	4 * 4 0	87 • 35
	· 5	0.01	10.04	1.922	11.898 12:741	#0+36 #32+38	11:434 15:452	-7+14 -14-77	: 58.23 : 25.52
	7	0.01.	12.01	*0.416	13.825	-22.58	20.572	.=29.54	9.48
	8	0.01	14:01	-1.205	15.512	-20.72	26.235	-44.55	-47 -28
	9	0.01	16.00	-1,054	17.319	-22.71	30+633	-51-63	-75+26
	10	0.01.	18 ±00	=0.422	19.096	-26+00	33 + 867	= 59∢22	-102 43
	11	0.01		=1.030	21.596	-24.55	40:030		=128 • 78
	-:12		55.00	-2.380	24.753	-14.27	44.639		-155-86
	13	The second secon	24.00	-3,355	28.036	-11.20	49,699		=186.46
	15	0.02		0,181	34.000	-22.66	56.205		-193.96
	16		30.00	3,241	38.000 41,813	=32+10 =48+99	64.759		<u>-213.39</u> -230.43
	17			2.952	11.024	=53 · 70	=7:1349	32 * 46	
	18		-2.00	2.982			=11+175	38.61	
	.19		-4.02	3.072	11.536		-14,861	44.69	and the second of the second o
	20	0.02	-5+99	2.861			#19.247	. 54+74	.181.46
	21		-6-6-	2.745	13-630	-28+64	-24+048	70.21	
	.22		-10+04	1.476	13.524		#28,373	81.62	•
	:23		=12.00	0.361	14.608		#32·651	94.66	252 • 13
	24 25		-16.00 -16.00	-0.512	15.946		#36+898		
	26		=18.00	=1.139 =1.416	17.861		#41+416 #46+795	118+79 131+23	.318 · 81 349 • 26
	27		-50-00	-2.108			451+687	142.98	384.33
	28		-21,98	=2.440	25.512		-56.765	152.63	419+33
y 100	29		-24.00	=3.024	28.855		-61.566	164.31	442.66
C C	31		-28.00	_=2 , ç,96	38 133		=69.470	143.28	
	32	170	-SUNUE	-0.271	41.735		#72°380	136.71	:426.93
	33	0.01	0.00	2,651	11:054	~52,68	.=6 • 596	28.77	143.79

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

RUN 30 11/19/81 0907 ' RUN 30

TEMP . 82.

PO 14.4990

QPSF : 75.00 VFPS 258.59 RNFT 1518851. MACH 0.2266

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

	7+1	RUNS	DATA	AT UPRIO	HT TRUNN	I EN	FULL :SC/	LE DATA	<u> </u>	- 178
	PNT	.ALPHA	PSI	'L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q	
	1	-0.05	0.00	2.833	11+100	-51 ,55	-6.447	30∉65	143.17	
	2		1.99	2.867	11.833	-52.60	:-2.067	23+34	1130 .63	
	3		4.00	2.633	11+333	-50+39	2+467	13462	107+50	
٠.	· 4	=0.01	6+04	2,433	11.833	#46+32	7.033	4.98	: 84 #5Q	
	, 5	0.00	8 +03	1.967	12.133	=39.43	11.267	=6 <02	55+57	
	6	0.00	9.99	0.933	12.867	-30,79	15.933	-17-54	: 22-17	
	. 7	0.00	12.00	-0.600	-14-033	-19 -73	21.200	-30.97	-13.67	
	8	0.00	13.99	-0.900	15.400	-19+74	26.400	42.61	-48.27	
	. 9	10-00		-0.767	17.213	-21-52	31.300	-52-65	-77+00	
	10	0 • 0 g	18 + 03	=0.767	19.300	-25 +46	35.200	=60.36	=106 • 87	
	.11	. 0.01	: 20.01	=1.433	21:+980	=23,70	39.500	-=69 + 26	#136 #25	
	12	0.01	21.99	-2,860	24.933	-15.01	44+633	-78.79	=159.92	•
	13	0.01	. 24 -00	=1.140	30.267	=16+84	51,967	-91 c32	+178.91	
	14	0.01	26.02	0.187	33.947	=23.88	56.353	=94.03	-198.01	
		0.01	27.98	1,813	27.573	-34+55	60.633	-90-93	-216.71	
	16	0.01	30+00	2.447	41.833	=50.06	64 613	-86 :72	4237.54	
	17	0.01	0.01	. 2 . 967	11.100	=52 · 68	=7.367	34.03	145 . 26	,
	18	0.01	2.00	3,127	11.300	-51.51	-11-553	40 • 84	155.80	
	19	0.04	#3.98	3.067	11,667	47:15	-14.700	47+59	170.38	
	20	0.04	-5-99	2.767	12.167		#18.527	58+24	183.97	Mark.
	21	0.04	· #8.00	2.400	12.733	, a	423.667	71.51	207.57	<u> </u>
	.22	0 • 0 4	-10:00	1,267	13,600	=13.27	#28 · Q67	82.00	:230 • 20	
	÷23	0.04	.#12.05	0.000	15.000		#32.200	94,67	258 - 16	
**************************************	24	0.04	-14-00	-0.433	16.100	•	#36+733	108.98	:287+65	
	25	0.04	-15.99	-0.967	17.933	18.49	#41.633	:121.50	318 . 78	4
	26	0.04	-17.98	-1.267	20+300		-47.093	133-10	352 - 80	
مستنيب ومسمعة والإنسان المستنيد	27	0.04	-20-00		22+833		452.000	145.85		
(28	0.04	=21.99	=2.533	25.833		#57 · 033	156 +90	422.62	
<u> </u>	29	-	=24+00	=3.200	29.227		≡62.067	167 - 99	453.71	
	30		-25:99		33,667		-63.733	141.52		
tox f	31		*27.98	=2.067	38.300		-69 - 667	145.57	416.40	
• ,	:32		-30.01	0.480	41.880		#72.300	135+50		
	33				11.133		-6.433	29.51	143.79	

YOUGHT LOW SPEED WIND TUNNEL TEST 1630

WIND :AXES

RUN 31 11/19/81 0907 RUN

* TEMP 84.

· PO 14.5334 ·

UPRIGHT ALIGNMENT RUN DATA AT UPRIV TRUNNION FULL SCALE DATA

PNT	.ALPHA	PSI	, [\ 0	D/Q	PM/Q	Y/Q	RM/Q	YMZQ
1	0.02	0.00	=2.100	11.233	55,39	6.400	32.67	=132.67
' 2	:-2.00	0.00	-7.067	11.233	74 * 16	6.700	: 39.88	=136.37
3		0.00	-12.600	11 487	91.52	6.867	46+64	-141+27
- 4	: =5 • 98	0+00	#17 833	11.867	106.76	6.800	50+59	=143.67
. 5	=8 - 01	0 • 0 0	#23,100	:12.533	121.49	6.340	56 + 06	=142 •00
6	-10.00	0.00	#29,467	13 833	141,50	5.880	61+24	*145·20
. 7	-11.99	0.00	-34,300	15.360	145.77	5.867	66+08	≈139 • 10
. 8	-13,98	0.00	#39 \$567	17.000	152+38	5.167	68.78	#133.17
9	-15-00	C-00	-42-100	17.967	-157+99	- 5.233	72-16	-135.40
10	: = 0 • 0 1	0.00	-1,433	11:433	54+79	5.167	30.71	=129 •23
11	. 1:99	0.00	3,467	11.567	41+69	5.000	25+26	=127 . 87
:12	4.00	0.00	8,300	11.833		4.580	20.69	-125·37 ·
13	5.03	0+00				5.347	15.02	-127-17
14	7.98	0.00	16.767	.12.433	~ 17.15	5.973	10.43	-127.07
15	9.99	0.00	20.967	13.200		5.733	3.69	=129.47
16	:12.01	0 0 0 0	25.600	14+040	1:11	. 6,000	=1+19	=129 • 10
17	13.99	0.00	28.200	15 + 633		7.067	=8 e02	=122.07
18	16,00	0.00		17.267		6.513	=14.47	M124+63
19	17.99	0.00				· · · · · · · · · · · · · · · · · · ·		=121.77
20	20.01	0.00			· · · · · · · · · · · · · · · · · · ·			-117.73
21	.55.05	0.00						×120+67
:22	24.02	0.00						=111 · 60
								=108×43
	-0.03	0.01	-1.367	11.447	54+63	4,667		-129.77
	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20	1 0.02 2 :=2.00 3 :=3.98 4 =5.98 5 =8.01 6 =10.00 7 =11.99 8 =13.98 9 =15.00 10 =0.01 11 1.99 12 4.00 13 6.03 14 7.98 15 9.99 16 :12,01 17 13.99 18 16.00 19 17.99 20 20.01 21 :22.02 :22 24.02 23 :25.00	1 0.02 0.00 2 :=2.00 0.00 3 :=3.98 0.00 4 =5.98 0.00 5 =8.01 0.00 6 =10.00 0.00 7 =11.99 0.00 8 =13.98 0.00 10 =0.01 0.00 11 1.99 0.00 12 4.00 0.00 13 6.03 0.00 14 7.98 0.00 15 3.99 0.00 16 :12.01 0.00 17 13.99 0.00 18 16.00 0.00 19 17.99 0.00 20 20.01 0.00 21 :22.02 0.00 22 24.02 0.00 23 25.00 0.00	1 0.02 0.00 =1.100 2 :=2.00 0.00 =7.067 3 :=3.98 0.00 =12.600 4 =5.98 0.00 =17.833 5 =8.01 0.00 =23.100 6 =10.00 0.00 =29.467 7 =11.99 0.00 =34.300 8 =13.98 0.00 =34.300 10 =0.01 0.00 =1.433 11 1.99 0.00 3.467 12 4.00 0.00 2.300 13 6.03 0.00 12.333 14 7.98 0.00 16.767 15 9.99 0.00 20.967 16 :12.01 0.00 25.600 17 13.99 0.00 20.967 16 :12.01 0.00 25.600 17 13.99 0.00 33.027 20 20.01 0.00 35.133 21 :22.02 0.00 39.273 :22 24.02 0.00 42.140 23 25.00 0.00 42.140	1 0.02 0.00 =1.100 11.233 2 :=2.00 0.00 =7.067 11.233 3 :=3.98 0.00 =12.600 11.487 4 =5.98 0.00 =17.833 11.867 5 =8.01 0.00 =23.100 12.533 6 =10.00 0.00 =29.467 13.833 7 =11.99 0.00 =34.300 15.360 8 =13.98 0.00 =34.300 15.360 9 =15.00 0.00 =42.100 17.967 10 =0.01 0.00 =1.433 11.433 11 1.99 0.00 3.467 11.567 12 4.00 0.00 3.467 11.567 12 4.00 0.00 23.33 12.000 14 7.98 0.00 16.767 12.433 15 9.99 0.00 20.967 13.200 16 :12.01 0.00 25.600 14.040 17 13.99 0.00 25.600 14.040 17 13.99 0.00 25.600 15.633 18 16.00 0.00 30.627 17.267 19 17.99 0.00 33.027 19.500 20 20.01 0.00 35.133 21.400 21 :22.02 0.00 39.273 23.900 :22 24.02 0.00 42.140 26.787 .23 25.00 0.00 44.873 28.547	1 0.02 0.00 =1.100 11.233 55.39 2 :=2.00 0.00 =7.067 11.233 74.16 3 :=3.98 0.00 =12.600 11.487 51.52 4 =5.98 0.00 =17.833 11.867 106.76 5 =8.01 0.00 =23.100 12.533 121.49 6 =10.00 0.00 =23.467 13.823 141.50 7 =11.99 0.00 =34.300 15.360 145.77 8 =13.98 0.00 =34.300 15.360 145.77 8 =13.98 0.00 =34.300 17.967 157.99 10 =0.01 0.00 =1.433 11.433 54.79 11 1.99 0.00 3.467 11.567 41.69 12 4.00 0.00 8.300 11.833 30.54 13 6.03 0.00 12.333 12.000 21.50 14 7.98 0.00 16.767 12.433 17.15 15 9.99 0.00 25.600 14.040 1.11 17 13.99 0.00 25.600 15.633 =21.95 16 :12.01 0.00 25.600 15.633 =21.95 16 :12.01 0.00 25.600 15.633 =21.95 16 :12.01 0.00 30.627 17.267 =28.27 19 17.99 0.00 33.027 19.500 =62.31 20 20.01 0.00 35.133 21.400 =89.23 21 :22.02 0.00 42.140 26.787 =124.44 23 25.00 0.00 42.140 26.787 =124.44	1 0.02 0.00 =1.100 11.233 55.39 6.400 2 :=2.00 0.00 =7.067 11.233 74.16 6.700 3 :=3.98 0.00 =12.600 11.487 91.52 6.867 4 =6.98 0.00 =17.833 11.867 106.76 6.800 5 =8.01 0.00 =23.100 12.533 121.49 6.340 6.10.00 0.00 =29.467 13.823 141.50 5.886 7 =11.99 0.00 =34.300 15.360 145.77 5.867 8 =13.98 0.00 =39.567 17.000 152.38 5.167 9 =15.00 6.00 =42.100 17.967 157.99 5.233 10 =0.01 0.00 =1.433 11.433 54.79 5.167 11 1.99 0.00 3.467 11.567 41.69 5.000 12 4.00 0.00 8.300 11.833 30.54 9.880 13 6.03 0.00 12.333 12.000 21.50 5.347 14 7.98 0.00 16.767 12.433 17.15 5.373 15 9.99 0.00 25.600 14.040 1.11 6.000 17 13.99 0.00 25.600 14.040 1.11 6.000 17 13.99 0.00 28.200 15.633 =21.95 7.067 18 16.00 0.00 28.200 15.633 =21.95 7.067 18 16.00 0.00 30.627 17.267 =28.27 6.513 17.99 0.00 33.027 19.500 =62.31 4.287 20 20.01 0.00 35.133 21.400 =89.23 2.733 21.22.02 0.00 42.140 26.787 =124.44 1.567 23 .25.00 0.00 44.873 28.547 =135.65 2.267	1 0.02 0.00 =1.100 11.233 35.39 6.400 32.67 12:=2.00 0.00 =7.067 11.233 74.16 5.700 39.88 13:=3.98 0.00 =12.600 11.487 51.52 6.867 46.64 4 =5.98 0.00 =17.833 11.867 106.76 6.800 50.59 5 =8.01 0.00 =23.100 12.533 121.49 6.340 56.06 6 =10.00 0.00 =29.467 13.833 141.50 5.880 61.24 7 =11.99 0.00 =34.300 15.360 145.77 5.867 66.08 8 =13.98 0.50 =39.567 17.000 152.38 5.167 68.78 9 =15.00 6.00 =42.100 17.967 157.99 5.233 72.16 10 =0.01 0.00 =1.433 11.433 54.79 5.167 30.71 11 1.99 0.00 3.467 11.567 41.69 5.000 25.26 12 4.00 0.00 8.300 11.833 30.54 4.880 20.69 13 6.03 0.00 12.333 12.000 21.50 5.347 15.02 14 7.98 0.00 16.767 12.433 17.15 5.973 10.43 15 3.99 0.00 28.200 15.633 =21.95 7.067 =8.02 18 16.00 0.00 28.200 15.633 =21.95 7.067 =8.02 18 16.00 0.00 30.627 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 33.027 17.267 =28.27 6.513 =14.47 19 17.99 0.00 35.133 21.400 =89.23 2.733 =21.66

VOUGHT LAW SPEED WIND TUNNEL TEST 630

WIND AXES

		n 4 M P	A / 1 · 1 · 1				
RUN			11/19/8	1 0907	and the second section of the second	: RUN :32	\$ 200 200 200 200 200 200 200 200 200 20
	· TEM	P 94•			PØ. 14.5	5187	
o PS			61.26 TO# TO5			MACH 0+2364	### ### ### ##########################
<u> </u>	Ò	0 :32 T12 T13		Q 0	0 , 0	Q	
SINGLE	SUPPORT DA			Ar Cogo	IEUL L	SCALE DATA	
PNT .AL	PHA PSI	·L/Q	D/Q	PM/Q	Y/Q .	RM/Q 'Y	M/Q

		• •	•					
PNT	.ALPHA	PSI	.L/B	D/Q	PM/Q	Y/9 .	RM/Q	' YM/Q
**************************************	0.03	0.00	-2,667	8.867	47.78		21.25	
		0.00	=9.333	8.900	69.36	5.600		€153 €87
	-4.00		-15.367	9,227	92.74	5.747		*154.94
	=6.00	0.00	=21,867	10 + 100	112.75	5 473	40 • 29	
. 5	: ≍8 • 0 0	0 0 0 0	#26.800	11 • 167	124.22	5 • 633	46.78	
	≈10.00	0 + 00	=30.633 .	12.700	105.47	6.733	55+54	=163.72
7	w12.01	0+00	=36.800	.14.293	112.48	7,613	66-19	-172+50
	-14.00	0.00	#42.307	16.100	122.76	6.887	69.09	-160-79
9	-14,99	0.00	-44.967	17.200	128 - 85	. 6.933	75.39	=164.03
10	0.00	0,00	-2.500	8 • 527	46 . 71	5 . 673	. 22.03	-152.33
11	2.03	0.00	2,967	8 + 567	35 + 33	5.460	15.88	-150 - 17
:12	3.99	0.00	7,633	8 • 600	26 + 80	5.200	10.57	
13:	5.99	0.00	12,067	8.800	20.78	3 5.200	4 • 15	=140+34
	7.99	0.00	16.333	9.233	22.70	5,493	-2.30	
15		0700	21.167	9.867		5.767		=132.68
والمستحد والمرابط والمراجع والمراجع والمنافع والمستحدد والمستحد والمراجع والمراجع والمنافع والمراجع والمستحدد	:12,04	0.00	25 4 6 6 7	10.833	23,99	5.700	=15 +83	
17	13.99	0.00	28:160	12.560	4+68	6.567	=25.66	
18	16.01	0.00	31.340	14.093	5.74			=118 • 64
19	18.00		35.340	16.300	-19.94		-33+29	
50		0.00	37.660	The state of the s	-52.65			-127.01
<u> Zi</u>	21.99		40-640	21.200		5,307		=136.18
22		0.00	44.107	24 320	=90.86	5.833	=47 .52	
23	24.99	0 + 0 0	46.800	25.993	*96 • 85		=54 +10	
24		0 + 0 0	=2.333	8.600	48.69	5.360		=151.62
4 1	- 5 1 0 5		-6.333	B • 6 U U	- 70107	31300		TATOR

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YOUGHT LAW SPEED WIND TUNNEL TEST 630

WIND AXES

RUN 33 11/19/81 0907 RUN 33 PO 14.5187 PO 1505745. MACH 0-2264

TOT TOZ TO3 TO4 TO5 TO6 TO7 TO8 TO5 T10

O O 33 O O O O O O O

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

O O 32 32 O O 1 O O 1

	BING	LE SUP	ORT DAT	À	DATA	LT C.G.	FULL	SCALE D	ATA
	PNT	ALPHA	,psī	Ĺ/Q	D/Q	PM/Q	Y/Q	RM/Q	. ለዛ\ <i>ፅ</i>
	1	0.91	0.01	=2.733	8.567	49.27	6.320	24+23	≈161•79
	2	0.01	-2.01	:=2.767	8 - 627		1+967		-139×43
	: 3		*4.01	=2.667	8.767	50.53	:=2.567		=112.00
	- 4	0.01	· =6.00	-2.300	9.067	46 - 17	=7.067	. 22.70	=94.68
	. 5	0.01	= 7.₽99	×1, ±567	9.700	39 . 28	m11.527	20.08	=66,43
	6	0.01	· =9.99	=0.467	10.540	31.22	m16.393	17:15	
	7	0.01	-12+00	0.800	12.033	: 21.06	▶21.9 00	55.38	≈1 0 • 75
	8		-13.99	1.500	13,600		#27.033		1 21.20
	9		-15.99	3.100	15.333		.31.733		
	10	0.01	-17.98	5,000	17:447	-1.58	#36 + 933	13,27	. 84 - 19
	11		€Q.0S=.	7.433	20 - 100	=15.26		11.20	124 : 42
	12		:=22.00	3.767	23.200		#47.4467	7.36	
	13		-23.99	12.700	26.633			range, and the same and the same and the	
	-14		26.01	15.667		75.77		-0.20	the form the state of the state
도본 등 등록하는 경우 등록 기급을 통합하는 기계 기계 기계 등록 기급을 통합하는 기계	15		:=28:01	18.240			#61.273		
Titalian in the state of the st	16		·*30.02	19,647	37.100	=100+72	#64+580	3.36	:228 *53
	17	0.01	0.00	-2,400	8 • 633	48.18	6.993	: 21.98	
	18	0.01	2.00	=2.700	8.767	48.51	11.067	. 22 49	
	19	0.01	3.99	-2.667			14,580		-193·10
	20	0.01		-2.420	9.660				-196.28
	21	0.01	7.99		10.367				-206-16
مسيد في پيرون دو مختاف مصوم و محت آخر بين مي آخر ي آخري آخري آخري آخري آخري آخري آخري المجترف و محتود و محتود و	:22	0.01	10.00	≈0,500	11.200	8,96	25.767		
	23	0.01	11.99	0.667	12:467		30,200		=246+64
	24	0.01	13.98	1,800	14.333	=10.21	35.267		=266.94
	25	9.03	15.99	3.300	-13+153		40.767		=298·61
	26	0.01	17.99	5,133		The state of the s	45,600		=328+58
- 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	27		: 20.02	7.233	20.800				÷372∙95
	28	0.01	55.00	9,533	23.567	=72.32	56.907		=416+14
i	29		: 23+98	11.347	26 + 833		61.900		=443 * 67
,	30	0.01	26+00	13.053	30.333	-87·41	67.100		*475 * 03
and the same of th	31	0.01	28:01	13.647	35.420	=99·18			=403·60
· · · · · · · · · · · · · · · · · · ·	35	0.01	30.01						
ut.	33			14,060	38.913	-67.54			-404-48
الم المعاونية والمستوافقة والمستوافقا والمستوافقة والمستوافقة والمستوافقة والمستوافقا والمستوافقا وال	.53	0.01	0.00	-2.167	8 • 567	49-42	<u> </u>	27=18	-162.61

ORIGINAL PACE IS OF POOR QUALITY

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VOUGHT LOW SPEED WIND TUNNEL TEST	53	3	ļ	ţ	ţ	ţ	ţ	į	į		i	į	ì	:	3	;	,	Ĺ	Į.	Į.	į	į	Ĺ	į	į		į	į	Ŀ	į	Ĺ	į	Ĺ	Ĺ	į	Ĺ)	è.	è	ż	ż	ż	į	ĺ	ĺ	Í	į	i		٠		_	:	Ľ	Ì	Ž	ì	ė	ź	3	ċ	÷	F	_	ľ]	_	_		i		_	Ĺ			Ł	j	l	Š	1	1	h	ŀ	1	١	ľ	1	7	-		2	ľ	ĺ	h	ı	E	7	l	k	١				2	Ĺ		٠	ľ		ž	E	1	2	F	į	ì	8	ŝ				Ė.	Ė	è	ì	j	1	ð	ŧ				Ļ	Ļ	į					Ĺ	Į.	1	ſ.	ı	١	Н
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RUN 34	9		11/19/	E1 090		A STATE OF THE STA	RUN 34	A
•	TEMP	86.			· PB. 14	.5187		
gPeF : 83∢		ar e i			1584019. 17 708 TO	A. William	0.42382	
	() Q	0 33 12 T13	, Q	0 0	0 0 17 718 T1 1 0	0 0		<u> </u>

	BING	LE SUP	CRT DAT		DATA	AT C.G.	FULL	SCALE D	TA
	PNT	.ALPHA	PSI	'L/Q	'D/Q	PM/Q	PVY.	RM/Q	· YM/Q
	1	0.02	0.01	-2,651	8.452	∤8+23	6.199	24167	4162.35
	. 2	0.02	=1.99	-2.651	8.584	49 441	1.259		-133.63
	3		4.00	-2.651	8.765	48+05	:=3.289		=108.53
	4	0.02	. =6+00	=2.199	9 4 1 5 7	42+74	'=7 +777	24+04	-90.09
•	. 5	0.02	. =8 ; 07	二主。4 440	9.759	36+80	#12.506	21.38	=62 • 15
	6		=10.00	=0.422.	10.572	29.29	#17.0265	18 * 10	=32.56
	7	2010	.=12.00	0.873	:12.169	18 - 58	M22,657	15,57	-7.74
	8	0.02	~13 599	1,928	13.705	14+55		14.70	* 24 • 55
용하다 가 됐다. 내 기계를 보였다.	. 9	0.02	-15,99	3,223	15.452		#32 · 416	15.06	. 53.30
	10	0.08	#17 ₽99	4,970	17.470	-2:32	#37:325	13.59	85.91
_	11	0.02	:-20:00	7.470	20.120	#13+89		12+70	.124 • 22
·	:12	0.02	=22.02	10.000	23 • 259	=33 - 85		7 * 65	162.52 -
	13	0.02	-23+99	12.651	26.657		H52 . 566	2.90	194.40
	14		-26.02	15,030			*57.054	2-13	.211 * 57
	15		-28.02	18.042			#61 . 030		.216.05
	16		-30.00	19,012	37.018	=98+1 4		6.28	
	17.		0 400	=3.012	8 • 614	44+71	6.620		=163+64
	18	0.02		=3.012	8.765	44.46			=177.43
	:19	0.02		-2,982		38.38			=190×13
그렇게 하셨습니다 그 없이다	20	0.02		-2.831	9.669	30.45			-194+14
	21	0.02		-2.199	10.241	19.93			=203.82
Eq.,	:22	0.02	9.98	=1.114	11.175	8+45			=219:32
	23	0.02		0,030	12+410	#1+83	29.723		-242.02
	24	0.02	13.99	1,054	14.187	=2 ± 40			=261.77
	25	0.02		2.934	16.054	¤21 ∗42		32.96	=295.63
	26	0.02	17.99	4.608	18.012	-34.72			=324+03
	27	0.05	19.99	6,476	20.398	-51.05			-367.50
	28	0.05							
<i>(</i> **	29	0.02		8 765	23.253	=68:22		42*13	
,				8.705	23.217	≈67+49	56,199		
-	30 31	0.02		11.265	26.536	=85.17	61 (337		M441.78
		0.05		12.916	30.060				
	32	0.05		13.102	35 • 247				
	33	0.02	. 29.99	13.590	38,657	≈66 • 23	70 + 187	M 5 + 3 4	=406+66

WIND AXES

RUN 35

TEMP 68.

RUN 35

TEMP 68.

RUN 35

TOTAL TOTA

	SING	LE SUPP	ORT DAY	<u> </u>	DATA A	T C.G.	FULL	SCALE DA	IA.
	PNT	ALPHA	:PSI	.F\6	.D/6	PM/Q	O\Y'	RM/Q	. AW\0
	1	0.00	*0.01	-2.467	8.100	43.D2	0.567	0 +55	*10+35
	2	:-2+01	=0.01	*8.867	8.300	62.52	0.733	1.73	*10.32
	3	m4+02		*15.233	8.767	88.54	1:067	3.20	*13.82
41.41.41.41.41.41.41.41.41.41.41.41.41.4	. 4	-6.02	=0.01	#21.533	9.533	109+12	. 1:300	3+64	≈14.50
••	: 5	-8.01		#27.433	10.600	123.86	1.373	4 .62	≈16∗08
	6	m10.01		=31.413 .	12.100	118.03	1.767	4.03	=18+64
COLUMN TO THE PARTY OF THE PART	7	The state of the s		**36 * 867	13.900	111.73	1.567	6+34	*16+82
	8	-14.01		×42.533	15.800	122+70	9.500	6.48	.*11.50
	9			*45,220	16.947	127+18	0.713	6 • 45	*11*50
encontracted trackers in a second sec	10	-0.01		-2.500	8 • 133	42,95	0.767	0 + 58	-11.26
	11	: 2.01	-0.01	3.267	8.133	: 31+12	0.567	· =0 < 12	=13.67
	12	. 4.01	-0.01	7.767	8.233	22.42	. 0.433	-1.03	=13.64 -
	13		mO+01	12.333	8.367	16+33	0,567	-2.64	w15.22
	1.4		#0.01	16.733	8.813	17:10	C+733	-3.90	-15 *07
	15		-0.01		9.567	18.16	0:900	~5+05	#14 *66
CONTRACTOR OF THE PROPERTY OF	.16	:12+00		26.040	10.133	19.23	0.633	=5:83	*9.29
	17	14.03		28.767	:12.233	1.26	1.433	-9492	· =1 415
	18			31.607	13.600	2.54	2 . 433	-13.52	· =3.43
	19		-0.01	34.153	16.060	-28.50	1.347	#10+94	**8*92
	50		-0.01	37.540	18 • 433	#54*18	0.120	m5+89	. =9.55
	51		mO.Q1	40.447	21.140	·074.93	#C +567	m4 x 1.1	*12.52
ares from the manual classic of the second s	.22		mOeO1		24.020	-88.78	0.433	-8.10	.=10:39
	23		-0.01		26.233	-96.81	1.263	-12-63	≈11 a 10
	24				8 • 1/33	43.05	0.567	0.02	-11.15

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OF	POOR	OUALI	TY

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YOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND :AXES

0 0 32 32 0 0 1 0 0 0

SIN	QLE SUPP	ORT DA	A	DATA 'A	T C.A.	FULL	SCALE DA	<u> </u>
FNT	ALPHA	PSI	L/Q	DIA	PM/Q	~ Y/Q	RM/Q	YM/Q
1	0.01	-0.01	-1.333	7.900	28.05	. 0.080	-2.71	1.09
사람들이 얼마나를 잃었다. 밝숙	ere in the property of the first term of the contract of the c	-0.01	-7,933	8.200	+5 +45	0,353	-2.44	0+04
3			-14.033	8 • 600	63.44	0.913	= 1.01	-++94
4	= 5.99 ·	=0.01	=19.700	9,267	64+16	1 + 047	≠0 •53	-6.26
5	:=8.03	=0.01	#24.400	10.700	82.50	1.213	0 #09	· ≈7.58
6	w10+00 ·	=0.01	=29.533	12.013	86 • 26.	1.384	0.91	=7 * 82
7	-12.01	-0.01	x/35.500	.13.500		1.080	0.53	4 =4+80
- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	-13,99			15.527	107+48	. 0.347	0.23	1 - 17
			-44.667	14.840	116.87		. 0.60	1 . 87
10		=0.01	=1,433	7.900	. 58 . 10.	0.180	E+43	0.70 -
11	: 2.02	=0.01	4.000	7.967	19.25	-0.020		2.17
:12				8.000		≈ 0.253	· w1 .38	1.83
13		-0.01				-0.187	-1.65	
				8.567		0.047	-3.18	0.33
			21,233		18.98	A CONTRACTOR OF THE STATE OF TH	The state of the second state of the	
16		=0.01	24,800	10.233	37.16	. 0.367	- ≥5.06	0415
17		#0.01	26.033	11.907	42.28	1.247	. =6.75	8.77
18		=0.01	28.993	13.213	45.58	1.987	×8+29	4 • 86
19		-0.01	32.893	15.680	=8+64	1.327		
20		-0.01		18.273	-40.88	-0,420	-1.34	
		A CONTRACTOR OF THE STATE OF TH	39,727	20:813	-63.28	-0.653	0.82	· -S-06
.22		=0.01	43,520	23.767	×84.82	0.047	· m1.38	2.05
;23		=0 e Q1	47 • 100	25.860	=32+88	0.813	= 5∗33	1 • 65
.24		=0.01	=1.667	7 • 867	30 +53	0 + 0 4 7	=2.56	1.15

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YOUGHT LOW SPEED WIND TUNNEL TEST 630

	· RUN:	·37			11/	30/81	0849		2	RUN	<i>'</i> 37	
			TEMP	80				PO	14-6464			
-	GPSI	75.	00	YFP	s 256.8	1	RNFT 15	33731	• MAC	H 0 % 2	254	
		*	TOT	T02	T03 T04	T-05	T06 T07	BOT	TOS T10			5. s
10 (10) (4) (4) (10)	W. E.		Ţ1‡			T15			T19 T20	of the second second		

SINGLE SUPPORT .DA	ra da	TA AT C.G.	FUL.	SCALE DATA)
PNT ALPHA PET	.F\d .0	/Q PM/Q°	'Y/6	RH/Q '	YM/Q
T =0.01 -0.01	7.467 6	667 =107.82	09107	-1.99	1+19
: 2 .=1¥98 + ≠0¥01	3.500 : 6	500 =127.77	0.433	=2.09	-1.31
: 3 →WA € 00 + HO € 01	-0.033 . 6	467 =145+49	0.900	#2.36 ×	=5.05
*	·-3.933 6	733 -163-27	0.993	-1.89	-4.77
5 1-8.000.01	-7,700 7.	133 -180.38	. 1 . 100	-1.76	-5.8Q
6 =9.99 =0.01	m12.039 · 7.	767 -194+63	. 1.233	-1.89 .	-5.00
7 412:00 40:01		533 =203,21	1.013	#1×73 ·	-4.71
8 =13.99 =0.01	#21.567 9	700 =214+04	1 0:287	=1√89 •	=0.51
: 9 #15:00 · #0:01	#23.500 -10	433 =218.71	. 0.100	-1+25	1,62
10.000	7.433 . 6	600 =107.25	E1210	#1.688	0.38
11 : 2.01 : =0.01	10.933 6	867 -86.16	-0.067	· =1.13	0.58
12 4.02 =0.01	13.867 7	087 -66.42	-0.267	-0.87	0.98
13 5.99 =0.01		5,00 =47.61	=0.267	=1.55	1.13
14 : 8 • 00 · = 0 • 01	19.767 8	000 -=28+00	0.000	-2.63	=0.50
15 10:00 #0:01	22,900 : 8	700 - =6:10	0.500	≠5 ∗49 .	=1.74
16 :12:00 =0:01	26.200 9	7/10 15.59	0,633	#5 e 6 6	-0.69
17. 13.99 -0.01	26.827 11	300 33.50	1.520	13.27	8 . 65
18 16.01 -0.01		780 49.54	: 2:153	-13.88	6.88
19. 18.02 =0.01		593 64.93	0.700	=5472	=0.35
20 20 02 =0 01		447 76.76	-0.700	-2.64	-0.24
21 :22 : 02 : =0 : 01		960 88 89	-0.733	-1-19	-2 - 44
22: 24.00 #0.01		967 100.68	-9:167	-1441	0.43
23 25.00 -0.01		233 104.95	0.700	-6432	1.32
-24 =6.01 =0.01		667 -107-29	. 0.100	-1-89	0.28

WIND (AXES

PNT .ALPHA PSI L/Q D/Q PM/Q Y/Q RM/Q YM/Q 1		SINC	LE SUPR	ORT DA		DATA	T 0.0.	FULL	SCALE DA	TA
2		PNT	ALPHA	Paï	٦/٥.	۵/۵.	PM/Q	Y/Q	RM/Q	* YM/Q
3 ; -3 · 5 · 6 · 0 · 0 1		1								
4 =5.99 = 0.01 =3.933	print to the second									
5		. 4								
7 =11.99 = 0.01 =17.100 = 9.033 =196.65		5	.=8.02 ·	=0.01				7.+240	45 - 17	=164+38
**************************************		6	-9.99	=0.01	=12,100.	8.267	=189.01	7.720	53 * 13	=170•30
10. 0.00 =0.01 7,433 7.133 =102.37 5.967 19.37 =148.10 11 : 2.00 =0.01 10.800 7.433 =82.88 5.367 14.09 =140.26 12 3.99 =0.01 13.433 7.700 =65.14 4.893 9.55 =132.67 - 13 6.01 =0.01 16.600 8.033 =44.40 4.407 3.32 =128.47 14 8.01 =0.01 19.733 8.433 =24.38 4.667 =3.29 =120.76 15 10.00 =0.01 22.767 9.167 =4.54 5.067 =9.77 =119.29 16 :22.01 =0.01 25.833 10.100 16.41 5.200 =16.03 =119.05. 17 :13.99 =0.01 26.520 11.767 34.72 6.100 =27.43 =111.11 18 15.99 =0.01 28.667 13.167 50.78 6.633 =34.14 =109.18 19 18.00 =0.01 28.973 16.647 74.35 3.967 =30.78 =122.02 21 :22.02 =0.01 30.240 18.407 \$7.86 4.027 =34.55 =128.93 22 :24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52		7				9.033	-196.65	7.567		
10. 0.00 =0.01 7.433 7.133 =102.37 5.967 19.37 =148.10 11 2.000 =0.01 10.800 7.433 =82.88 5.367 14.09 =140.26 12 3.99 =0.01 13.433 7.700 =65.14		, 🛊				.10.200	-205.97	6.847		
11 : 2000 =0.01 10.800 7.433 =82.88 5.367 14.09 =140.26 12 3.99 =0.01 13.433 7.700 =65.14 4.893 9.55 =132.67 - 13 6.01 =0.01 16.600 8.033 =44.40 4.407 3.32 =128.47 14 8.01 =0.01 19.733 8.433 =24.38 4.667 =3.29 =120.76 15 10.00 =0.01 22.767 9.167 =4.54 5.067 =9.77 =119.29 16 :22.01 =0.01 25.833 10.100 16.41 5.200 =16.03 =119.05. 17 :13.99 =0.01 26.520 11.767 34.72 6.100 =27.43 =111.11 18 15.99 =0.01 28.667 13.167 50.78 6.633 =34.14 =109.18 19 18.00 =0.01 28.907 14.840 64.60 4.633 =31.46 =119.17 20 20.01 =0.01 28.973 16.647 74.35 3.967 =30.78 =122.02 21 :22.02 =0.01 30.240 18.407 87.86 4.027 =34.55 =128.93 22 -24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52 23 -25.00 =0.01 34.073 21.600 100.20 5.5587 =48.95 =133.21		:99	-15.02	-0.01	=23.500	10.967	-210.6R	6 6 4 3 3	67.87	=152.93
11 : 2.00 = 0.01 10.800 7.433 = 82.88 5.367 14.09 = 140.26 12 3.99 = 0.01 13.433 7.700 = 65.14 4.893 9.55 = 132.67 13 6.01 = 0.01 16.600 8.033 = 44.40 4.407 3.32 = 128.47 14 8.01 = 0.01 19.733 8.433 = 24.38 4.667 = 3.29 = 120.76 15 10.00 = 0.01 22.767 9.167 = 4.54 5.067 = 9.77 = 119.29 16 : 12.01 = 0.01 25.833 10.100 16.41 5.200 = 16.03 = 119.05 17 : 13.99 = 0.01 26.520 11.767 34.72 6.100 = 27.43 = 111.11 18 15.99 = 0.01 28.667 13.167 50.78 6.633 = 34.14 = 109.18 19 18.00 = 0.01 28.907 14.840 64.60 4.633 = 31.46 = 119.17 20 20.01 = 0.01 28.973 16.647 74.35 3.967 = 30.78 = 122.02 21 : 22.02 = 0.01 30.240 18.407 87.86 4.027 = 34.55 = 128.93 22 -24.01 = 0.01 34.073 21.600 100.20 : 5.587 = 48.95 = 133.21		10	0.00	=0.01	7 . 433	7.133	=102:37	5 . 967	19:37	=148 • 10
12 3.99 =0.01 13.433 7.700 =65.14 4.893 9.55 =132.67 - 13 6.01 =0.01 16.600 8.033 =44.40 4.407 3.32 =128.47 14 8.01 =0.01 19.733 8.433 =24.38 4.667 =3.29 =120.76 15 10.00 =0.01 22.767 9.167 =4.54 5.067 =9.77 =119.29 16 12.01 =0.01 25.833 10.100 16.41 5.200 =16.03 =119.05 17 13.99 =0.01 26.520 11.767 34.72 6.100 =27.43 =111.11 18 15.99 =0.01 28.667 13.167 50.78 6.633 =34.14 =109.18 19 18.00 =0.01 28.907 14.840 64.60 4.633 =31.46 =119.17 20 20.01 =0.01 28.973 16.647 74.35 3.967 =30.78 =122.02 21 22.02 =0.01 30.240 18.407 87.86 4.027 =34.55 =128.93 22 -24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52 23 -25.00 =0.01 34.073 21.600 100.20 5.587 =48.95 =133.21		11	: 200Q ·	=0.01	10.800	7 + 433		5+367	14+09	=140+26
13 6.01 =0.01 16.600 8.033 =44.40 4.407 3.32 =128.47 14 8.01 =0.01 19.733 8.433 =24.38 4.667 =3.29 =120.76 15 10.00 =0.01 22.767 9.167 =4.54 5.067 =9.77 =119.29 16 12.01 =0.01 25.833 10.100 16.41 5.200 =16.03 =119.05 17 13.99 =0.01 26.520 11.767 34.72 6.100 =27.43 =111.11 18 15.99 =0.01 28.667 13.167 50.78 6.633 =34.14 =109.18 19 18.00 =0.01 28.907 14.840 64.60 4.633 =31.46 =119.17 20 20.01 =0.01 28.973 16.647 74.35 3.967 =30.78 =122.02 21 22.02 =0.01 30.240 18.407 87.86 4.027 =34.55 =128.93 22 24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52 23 25.00 =0.01 34.073 21.600 100.20 5.587 =48.95 =133.21		:12	3.99	=0.01	13.433			4 . 893	9 + 55	4132.67 -
15 10:00 =0:01 22:767 9:167 =4:54 5:067 =9:77 =119:29 16 :12:01 =0:01 25:833 10:100 16:41 5:200 =16:03 =119:05. 17 :13:99 =0:01 26:520 11:767 34:72 6:100 =27:43 =111:11 18 15:99 =0:01 28:667 13:167 50:78 6:633 =34:14 =109:18 19 18:00 =0:01 28:907 :14:840: 64:60 4:633 =31:46 =119:17 20 20:01 =0:01 28:973 16:647 74:35 3:967 =30:78 =122:02 21 :22:02 =0:01 30:240 18:407 87:86 4:027 =34:55 =128:93 22 :24:01 =0:01 31:827 20:273 96:56 4:867 =44:25 =131:52 23 :25:00 =0:01 34:073 21:600 100:20 5:587 =48:95 =133:21		13			16,600	8 • 033		. 4.407		
16 :12:01 =0:01 25:833 10:100 16:41 5:200 =16:03 =119:05. 17 :13:99 =0:01 26:520 11:767 34:72 6:100 =27:43 =111:11 18 15:99 =0:01 28:667 13:167 50:78 6:633 =34:14 =109:18 19 18:00 =0:01 28:907 14:840: 64:60 4:633 =31:46 =119:17 20: 20:01 =0:01 28:973 16:647 74:35 3:967 =30:78 =122:02 21 :22:02 =0:01 30:240 18:407 87:86 4:027 =34:55 =128:93 22 :24:01 =0:01 31:827 20:273 96:56 4:867 =44:25 =131:52 23 :25:00 =0:01 34:073 21:600 100:20 5:587 =48:95 =133:21	Section 1985	14	8.01	-0.01	19,733.	8+433	24.38	4 . 667	·3·29	=120.76
17 :13:99 =0:01		-15	10.00	-0.01	22.767	9+167	=4+54	1 5.067	-9.77	=119.29
17 :13*99 =0*01 26*520 11*767 34*72 6*100 =27*43 =111*11 18 15*99 =0*01 28*667 13*167 50*78 6*633 =34*14 =109*18 19 18*00 =0*01 28*907 14*840 64*60 4*633 =31*46 =119*17 20 20*01 =0*01 28*973 16*647 74*35 3*967 =30*78 =122*02 21 :22*02 =0*01 30*240 18*407 87*86 4*027 =34*55 =128*93 22 :24*01 =0*01 31*827 20*273 96*56 4*867 =44*25 =131*52 :23 :25*00 =0*01 34*073 21*600 100*20 55*587 =48*95 =133*21		16	12.01	=0.01	25.833	10:100	16.41	5.200	=16.03	-119 • 05.
18 15.99 =0.01 28.667 13.167 50.78 6.633 =34.14 =109.18 19 18.00 =0.01 28.907 14.840. 64.60 4.633 =31.46 =119.17 20 20.01 =0.01 28.973 16.647 74.35 3.967 =30.78 =122.02 21 22.02 =0.01 30.240 18.407 87.86 4.027 =34.55 =128.93 22 24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52 23 25.00 =0.01 34.073 21.600 100.20 5.587 =48.95 =133.21		17	13.99	=0.01	26.520	11.767		4.100	=27 :43	=111.11
19 18,00 =0.01 28.907 .14.840. 64.60 4.633 =31.46 =119.17 20: 20.01 =0.01 28.973 16.647 74.35 3.967 =30.78 =122.02 21 :22.02 =0.01 30.240 18.407 87.86 4.027 =34.55 =128.93 .22 .24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52 .23 .25.00 =0.01 34.073 21.600 100.20 : 5.587 =48.95 =133.21		18	15.99	=0.01	28.667	13 • 167		6 • 633	-34-14	=109 • 18
20: 20:01 = 0:01 28:973 16:647 74:35 3:967 = 30:78 = 122:02 21 :22:02 = 0:01 30:240 18:407 87:86 4:027 = 34:55 = 128:93 .22 :24:01 = 0:01 31:827 20:273 96:56 4:867 = 44:25 = 131:52 .23 :25:00 = 0:01 34:073 21:600 100:20 5:587 = 48:95 = 133:21		19	18.00	-0.01	28.907	-14-840		· 4+633	-31+46	-119+17
21 :22.02 =0.01 30.240 18.407 87.86 4.027 =34.55 =128.93 .22 .24.01 =0.01 31.827 20.273 96.56 4.867 =44.25 =131.52 .23 .25.00 =0.01 34.073 21.600 100.20 : 5.587 =48.95 =133.21		50.	20.01	-0.01				3.967	-30.78	-122.02
22 ·24 ·01 =0 ·01 31 ·827 20 ·273 96 ·56 4 ·867 =44 ·25 =131 ·52 23 25 ·00 =0 ·01 34 ·073 21 ·600 100 ·20 : 5 ·587 =48 ·95 =133 ·21		21	:22.02	-0.001				4.027		
23 25.00 =0.01 34.073 21.600 100.20 : 5.587 =48.95 =133.21	<u>i; (E. 1916) — 'a mai a mai a</u>	.22	-24.01	-0.01						
		23	25.00	-0.01						
		24	-0.02	-0.01						

RUN 39		41/1	9/81	0907				RUN 35	1.3
	TEMP : 94.				PO	14+	6464·		
GPSF 75.0	00 YFPS							0 < 2254	
•	0 0 T11 T12 T	39 0	0 T15 T1	0 = 0	Ø	. 0	Ó		

PNT	ALPHA	PSI	'L/Q	.D\d	PM/Q	DVY.	RM/Q	' YM/Q.
	0.02	0.01	-1.333	5.767	-91+24	i 5.567		=147+58
	-2.02	0.01	-2.300	5 6873	*108+37	5 . 613		=149+35
	4-00	0.01	-3.133	5 : 693	-123.58	6.133		≈159.36
4	-6.02	0.01	=4.033	6 4 133	=140 .56	· 6:733		=164.06
5	=8 • 01	0.01	#4.900	6 . 467	#155 - 18	7.120	•	=168+34
6	=9.99	0.01	=6.000	6.933	=166487	7.267	. 54+79	=168+96
7	-11.99	0,01	-7,133	* **400	-176+94	6,933	. 58.87	=161.70
- ANGRES NORTH AND 3	-14.00	0.01	-8.233	7.527		6.067	61.88	=149.09
er in de la	=15.01	0.01	-8.900		=192,93	5.933	. 63.76	=145.06
10	:=0.01	0.01	.=1.367	5.767	=91.76	5 . 567	20.26	×145 * 42
11	: 2.00	0.01	=0,433	5,833	=76 47	5 . 267	13.98	=139+52
.12	4.01	0.01	0.633	5.733		. 4.713	8 • 47	=128.56 -
13	4.C1	0.01	0.600	5.767		41667	7 • 99	=130.49
	6.02	0.01	1.533	5.800	And the second of the second o	4 4 100	4.61	-122.95
15		0.01	2.300	5 . 807	=29.40	3 . 8 6 7	0.23	-119.92
.16	10.01	0.01	3,233	. 6.000	=10.61	3,533	=5 €42	=119.57
17	11.98	0.01	4.267	. 6.233	5.79	4 . 067	=9 *48	-119·69
18	.14.03	0.01	5.300	6.527	20.60	4.200	■15+54	=123.48
£ 19	16.00	0.01	6.367	7 - 067		4.233		=125.59
20.		0.01	7.333	7.767	51.16	: 2.567		-117×13
<u> </u>		0.01	8.000	8.367		2 . 567		-113.74
22	:22 - 01	0.01	8.967	8.967	82.12	: 2.733		=116+40
.23:		0.01	9.867	9.633	95.72	3:133		=114.49
24	25.00	0.01	10,233	9.900		3.113		#116.48
25	-0.01	0.01	-1.400	5.767		5,427		*147.45

ORIGINAL PAGE IS OF POOR QUALITY.

A - 42

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ORIGINAL PACE IS VOUGHT LOW OF PEOPLY WHAT THE TEST 1630

WIND (AXES

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DATA AT C.G. FULL SCALE DATA SINGLE SUPPORT DATA RM/Q ' YM/Q .ALPHA PM/Q 'Y/@ PNT ,PSI L/Q 'D/Q ⇒ 21.38 **=**151.30 ----EE0.01- 10.033 44+54 5.767 7.267 29.51 -152.02 72,95 5.640 2 .-1.98 ·0.01 #13.767 7.800 38.00 -157.20 107.52 6.067 --4-02 ·0 • 01 -17 • 900 8.200 6.500 . 45.05 m163.98 9.033 137 . 48 ·=6 * 01 0.01 -21.800 . 51.21 =171.23 7.1200 '=7 · 98 0.01 #23.700 144+02 5 10 • 180 59489 -171.53 0.01 -24.900 7.4367 =10.01 137.03 11.340 66.22 m168.90 7.353 0.01 -27.267 -12,03 12.667 144.00 71,36 -165.22 6.967 0:01 =29:367 152.06 8 -14,01 13.967 67.81 -159.55 0.01 -29.300 6.600 9 -13.98 13.913 151 - 20 69.36 =150.21 6:013 10. =15:01 0.01 -30.947 14.727 161.30 5 . 867 : 22 59 **8154** 78 11. =0.02 0.01 =10.300 7 4 4 6 7 42.49 =6.667 . 6.900 15.49 -145.51 5 . 567 :12 : 5.05 0.01 18 . 82 -6.41 ; 5.033 7.82 -137.85 ++00 13 .0.01 -3.033 6.667 0.333 6.00 2,19 -133.86 4.700 14 0.01 6.633 _-27.72 4 . 567 **=2.69 =135.14** 8.02 =48.65 0.01 3.500 6.633 15 =7.83 =135.13 -75+33 - 4 + 687 9.99 0.01 16 7,400 - 6+667 **=12**089 **≈133**€66 :12:01 7 - 133 = 101 - 78 0.01 4.733 17 11.167 7.833 -112.94 =17.82 =135.18 · 4 • 767 13.833 18 14.02 0.01 =23.90 =133.54 8.967 -114.20 - 4.700 19 16:02 0.01 15.900 0.01 18:167 10:567 -118:12 3:173 **=25.18 =123.31** 20 18.00 =29.84 =120.36 20.00 0.01 19.567 11.733 -116.37 2.733 21. 0.01 20.733 :12.933 -110.69 : 2.953 ±33€42 ±120+28 .22 21.96 **=37** \ 66 **=118** \ 79 0.01 22.333 14.320 =110.13 1 3.100 .23 -24 - 01 -42×82 =117×74 23 . 400 15.200 -115.63 : 3,400 24 .24.98 0.01 43:47 5:687 22:03 =150:68 0.01 -10.167 7.267 -0.01

ORIGINAL PAGE IS OF POOR QUALITY

A-43

WOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

TEMP 94. 11/19/81 0907 RUN 41

GPSF 75 000 VFP9 260 12 RNFT 1484616 MACH 0 2254

	SIN	ALE SUPP	ORT DAT	A	DATA '	T C.G.	FULL	SCALE DA	TÀ
	PNT	ALPHA	.PSI	LPQ	.D\Ø	PM/Q	.Ā∖ē	RM/Q	· YM/Q
	1	0.01	0.01	-1,133	5 * 267	-94.38	=0.267	=1,+35,	0.76
그는 이 후 가능을 하셨다면 살았다.	: 2	:-2.01	0.01	-2.033	5 400	-110-10	-0.573	0.83	0.01
	3	-4.00	0.01	.=3.000	5 . 600	-127.70	=0.167	-0.66	1.44
	. 4	·=6:03	0.01	=3,867	5 + 800	=143.30	0 + 433	=0+79	· =2.78
	5	=7.99	0.01	# 4.700	6.100	=156+24	0.547	=0.88	-5-65
	. 6	×9.95	0.01	=5.700	6 • 433	=170:09	0 * 573	-0.91	- 20.61
	7	#12.01	0.01	-6.867	6.933	-181.94	0.367	-1-14	1 -0.09
	8	-14-04	0.01	-8,100	7.433	-192.46	-0.067	=1,62	3*33
	, 9	-15.00	.0.01	-8.667	7 . 7 67	-198.14	-0.0U7	=1.43	. 3+19
	10	0.02	0.01	=1:167	. 5 . 333	=94.28	=0:300	=1.33	2,62
	11	. 1.99	0.01	=0.267	5.300	=79+94	=Q+267	-1.36	0.07
	:12	4.01	0.01	0.733	5.300	=63.42	=0.400	=1 = 15	0+98 -
	13		0.01	1.667	5+367	-#48+38	-0.733	-0.59	0 • 6 6
	14	8.02	0.01	2.500	5+467	30.47	-0:833	-0.53	0.13
	15	10.01	0.01	3.400	5.600	-12.43		-0.59	· =0.33
	.16	11,98	0.01	4.400	5.800	4.19	=0.707	=0.75	=1.62
	17	13.99	0.01	5.433	6+167	20.30	-0.500	=0.76	=1.83
	18	16:02	0.01	6.433	6 6 6 6 7	37.28	=0.393	=0.61	-5-14
	19	18:01	0.01	7.300	7.233	52.97	#0.700	=Q+44	· =1 ×39
4	20	20.00	0.01	8.200	7.800	68.55	:=2.013	1+04	0.57
	21	22.01	20.01	9.067	8 - 500	83.49	-1.700	1 < 92	-1-58
CONTRACTOR OF THE PARTY OF THE	:22		0.01	10.000	9 . 167	99,03	=1:407	1.71	· =1 =70
	:23		0.01	10.400	9.467	105 85	=1 +400	1+79	-2+66
	24		0.01	-1.233	5 • 333	=94.98		=1.13	1.59
						<u> </u>			

													· ·	1
and the state of t		RUN :42	·	··		11/	19/8	1 05	207			<u></u>	RUN :42	<u> </u>
		•	TEMP	7 7	ś •				3	64	14.	6120		
and the second s	,	GPSF 75.	00	VF	98 8	56.1	6	RNFT	15	4644	9.	MACH	0 - 2257	
			TOT	702	FOT	T04	105	T06	TOT	BOT	TOS	T10		
			") Q	0	39	. 0	. 0	. 0	. 0	٠ ٥	ı Ç	0		, (I-1,0)
		·	T11					T16		718	T19	720		
er var er		·	***********											

de a sur l'adrianting de la contra del la contra de la contra del la contra del la contra de la contra del la contra d	SIN	LE SUPP	ORT DAT		· DATA	AT C.G.	FULU	SCALE SA	ra .
	PNT	.ALPHA	PSI	'L/Q	D/Q	PM/Q	'Y/Q	RMZQ	. AW\d
		=0.01	0.01	-0.867	5.600	-94-52	-0.367	-0.80	2+75
	2	1-2.00	-0.01	-1.800	5 • 680	-110-23	-0+167	-0+80	0.96
	3	3 - 3 - 5 B	0.01	-2.733	5.747	-125-40	0.000	=0.83	-1.00
	. 4	·=6 . 00	0.01	=3,633	5,980	-141+44	0.273	-1.Q1	-1.92
	, 5	′=7•99	0.01	-4.567	6.313	=157 •95	. 0.300	-0.71	· * 0 • 19
	6	· * 9 • 9 9	0+01	= 5.557.	6 • 680	=171.27	0.200	-0.98	0.58
	7	-12.02	0.01	-6.800	7.013		#0+047	-1-13	2 • 80
		-14.01	0.01	-7.900	7.613		-0.360	-0.72	4.50
	9	-15.02	0.01	-8.500	7.880		-0.400	-0+69	3+49
· · · · · · · · · · · · · · · · · · ·	10	0.01	0.01	=0.667	5.533	=93.33	=0.353	. #0+64	1+46
	11	: 2.00	0.01	0,233	5.580	=76 ≠99	₩0:360	≈0 €65	1.043
•	:12	. 4.02	0.01	1.267	5 • 5 4 7	=62.82	-0.600	≈0 ≈55	2 + 25
	:13		0.01	2,400	5.913		-1+067	· =0.52	0 • 63
eria.	-14	8.02	0.01	3.367		-31.26	-1.267	-0.40	0 < 13
	15		10.01	4.333	6.347		-1:367	=0+47	4 =0.38
	16		0.01	5,300	6.580	1,69	.=4.567	#0 +65	0.34
•	117		0.01	6,233	6.947	19+04	-1·847	- =0 +45	2.60
	1.8	16:01	0.01	7.167	7.413	35 • 61	-2.500	0 # 10	5.38
- 19-1 11-1-11-11-11-1-1-1-1-1-1-1-1-	:19		0.01	7.867	7.780		:=2.767	0+44	7.41
,	20		0.01	8.567	8+147	69.22	-3+267	3.07	6.95
	21		0.01	9.567	8.880		.=1 +067	2 + 95	-2.50
	.22		0.01	10,267	9.347		=1.067	2,55	-1.90
	:23		0.01	10.633	9.680		≈0 1967	2 42	=1.66
	24		0.01	=0.600	5.513	=94+69	m0 4367	=0.63	1.98
					, , , , , , , , , , , , , , , , , , , 				4720

ORIGINAL PLACE TO OF FOOR QUALITY

WOUGHT LAW SPEED WILL TUNNEL TEST 630

WIND AXES .

RUN 43 11/19/81 0907 1 RUN 43

* TEMP * 76.

· F6 . 14.6120.

	SINC	LE SUPPO	IRT DAT		DATA	T C.G.	FULL	SCALE D	ATAA	
	PNT	.ALPHA	PSI	.F\d	D/Q	PM/Q	'Y/Q	: RM/0	. AW/6	
	1	0.00	0.01	=1,033	6.800	#92.56	5.127		413 11.62	
	2	(#2.03	0.01	w1.967	6.233	-109+85	5 • 133		=137.40	-54
		-4.01	0.01	·=2,967	<u>, 6.330</u>	=125.64	5.633		#14 · 65	
	. 4	-6 + 0 O	0.01	=3.833	6.433	=140 ·42	6.000		#145 ·39	
W. p.	· 5	:≖8+00	0.01	=4.833	6.800	-15 .81	5.919		≈140 • 59	
	6	=10.02	·0.01	=5.933	7 • 233	=167.92	5 • 433		=128.55	
	. 7	-11,99	0.01	-7.000	7.700	-179.48	. 4.600	43.93	-111.71	
	8	-14.00	0.01	-8.233	8.300	-190 -77	4.000	+4.95	-101+85	
	: 9	~14.99	0.01	-8,833		=195.34	1 3.920	- 46.81	-100.93	
	10	10.00	0.01	-1,000	. 6.160	=92:67	5.120	. 21:11	4134 *93 .	
	.11	2.01	0.01	=0.167	6 • 167	=76 -13	· 4:713	14.76	×127 • 19	
	:12	- 4 = 00	0.01	0.900	6.167	= 60 ∙89	. 4.267		=121+11	*
	13	. 6.02	0.01	1.933	6.367		3,613	5.32	=118+59	
		8.02	0.01	3.067	6.580		: 3.193		-120.36	
		10:01	0.01	4.033	6.800	=14.91	3 • 067	-3.68	-122.03	
<u></u>		:12.04	0.01	5,100	7. 133	1.87	: 2,933	· =8.61	=123.39	
		.14.00	0.01	5,933	7.567	15,50	: 2.567	12+70	=122.70	
	18	16.00	0.01	6.767	7.4833	1 32.36	: 2.233	=16.33	-119.01	:
		17.99	0.01	7.433	8,367	49,65	1.860		-114.30	
		19.99	0.01	8.067	8 • 833	65-12		-22.20	-108-19	
•	21.		0.01	8,833	9.367	82.25		-24.30		
	.22		0.01	9.833	10.033	97+14	: 3:767	=32,25		
	,23		0.01	10.100	10.267	102 43	3.700	=33+50		
	-24		0.01	-1.033	6.113	=92·50	5.173		■134 • 94	
			: -				--		* * ****	-

WIND AXES

+ RUN +4 T1/19/81 0907 RUN 44

* TEMP 76.

R0 14.5973

	1	GPSF	•	75	.0	0		YF	P8 2	56+2	9	RNF	T 15	1566	B •	MACH	0 .2258		
	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		e in in Silverin			TG	1	T02	T03	T04	T.05.	T06	707	708	T09	T10		- H - W - 1	,
·		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		-			0	Q	39	٥	٥	• 0	0	Q	1 Q	Ō			
					•	T.1	t	T12	713	T14	T15	T16	T17	T18	719	T20			
						j, e	Ó	-				. 0	-		: 0	Ò			

									at T	
	SING	LE BUPP	ORT DAT	<u> </u>	. DATA	T. C.G.	FULL	SCALE D	ATA	
	PNT	.ALPHA	PSI	L/Q	.D/d	· PM/Q	. A/d	RM/Q	. AW\a	
	9 1	0.01	0.01	=1,100	6.213	=93:73	5,113		#133.34	
	. 2	-4.00	0.01	=1.933 =2.967		-111.36 -126.43	5.333		=136+12 =142+55	
	• 4	.=6.02	0.01	=3.933	6.533	=142+87	6.067	35 +00	≈146 • 00	
	: 5 6	=8.01 =10.00	0.01 0.01	=4,933 =5.867.	6 • 820	=156+12 =167+16	6 • 000 5 • 600	40.93 42.62	=142 *26 =127 *92	
	7.	-12.01	0.01	-7.133	7 . 700	-178-24	4,627	43.07	-111:63	
	, 8 , 9	=13.99 =15.01	0.01	-8.167 -8.567	8 • 267	=189+30 =196+26	3.967 4.033		=102.37 =101.24	
<u> </u>	10	-0.01	0.01	-1.000	- 6+280	-95.15	5,167	20.08	4134 • 85	•
	11:12	1.99	0.01 0.01	-0.167 0.900	6 • 267 6 • 300	=76+04 =62+09	· 4 • 627	14+14 9+10	=125+94 =117 < 67	
	13	6.00	0.01	5.033	6.373	-46.67	3.587	3 + 49	-117-73	
	14	7.99 9.99	0.01	2.967 3 4.000	6.600	=33.05 =17.30	3,253 3,080		=117.51 =120.58	
	16	:12.02	0.01	4.967	7.300	=2.11	: 2:967	· =9.28	=124 - 84	
	17		0.01	6.000 6.933	7 • 700 8 • 067	13+24 29•71	2 • 627 2 • 267	=13.58 =17.57	=122+20 =116+45	
	.19	18.00	0.01	7.433	8+467	44.40	1.753	-20.85	-112-16)
$\frac{d}{dt} = \frac{dt}{dt}$ $\frac{dt}{dt} = \frac{dt}{dt}$ $\frac{dt}{dt} = \frac{dt}{dt}$	20 21		0.01	8,233	9.000	61+85 77+38	1 • 1 8 0	-23.43 -26.97	=106.78	
<u> </u>	.22.	.23.99	0.01	9.867	10.200	89,98	; 3,933	=33.07	=120.38	1
	23; 24	E0.55:	0.01 0.01	10.267	10.533 6.267	97:11 =93:56	3.700 5.033	-35 ÷86	<pre>=118 • 70 =131 • 80</pre>	
	T T		4 7 7 4		₩ ₩ ₩ /	-30100				***********

ORIGINAL PAGE IN OF POOR QUALITY

A-47

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND :AXES

ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	' YM/Q
			7.500	22,98	4.947		=129+29
				48.96	* 5.033		-131.27
			8.567	75.35	· 5 • 633	32+04	=139.51
≖6 + 03			9 167	103+94	· 6 • 08¢		
=8.00	0.01	-21,333	10+333	110:38	6.233	45 ₹54	=147 #00
=10.05	0.01	=23.200·	11.520	108.37	5.000	49.70	-143.07
-12.01	0.01	-25,833	:12.773	120.51	5.433	51.84	-133.11
-14.02	0.01	-28.200	14.100		- 4.733	53.96	-118:17
m14.99						55.78	-114.85
0.00	0.01					18+84	=127 × 05
. 2.03	0.01					12.65	=124+06
4.00	0.01						=121·51 -
							=119.22
							#120·53
						The fight by a second of	=123.94
							=124.66
							=123+22
							=120•97
							=116.75
7 T T T T T T T T T T T T T T T T T T T							-111-15
							-104.21
							#121+24
-0.01	0.01	*** A .L A A	*~				=128 - 28
	0.02 -2.00 -3.98 -6.03 -8.00 -10.05 -12.01 -14.02 -14.99 -0.00 -2.03 -4.00 -0.02 -7.99 -10.02 -12.01 -13.99 -16.00 -18.01 -20.03 -22.00 -24.04 -24.99	0.02 0.01 -2.00 0.01 -3.98 0.01 -6.03 0.01 -8.00 0.01 -10.05 0.01 -12.01 0.01 -14.02 0.01 -14.09 0.01 -2.03 0.01 -4.00 0.01 -6.02 0.01 -7.99 0.01 -12.01 0.01 -13.99 0.01 -13.99 0.01 -13.99 0.01 -13.99 0.01 -13.99 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01 -14.00 0.01	0.02 0.01 -8.533 -2.00 0.01 -12.433 -3.98 0.01 -15.833 -6.03 0.01 -19.700 -8.00 0.01 -21.333 -10.05 0.01 -23.200 -12.01 0.01 -25.833 -14.02 0.01 -25.833 -14.02 0.01 -28.200 0.00 0.01 -29.600 0.00 0.01 -8.633 -2.03 0.01 -5.133 -4.00 0.01 -2.033 -4.00 0.01 -2.033 -7.99 0.01 1.033 -7.99 0.01 10.467 13.99 0.01 10.467 13.99 0.01 13.433 16.00 0.01 15.633 18.01 0.01 17.667 20.03 0.01 19.567 -22.00 0.01 22.567 -24.99 0.01 23.400	0.02 0.01 -8.533 7.500 -2.00 0.01 -12.433 8.000 -3.98 0.01 -15.833 8.567 -6.03 0.01 -15.833 10.333 -10.05 0.01 -23.200 11.520 -12.01 0.01 -25.833 12.773 -14.02 0.01 -25.833 12.773 -14.02 0.01 -28.200 14.100 -14.99 0.01 -29.600 14.833 0.00 0.01 -8.633 7.567 -2.03 0.01 -5.133 7.267 -4.00 0.01 -2.033 7.167 -7.99 0.01 1.033 7.167 -7.99 0.01 1.033 7.167 -7.99 0.01 10.467 7.967 13.99 0.01 10.467 7.967 13.99 0.01 13.433 8.733 16.00 0.01 15.633 9.800 18.01 0.01 17.667 10.840 -20.03 0.01 15.633 9.800 18.01 0.01 17.667 12.233 -24.04 0.01 22.567 14.947 -24.99 0.01 23.400 15.593	0.02 0.01 -8.533 7.500 22.98 -2.00 0.01 -12.433 8.000 48.96 -3.98 0.01 -15.833 8.567 75.35 -6.03 0.01 -19.700 9.167 103.94 -8.00 0.01 -21.333 10.333 110.38 -10.05 0.01 -23.200 11.520 108.37 -12.01 0.01 -25.833 12.773 120.51 -14.02 0.01 -28.200 14.100 132.05 -14.99 0.01 -29.600 14.833 140.08 0.00 0.01 -8.633 7.567 23.04 -2.03 0.01 -5.133 7.267 0.59 -4.00 0.01 -2.033 7.167 -31.27 -7.99 0.01 1.033 7.167 -31.27 -7.99 0.01 10.467 7.967 -85.08 10.02 0.01 7.233 7.500 -64.80 -12.01 0.01 10.467 7.967 -85.04 -13.99 0.01 13.433 8.733 -98.38 -16.00 0.01 15.633 9.800 -106.04 -18.01 0.01 17.667 10.840 -113.17 -20.03 0.01 19.567 12.233 -116.03 -24.04 0.01 22.567 14.947 -116.94 -24.99 0.01 23.400 15.593 -118.33	0.02	0.02

93 	RUN 46 11/19/81 0907 RUN 46
	TEMP 76. RØ 14.5973
	QPSF 75,00 VFP8 256.29 RNFT 1545668. MACH 0.2258
	TO1 YO2 TO3 TO4 TOS TO6 TO7 TO8 TO9 T10
	T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

\$IN	BLE BUPRI	BRT DAT		DATA	7 C.G.	FULL	SCALE D	YTA
PNT	.ALPHA	PSI	L/9	.b\ø	PM/Q	evy.	RM/Q	' YM/Q
	-0.01	0.01	=9.700	7.700	39.73	5.273		=134.79
	-1.99	0.01	-13.433	8 : 100	67+45	: 5.500	26.92	=137.63
- 1 : 1 : 1 : 1 : 1 : 1 : 1 : 1 : 1 : 1	-4+03	0.01	#17.867	8.767	105.39	5.760		=146 €03
. 4	=6 ¢ 0 Q	.0.01	-21.500	9.433	133 43	6.300	40.35	H151 • 71
5	-8.02	0.01	-23,820	10.613	143 + 01	6 + 400	46 . 22	4153.56
6	=9.95		-24.740.	11.820	132 87	6 • 413	52.75	H150.51
7.		0.01		13.100	139+63	5 + 767	54 : 23	≈138.09
	-14:02		-29.267	14.367	147.78	5 . 367	58.25	=130+65
	-15.02	0.01		15.040	154.20	5.033		≈125∗39
1.0	:=0.01	0.01	=9.767	7.+800	40 - 57	, 5.233	20+44	
11	: 2.01	0.01	#6.233	7.400	16.91	5.167		≈130 • 40
12	3098	0.01	≥2.633	7.300	7.78	4.713		#126·80 -
		Mail.	0.833	7.400	=28.79	4 9 0 4 7		=129+26
14		6.01			-50.11	. 3.853		+133.41
15					-75.82	3.767		≠135
	12.01	0.01	11,733	80883	#103.56	3.567		=134+15
17	:13.99	0.01	14.400	9.033	6127147	: 30887		=131·97
18		0.01	16.500	10.067				=126.68
19		0.01	18,667		-125.19			~ <u>{20.39</u>
20		0.01	19,867		-124.79			91846-52
		0.01				0.267		-(ale85
21		0.01	21.233		#115.56	4.000	-36.01	
			21,100	13.700	=116:77		-41-09	
23		10.0	22,500	15 + 127		3 : 833		#119.99
24		0.01	23.167	15.727		3 • 853		
25	0.00	0.01	-9+620	7.767	39 • 40	5.267	CUNTS	≈133 .93

WIND AXES

RUN 47 \$1/19/81 0907 : RUK 47

TEMP 76.

* 18 CAL

P5 . 14.5973

	SIN	LE SUPP	ORT DA		DATA	T C.G.	1FULL	SCALE D	
	PNT	.ALPHA	PSI	Ĺ/a	D/Q	PM/Q	Y/Q	RM/9	· YM/Q
	1	-0.02	0.02	-9.500	9.067	33.01	5.093		=136 *93
	. 2	-2.00	0.02	m13.767	9 . 600	57.34/	3.627		#132*63
	3	-3.99	00.02	m18.933	10,033	89.69	13.293		-125 • 79
7 (. 4	:-5.98	0.02	=22,933	10.700	113 • 70	・ 4+827	39,59	
No. of	. 5	=8.02	0.02	-26,653	12.020	119.05	. 6:260	45 • 89	=144=91
	6	=10.00	0.02	-29,900	13 4833	112.19	5 660	52.09	=138 · 67
	. 7	-12.00	0.02	-33.667	16.167	121,55	: 5.527	58,41	#135.38
	. 8	-14.02	0.403		19:073		. 4.960	60.56	#125·48
	9		50.0	#36.707	20+433	144.65	5+C27	. 62.16	-122.88
	10	20:02	0.02		9 • 187	32.81	· 5 : 127	19+18	-1 236√95
	11	: 2.00	0.02	₩3.800	9.267	15:40	5.927	12:47	m137.77
	12	3.99	0.02		9.533	1.20	6.327	4 . 88	≈137.43 -
		3.98	0.402		10.133	*14.63	. 5.560	=1.17	4132.51
	14		0.02		10.767	29+70	4.927	-5.99	=128.68
	15		0.02		11.700		. 4.467	-10-43	=125 ·56
<u> ئۇرىلىلىيىسىلىنىلىلى ئىسىدى ئىلىنى ئىسىگىلىنى ئىسىگىي</u>	16	.12,01	0,02		:12.647	=52.46	4.093	-12.96	=123.90
	17	.14.01	0402		14.033	=66.00	. 3,327	= 15 •53	=120 · 46
	18		0.02		15.547	≈75·62	2.993	=19-29	=114 • 59
	19		0.02		17.300	-85.30°	, 2.593		#111+84
	50	* * * * * * * * * * * * * * * * * * * *	0.02		19:373	-90+84	2.560		=114.34
	21		0.02		55.500	*97.66	5.360		=129.23
	55		0.02		25.500	≈112.28	6.427		#136.26
	,23	24.97	0.02		27.233	*119+64	6.860		=139.51
	24	•	0.05		9.167	33 • 82	5.060		#138 #69
· · · · · · · · · · · · · · · · · · ·	<u> </u>	<u></u>		-0.00/	36701			- W 11 W	

. RUN :			11/19/8	1 1907	: RI	UN :48
	TEMP	76,			P6 14+5973	
aP8F					45668. MACH	0 x 2 3 5 8
	T11	0 48	0 0 T14 T15	0 0	0 0 0 718 719 720	

	SING	LE BUP	PORT DA	7 A	DATA	C.G.	FUL	SCALE D	ATA
	PNT	ALPHA	PSI	.F\d	' 'D/Q	PM/Q	Y/Q	RM/Q	· YM/G
	1		0.01		:12.900	43+32			4136*38
	2		2.02	-9,813	12.867	44,46	2,333		#133.75
·	; 3		-3.98	m10.133	12.733	48.80	-0.367	17.63	=128 * 43
	4		- =6.01	=10,600	113 . 167	52.50	·=4 • 100	: 21/27	-120·49
	5	0.02	• =8 ∗00	#10.100	113.633	49 • 29	' = 7∙967	. 21 + 18	≈100•22
	6		=10.02	= 9.233.	.14.600	42.21	≈12.767	19 87	*71.96
ta una articolor La Nagada	7	0.02	-12-00	-8.000	15.600	32+74	#17+533	18.96	*用本件+CK
생님	. 8	0.02	.#14+00	-6,833	16.900	24.99	#22.620	17-14	-19+55
	9.	0.01	-16.01	-4.967		14.01	-27.+333	16/87	. 11+94
	10	0.01	=18+00	#2,333	20 + 627	2:62	#32,633	14+60	· 40#89
	11	0.01	:=20 02	00200	23.133	=9 · 05	#37 • 633	12.41	72 + 76
	12	0.00	-22 .00	10380	26 * 047	=22.27	#43 + 100	10.93	91.90 -
	.13	0.00	.=24.00				-48.367	10,50	.158.31
alga .,	14	0.00	-26.00	. 5.727		=36.28	#53 · 033	11.32	1139.75
. 19 ₁₃	15	0.00	-28.01	6.833			457.453		159.71
	16	0.00	·=30.01	6.647	40.000	=25+04	#61:120	27:02	172 433
	17	0 + 0 0	-0.03	=9.000	12.867	40.88		15010	
	18	0.00	2.01	=8.600	:13.000		, ,	12:08	=122 ∗63
	19	0.00	4 402		:13.367				#121 ×68
	20	0.00	8.02	-7.367			17.140		-155.53
	21		10:01	-6.700	15.600				*173.51
· · · · · · · · · · · · · · · · · · ·	.22.			-5,900	16.800				=199 • 47
	23.			=4.633	18,333	2+34	30.187		≈225 •69
	24	0.00		=3.200	20.133	=8.80	· ·		=255×15
	25			-1.133	22.400	=20.58			≈288.68
My J	26			0.933	24.933				=303+24
	27		. 22.00	2,120	27.707	-38.10			-299•09
	28	0.00		4,433	31.033	=48,17			=326+64
	29	0.00		5,767	34+600	≠50 €23			-347+02
	30	0.00		6.027	38 • 293	=44·48			=366 • 44
	31	-0.00		4.300	41.847				=366.95
	.32	0.00		-8.933	12.867	41.72			=137+40
12			.1		**-	7-7/6			7 ~ ~ 7 7 7

WIND :AXES

-	·	RUN (A9	11/1	9/81 0907	**************************************	RUN 149
		, TEW	> 55•	3	NO. 14.6562	
		QPSF : 75.00	VFPS 250.7:	RNFT 26	29067 MAC	H 0#2854
		TOT	TO2 TO3 TO4	705 TO6 TO7	708 TOS T10	<u> </u>
		T11	The second secon	0 0 0 T15 T16 T17	718 T19 T20	

	SING	LE SUPP	ORT DAY		DATA	T C.G.	FULL	SCALE D	MA
	PNT	ALPHA	PSI	.r\d	.D\d.	PM/Q	Y/Q	RMZQ	YM/Q
	1	0.01	0.01	-1.033	6.000	-95+34	5 • 753		-154.90
	' 2	-1.39	0.01	-1.833		-109:87	6.340		-158+81 -160+56
_ 7	<u> </u>	-4.00 -6.01	0.01	=2.700 =3.600	6 • 400	=129.98 =144.67	6.787	+0.29	=167+75
	5	=8.01	0.01	=4.700	6.767	=157+25	7.253	47+50	
	6	19.60	0.01	#5.800			7.227	53,59	=167 • 44
		-12.02	0.01	-6,933	7.667	-178:33	. 6+853	59,26	~162~63
	8	-14.02	0.01	-8.100	8.233	-188.76	. 6.253		m151 +95
	9	-14.98	0.01	=B.667	and the second of the second o				m148+00
	10	0.00	0.01	=1.000	5.967	=94,23	5.733	21.00	., .
	11	: 2.01	0.01	=0,033	5.940	=79+28	5.387	15,85	TE 1
	12	· 4:00	0.01	1.033	5.900	=65.29	. 4.927	*****	≈134•79 -
	13	6.01	0.01	1.833	5.900	=49.69	4,393		=131.98
	14	8.00	.0.01	2.733	6.100		. 4.Q87		≈128•30
		10:01	0.01	3,567	6.267	=16+09	- A+100		=127.62
		:12:01	0.01	. 4,533	6,500	0 #82	. 4:153		4131.75
	17	13.99	0.01	5,633	6 • 833	15 €82	4 . 287		
	18	16.02	0.01	. 6.800	7.300	29.99	4 • 1 87	The second secon	<u>=133+33</u>
	19	and the second of the second o		8.000	8.200				4125.32
	20		0.01	8,833	8.733	60.20	: 2.693		-124+14
	21		*0.01	9.733		75.07	. 3.013		4124.90
	:52		0.01	10:467	10.067		3.087	and the second second	
	:23		0.01	100900	10 4 4 6 7	∘ 95 € 57	3.053		=120.86
	.24	3.00	-0.01	=1.000	6.000	=95 -92	<u> 5 • 653</u>	21 * 05	=154.32

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

0 0 32 32 0 0 1 0 0

	STN	ALE SUPP	BRT DAW			7 C.G.	FULL SCALE DATA		
Water before the second	<u> </u>	344 301	13					L,	
	FNT	.ALPHA	;PSĮ	'L/Q	.D\đ	PM/Q	Y/Q	RM/Q	· YMZQ
	, \$	0.00	0.01	-1.100	5.933	-98+66	5.900		-157.50
	- A - 2	-3.00	0.01	-1.933		-114+86	6.333	. 28+66	
	3	-4.01	0.01	1-2,900	6.133	=129.74	6.800		=171.87
) nui	. 4	#6.00	0.01	.=3.933	. 6 . 433	=143.01	7.527		≈182 €18
	5	.=8+00	0.01	#4.967	6.700	≓153+68	7,853		-185+00
	6	≠9∙99	0.01	=6.100	7.200	=165.43	7.800	57 • 81	≈180 • 34
	7	-12.01	0.01	-7.267	7.633	-175 . 98	7.+280		=171 €95
100 mg	. 8	w13.98	0.01	=8+467	8.267	-185.60	6 6 6 3 3	67 +45	-159+20
	9	=15.01	0.01	-9,000	8.500	-190:12	. 6,333	68,465	m154 . 48
	10		0 0 01	=1.000	5.900	=97+96	5 800	20.97	-157 • 85
	11	: 2.02	0.01	=0.167	5 . 867	#83+49	5 . 600	13.98	m150+80
	:12		0.01	0.800	5 • 867	=68.56	5.133	8 4 6 1	=141.88
	13	. 6.03	0+01	1.767	5 . 867	-52+96	4.533	3 • 9 9	₼135.08
	14		20.0	2 . 667	6.000	=36 · Q5	4.207	-C=86	≒132•23
	15		0.01	3.500	6.167	-19.11	4 167	-5.50	-130.72
The state of the s	16		0.01	4., 400	6,400	-2.56	. 4.267	≒10+79	≈131 +83
	17		0.01	5,633	6.700	12.18	4.333	=15 *23	H134+63
	18		0.01	6.767	7.267	25.95	4.200	=20.56	=140+08
The same of the sa	19		.0,01	7,900	8.100	39,18	2.900		-125×47
	20		0.01	8,900	8.733		3.200	-30.61	-136 -93
	21		0.01	9.700	9.447		3.567	-35.52	
•	.22		0.01	10.533	10.207		: 3.633	·=41 · 10	
	23		0.01	10.867	10,467	87 +99	3 . 600	-43+15	
	.24		0.01	=1.067	5.967	-99.46	5.767		#158 #23
	- 1				***************************************				نيب نيسب بيسب بيسب

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20 0 0 32 32 0 0 1 0 0 1

SINGLE SUPPORT DATA										
1		SINC	ALE SUP	PORT DAT	'	DATA	T C.G.	FULL	SCALE D	VTA
2		PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	P\Y	RM/Q	YMZQ
2 0.01 -2.02 -0.783 5.873 -98.51 2.38U 14.32 -144.83		1	C • 01	0.00	=0.934	5 • 873	×96+64	5 • 783	19.52	-156+08
4		2	0.01	-2.02	-0.783	5 • 873		: 2 . 3 8 0	14432	-144.83
5 0.02 = 8.00						5.964	=99,93	₽0.663		
6 0.02 =9.99		- 4	. 0.01	· = 5.99	-0.301	6.325	=100.72	=3 •223	6 • 81	=143.83
7 0.02 = 12.00 0.934 9.157 #105.66 #15.181 = 9.72 = 87.67 8 0.02 = 14.01 0.783 10.542 = 94.64 #19.126 #11.03 = 67.49 9 0.02 = 15.99 0.331 12.048 = 81.84 #22.717 = 10.78 = 50.50 10 0.02 = 17.99 0.422 13.886 = 70.67 *26.566 = 10.08 = 29.64 11 0.02 = 19.99 0.482 15.964 = 60.65 *30.663 = 7.91 - 6.53 12 0.02 = 12.99 0.482 15.964 = 60.65 *30.663 = 7.91 - 6.53 12 0.02 = 23.99 0.873 21.235 = 41.54 *39.205 = 1.44 *29.57 14 0.02 = 25.99 1.205 *24.361 *34.08 *43.494 2.18 47.99 15 0.02 = 28.07 1.717 27.982 = 25.92 *47.795 6.07 69.80 16 0.02 = 30.03 21.93 *31.6687 = 16.72 *51.898 11.85 *60.08 17 0.02 *0.01 = 1.024 5.934 = 97.68 5.873 18.71 *156.52 18 0.02 2.01 *1.054 6.114 = 99.00 8.404 24.90 *159.13 19 0.02 3.99 *0.934 6.446 *101.65 10.886 31.15 *161.07 20 0.02 5.98 *0.873 6.898 = 105.72 :12.500 35.35 *149.38 21 0.02 7.98 *0.642 7.380 *111.51 15.458 40.87 *152.24 12 0.02 9.99 *0.120 8.253 = 118.99 19.247 47.10 = 172.08 12.10 *10.04 11.054 6.114 *10.44 27.99 15.458 40.87 *152.24 12.500 35.35 *149.38 21 0.02 14.948 0.211 9.217 *121.87 22.4892 51.85 *119.92 24 0.03 14.90 0.211 9.217 *121.87 22.492 55.85 *119.92 24 0.03 14.90 0.211 9.217 *121.87 22.492 55.85 *119.92 24 0.03 14.00 0.331 11.054 *116.86 27.919 55.75 *201.38 25 0.03 15.99 *0.030 12.620 *104.94 31.247 55.80 *214.96 26 0.04 18.00 0.452 14.367 *85.84 31.247 55.80 *214.96 26 0.04 18.00 0.452 14.367 *85.84 31.247 55.80 *214.96 26 0.04 18.00 0.452 14.367 *85.84 31.247 55.80 *214.96 26 0.00 12.99 *0.988 18.8946 *60.11 44.608 53.90 *232.51 27 *0.00 26.00 *1.235 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 *24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 *24.578 *28.46 53.464 41.55 *326.72 31 0.00 28.03 *21.62 *24.578 *24.55					0.271	6.928	#107+18	-7.018	0 +68	=125.07
8 G.02 = 14.01						7.771	#110.70	=10.564		
9 0.02 =15*99 0.331 12:048 =81*R4 #22*717 =10*78 :=50*50 10 0.02 =17*99 0.422 13*886 =70*67 =26*566 =10*08 =29*64 11 0.02 =19*99 0.482 15*964 =66*65 =30*663 =7*91 =-6*53 12 0.02 =21*99 0.483 18*373 =50*35 =34*910 =4*94 10*36 13 0.02 :=23*99 0.873 21*235 =41*54 *339*205 =1*44 29*57 14 0.02 =25*99 1*205 24*361 =34*08 =43*494 2*18 47*99 15 0.02 =28*07 1:717 27*982 =25*92 =47*796 6*07 69*80 16 0.02 =30*03 2*199 31*687 =16*72 =51*898 11*85 86*08 17 0.02 =0*01 =1*024 5*934 =97*68 5*273 18*74 =156*52 18 0*02 2*01 =1*054 6*114 =99*00 8*404 24*90 =159*13 19 0*02 3*99 =0*934 6*446 =101*65 10*886 31*15 =161*07 20 0*02 5*98 =0*873 6*898 =105*72 :12*500 35*35 =149*38 21 0*02 7*98 =0*873 6*898 =105*72 :12*500 35*35 =149*38 21 0*02 7*98 =0*873 6*898 =105*72 :12*500 35*35 =149*38 21 0*02 7*98 =0*873 6*898 =105*72 :12*500 35*35 =149*38 21 0*02 7*98 =0*873 6*898 =105*72 :12*500 35*35 =149*38 21 0*02 7*98 =0*873 6*898 =105*72 :12*500 35*35 =149*38 21 0*03 11*98 0*211 9*217 =121*87 22*892 51*86 =189*92 24 0*03 14*00 0*331 11*054 =116*86 27*319 55*75 =201*38 25 0*03 15*99 =0*030 12*620 =10*494 31*247 55*80 =214*96 26 0*04 18*00 =0*452 14*367 =88*84 35*651 54*43 =223*51 27 =0*01 20*01 =0*753 16*446 =76*132 39*910 54*39 =258*31 28 0*00 21*99 =0*988 18*946 =60*11 44*608 53*90 =2289*05 29 0*00 28*03 =1*416 21*506 =42*23 48*554 51*09 =311*62 30 0*00 28*03 =2*169 28*247 11*98 53*283 =1*75 =233*07 32 0*00 28*03 =2*169 28*247 11*98 53*283 =1*75 =233*07 32 0*00 29*99 =1*639 32*000 21*02 57*681 =8*63 =249*85					0,934	9.157	-105.66	=15.181	-9.72	-87.67
10 0.02 =17.99 0.422 13.886 =70.67 =26.566 =10.08 =29.64 11 0.02 =19.99 0.482 15.964 =60.65 =30.663 =7.91 =6.53 12 0.02 =21.99 0.483 18.373 =50.635 =34.910 =4.94 10.36 13 0.02 =23.99 0.873 21.235 =41.54 #39.205 =1.44 29.57 14 0.02 =28.07 1.717 27.982 =25.92 #47.795 6.07 69.80 15 0.02 =28.07 1.717 27.982 =25.92 #47.795 6.07 69.80 16 0.02 =30.03 2.199 34.687 =16.72 #51.898 11.85 86.08 17 0.02 =0.01 =1.024 5.934 =97.68 5.873 18.71 =156.52 18 0.02 2.01 =1.024 5.934 =97.68 5.873 18.71 =156.52 18 0.02 2.01 =1.024 6.114 =99.00 8.404 24.90 =159.13 19 0.02 3.99 =0.934 6.446 =101.65 10.886 31.15 =161.07 20 0.02 5.98 =0.873 6.898 =105.72 :12.500 35.35 =149.38 21 0.02 7.98 =0.873 6.898 =105.72 :12.500 35.35 =149.38 21 0.02 9.99 =0.120 8.253 =118.99 19.247 47.10 =172.08 23 0.03 11.98 0.211 9.217 =121.87 22.892 51.85 =189.92 24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 25 0.03 15.99 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.651 54.43 =232.51 27 =0.01 20.95 =0.988 18.946 =60.11 44.608 53.90 =229.05 12.90 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.575 =233.07 32 0.00 29.99 =1.639 32.00 21.00 577.681 =8.63 =249.85					0.783	10.542	=94+64	-19-126	-11.03	-67.49
11 0.02 = 19.99 0.482 15.964 = 60.65 = 30.663 = 7.91 = 6.53 12 0.02 = 21.99 0.633 18.373 = 50.35 = 34.910 = 4.94 10.36 13 0.02 = 23.99 0.873 21.235 = 41.54 = 839.206 = 1.44 29.57 14 0.02 = 25.99 1.205 24.361 = 34.08 = 43.494 2.18 47.99 15 0.02 = 28.07 1.717 27.982 = 25.92 = 47.795 6.07 69.80 16 0.02 = 30.03 2.199 31.687 = 16.72 = 51.898 11.85 86.08 17 0.02 = 0.01 = 1.024 5.934 = 97.68 5.873 18.71 = 156.52 18 0.02 2.01 = 1.024 5.934 = 97.68 5.873 18.71 = 156.52 18 0.02 2.01 = 1.054 6.114 = 99.00 8.404 24.90 = 159.13 19 0.02 3.99 = 0.934 6.446 = 101.65 10.886 31.15 = 161.07 20 0.02 5.98 = 0.873 6.898 = 105.72 :12.500 35.35 = 149.38 21 0.02 7.98 = 0.642 7.380 = 111.51 :15.458 40.87 = 152.24 12.20 0.02 9.99 = 0.120 8.253 = 118.99 19.247 47.10 = 172.08 23 0.03 11.98 0.211 9.217 = 121.87 22.892 51.85 = 189.92 24 0.03 14.00 0.331 11.054 = 116.86 27.319 55.75 = 201.38 25 0.03 15.99 = 0.030 12.620 = 104.94 31.247 55.80 = 214.96 26 0.04 18.00 = 0.452 14.367 = 85.64 35.651 54.43 = 232.51 27 = 0.01 20.01 = 0.753 16.446 = 76.32 39.910 54.39 = 258.31 28 0.00 21.99 = 0.988 18.946 = 60.11 44.608 53.90 = 289.05 29 0.00 23.98 = 1.416 21.506 = 42.23 48.554 51.09 = 311.62 30 0.00 26.00 = 1.235 24.578 = 28.46 53.464 41.55 = 326.72 31 0.00 28.03 = 2.169 28.247 11.98 53.283 = 1.75 = 233.07 32 0.00 29.99 = 1.639 32.000 21.02 57.681 = 8.63 = 249.85					0.331	12:048	-81 · 84	=22.717		·=50.50
12 0.02					0.422	13.886	=70 : 67	=26.566	=10.08	=29 +64
13			0.02	=19.99	0.482	15.964	=60,65	=30+663	=7+91	-6.53
14		12			0.433	18.373		-34.910	· = 4+94	10.36
14		13	0.02	:=23.99	0.873	21.235	=41+54	₩39 · 205	= =1+44	29.57
15		14	0.02	25.99	1.205	-24+361	-34.08	-43 - 494	2.18	
17		15	0.02	28.07					6.07	
17		.16	. 0.02	#30 • 03	2.199	31:687	=16+72	=51.∙898	11.85	86.08
18 0.02 2.01 =1.054 6.114 =99.00 8.404 24.90 =159.13 19 0.02 3.99 =0.934 6.446 =101.65 10.886 31.15 =161.07 20 0.02 5.98 =0.873 6.898 =105.72 :12.500 35.35 =149.38 21 0.02 7.98 =0.642 7.380 =111.51 :15.458 40.87 =152.24 :22 0.02 9.99 =0.120 8.253 =118.99 :19.247 47.10 =172.08 23 0.03 11.98 0.211 9.217 =121.87 .22.892 51.85 =189.92 24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 25 0.03 15.39 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.651 54.43 =232.51 27 =0.01 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85	<i>;</i>	17	0.02	≈0.01						=156.52
19 0.02 3.99 =0.934 6.446 =101.65 10.886 31.15 =161.07 20 0.02 5.98 =0.873 6.898 =105.72 :12.500 35.35 =149.38 21 0.02 7.98 =0.642 7.380 =111.51 :15.458 40.87 =152.24 :22 0.02 9.99 =0.120 8.253 =118.99 19.247 47.10 =172.08 23 0.03 11.98 0.211 9.217 =121.87 .22.892 51.85 =189.92 24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 25 0.03 15.99 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.651 54.43 =232.51 27 =0.01 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		18	0 . 05	2.01	=1.05 4	6 • 114				
20 0.02 5.98 =0.873 6.898 =105.72 :12.500 35.35 =149.38 21 0.02 7.98 =0.642 7.380 =111.51 15.458 40.87 =152.24 :22 0.02 9.99 =0.120 8.253 =118.99 19.247 47.10 =172.08 23 0.03 11.98 0.211 9.217 =121.87 22.892 51.85 =189.92 24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 25 0.03 15.39 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.651 54.43 =232.51 27 =0.01 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		19	0.05	3.99						
21 0.02 7.98 =0.542 7.380 =111.51 :15.458 40.87 =152.24 :22 0.02 9.99 =0.120 8.253 =118.99 :19.247 47.10 =172.08 :23 0.03 11.98 0.211 9.217 =121.87 .22.892 51.85 =189.92 :24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 :25 0.03 15.99 =0.030 12.620 =104.94 31.247 55.80 =214.96 :26 0.04 18.00 =0.452 14.367 =89.54 35.651 54.43 =232.51 :27 =0.01 :20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 :28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 :29 0.00 .23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 :30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 :31 0.00 .28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 :32 0.00 .29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		20	0.02	5.98				医髓 医肾上腺 医二甲基甲基二甲基甲基二甲基甲基二甲基甲基二甲基甲基二甲基甲基二甲基甲基二甲基		
122		21	0.02	7.98						
29 0.03 11.98 0.211 9.217 =121.87 .28.892 51.85 =189.92 24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 25 0.03 15.39 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.661 54.43 =232.51 27 =0.01 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		:22	0.02	9.99		8 • 253				
24 0.03 14.00 0.331 11.054 =116.86 27.319 55.75 =201.38 25 0.03 15.39 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.661 54.43 =232.51 27 =0.01 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		23	0.03	11.98						
25 0.03 15.99 =0.030 12.620 =104.94 31.247 55.80 =214.96 26 0.04 18.00 =0.452 14.367 =89.84 35.651 54.43 =232.51 27 =0.01 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		24	0.03	14.00						
26		25	0.03						55+80	-214.96
27 =0.01 : 20.01 =0.753 16.446 =76.32 39.910 54.39 =258.31 28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 : 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 : 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 : 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		26	0.04	18+00						
28 0.00 21.99 =0.988 18.946 =60.11 44.608 53.90 =289.05 29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85		27								
29 0.00 23.98 =1.416 21.506 =42.23 48.554 51.09 =311.62 30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85			0.00							
30 0.00 26.00 =1.235 24.578 =28.46 53.464 41.55 =326.72 31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85	ſ									
31 0.00 28.03 =2.169 28.247 11.98 53.283 =1.75 =233.07 32 0.00 29.99 =1.639 32.000 21.02 57.681 =8.63 =249.85										
32 0.00 29.99 -1.639 32.000 21.02 57.681 -8.63 -249.85	**************************************						.,,			
그는 그								and the second s		
		33.		0.00	=1.054	5.904	-97.55	5.813		

. 15th \$2

VOUGHT LAW SPEED WIND TUNNEL TEST 630

;	RUN	:52			11/1	9/8:	05	707	· · · · · · · · · · · · · · · · · · ·	· p. lpi-p. · · e	<u></u>	RUN 52	
		TEM	- 6,	6 •					Pd	14+6	808	•	•
China in the contract of the c	QPSF	75+00	VF	P8 2	53.10	5	RNF	158	3749	5 •	MACH	0+2252	ani i ani ani ani ani ani ani an
		TOI	T02	103	704	T05	T06	TOT	T08	TOS	T10		
	-,1,4,-3,4,-4,1	0	Q	32	0	0	Q	0	0	Q	0		
		(11	-		714 32			127	1:70	1.13	120	<u></u>	

COLUMN TO THE PARTY OF THE PART	SINO	LE SUPPO	ORT DA	<u> </u>	DATA .	T CaBa	FULL	SCALE DATA
	PNT	.ALPHA	PSI	L/Q	'D/Q	PM/Q	Y/Q	RM/Q 'YM/Q
And the second s	1	: 0.03	0.02	6.900	7.200	-108+76	6.067	19+88 -157+84
	. 2	-2.02	0.02	3.033	7 • 133	-128.69	. 6.333	, 26·26 -16 3655
	3	4-00	0.02	-0.533	7.200	=147.25	6.647	32+84 -166-45
	4	=6 · 01	0.02	#4.300	7.500	=163.56	6:800	40.65 =169.03
	5	≈8+02	0.02	≈8 • 267	7.900	m177 + 17	7 * 3 4 7	· 48 • 67 ≥173 • 86
	6	-10.01	0.02		8 • 467	=188 + 42	7.500	55.51 =180.73
The state of the s	7	-11.99	0.02	-17.767	9.293	€196.17	7.700	62497 =177.20
	8	-14-01	0.02	-22.467	10.600	-205.49	6.900	68 • 25 × 166 • 12
	9			-24.367		-208.61	6.567	71+44 m160+38
	10	#0 . Oi	0.02	6.867	7.233	=108.59	6 + 067	19.65 =157.71
	11	: 2.00	0.02	10.067	7.500	=89+32	5.900	14.82 =153.51
	12	. 4.02	0.02		7 • 673	=69.45	5.533	8 • 91 × 144 • 66
And the second s	13		0.02	16.067	8.067	H51 - 69	+ 4.500	2.77 =136.21
٧	14	7.98	0.02	18.900	8.633	-32.28	5.073	-3.06 -133.67
	15		0.02		9.433		5 . 400	=10.43 =129.50
Carried Company of the State of	1,6	:12.01	0.02	25.840	.10 . 367		5 + 467	=15+66 =125+02
	17	13.99	0.02	28.453	11.833	28.55	5.900	.=23.21 =119.99
	18	15.99	0.02		13 • 1.67		6.713	#33.85 =117.03
- Address of the Addr	19	18.01	0.02		15.580		. 4.533	=30 +58 =129 - 57
	20		0.02		17.187	63.35	4.387	#33 ×09 #135 ×13
	21	22.00	0.02		18.920		4.700	=37.65 =143.50
سيجهر فسنسس بيسيد بالمستوف	22		0.02		20.993	85 + 4 +	5 • 433	#47 •59 #148 • 94
	23		0 .02		22.133	88.71	6.347	-55 060 -147 173
	24		0.02		7 • 233		5 . 287	20.08 -155.42
					**************************************			· · · · · · · · · · · · · · · · · · ·

122

VOUGHT LOW SPEED WIND TUNNEL TEST 630

RUN :53 11/19/81 0907	NUN 53
TEMP 68.	Pd 14+6857
GPSF 75+00 VFPS 253+60 RNFT 15	80156 MACH 0.2251
TO1 TO2 TO3 TO4 TO5 TO6 TO7	708 Tos T10
0 0 32 0 3 4 4	
TO\$ TOS TOS TOS TOS TOS TOS	708 Tos T10 6 0 0 0 7 715 T20

						THE COLLEGE ST. S. AND AND ST. S.				
	SING	LE SUPP	ORT DA	'	LATALI	IL INIDAL	wildle the	SCALE D	VTA.	
•	PNT	.ALPHA	PSI	L/Q	D3 (!	4	4017	RMZQ	. AW\d	
	1	0.00	0.02	6.967	7.246	· STREET	6.100	20.30	-156+27	
	: 2	:-2.00	0.02	3.100		-1次かを学	6 • 100		=157 .80	
	3	-3.99	0.02	-0.533	7.200	-1490/c/	. 6.267		=158+06	
	4	.∞5.99	0 .02	=4 . 133	7.500	=164.82	6 • 5 6 7		=159+90	
V .	5	≈8 •00	0.02	-8.100	7,833	=178 - 24	7.073		=165+24	
	66	≈10.06	0.02	=12.433	8.467	=189.10	7.707		=172.36	
	7	-12.01	0.02	-17.533	9.267	-196.94	7 • 433		=168.78	
		-14.00	0.02	-22.167	10.367	-206.61	6.920	65.97	-162.24	
	9	-15.00	0.02	*24.367	11.133	-210-23	61427	68 • 81	=154.33	
	10	0.00	0.02	6.800	7.367	=105.29	6.033	. 20117	=155+75	
	11	: 2.00	0.02	10,100	7.553	≈85 •50	5,800	15 ∗03	=151 +06	
	.12	· 4 • 0 1	0.02	13,133	7.800	=66.33	5 • 413	10:37	□141•95	r
	.13		0.02	16,033	8 • 133	= 48+79	4 833	4.30	-133.57	
	14		0.02	19,067	8.667		4.900	-3.06	=128 . 85	
	15		0.02			=7.20	5.267	-9.92	=126.44	
	16	11.99	0.02	25.867	10,433	13.51	5 . 447	=15.46	=123.09	
	17	13.99	0.02	28.240	11.633		5.880	=22.90	#122 · 63	
	18	16.01	0.02	29.367	13.327	49 • 04	6.553	=33+99	=116.34	
	19		0.02		15.600	56,58	. 4,300	-28.86	=126.29	411
	20		0.02		17.400		4.200	-30.22	=130.51	
	21	CONTRACTOR CONTRACTOR STATE	0.02		19.000		. 4.400	-34.83	=136+63	
معقده و درست به در 	.22		0.02		20.853		5 . 187	44-18	=141.80	
	23		0.02	34.027	21.967		5 . 500	=50・7ブ	=140.30	
	24		0.02		7 • 307		5 • 887	20.41	=156+25	

		A: DNIW	XES			
RU	Ñ .54	يندو و در	11/19/81 (907	. RU	N 54
	TEM	p. 68.	•	Põ	14.6857	
QP	• • •		3,60 RNF			+2251

A STATE OF THE PARTY OF THE PAR	SING	LE SUPPO	RT DAT	<u> </u>	DATA A	I C.G.	FULL SCALE DATA		
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	P\Y'	RM/Q	· YMZQ
ALL SALES	1	0.00	0.02	=1.533	8+033	24.29	0.100	=2+39	2.68
	2	-1-99	0.02	-7.600	8+300	40 + 26	0.033	* *2.18	2.64
	3	4-01		-14-067	8.833	60.82	0.307	=1.59	0.07
	4	=6.00	0.02	-19.833	9.600	80.22	0.367	ニュェファ	1 + 63
•	5	-7.99	0.02		10.953	83 • 52	0 + 7 0 0	≈0 • 98	=1.92
	6	=10.00	0.02		12.367	84 • 18	1.167	1.00	. =2 . 84
		-12.01	0.02		13.833	98.44	0.960	=0+30	0.09
		-14,01	0.02		15.867	113.31	0 + 420	0 -85	3.17
		=15.00	0.02		16.987	119.52	0 . 133	1:07	4.01
	10		0.02		8 • 133	24.36	0.127	-2.40	3 + 05
	11	2.01	0.02		8 • 100	16.19	0+100	=2 ∗25	2.29
	12		0.02		8 • 167	9 81	0.033	=2.02	2.51
	13		0.02		8 • 333	6.76	=0.033	-2.16	1.79
	14	8.01	0.02		8 • 833	7+44	0.167	- =2074	0.75
	15		0.02		9.600	14.56	0.533	=3.85	1.32
	16		0.02		10.600	32.82	0.800	#4 + 39	1.78
•	17		0.02		11.867	56.28	1.280	= 5 • 45	3 + 47
	18		0.02		13.453	50.00	2.333	■7 • 46	7 • 17
	19		0.02		16.567	=16.23	0.173	-2.70	2 • 35
	20		0.02		18.587	-49.37	-0.367	-0.35	. =0.43
3	21	11.1	0.02		21.533	=72,26	=0.333	1 .86	-3.06
<u> </u>	22		0.02		24.327	=91.93	0 + 433	=1.52	· =3.16
	23		0.02		26.300	=98 +33	1:033	=3.95	0 + 45
	24		0 * 02		8.067	25.71	=0.067	=2.36	3.69

WIND :AXES

TEMP 70. P5 14.6857.

QPSF' 75.00 VFPS 254.08 RNFT 1572614. MACH 0.2251

T01 T02 T03 T04 T05 T06 T07 T08 T09 T10

0 0 32 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T18 T20

0 0 32 32 0 0 1 0 0 0

i aīv	GLE SUPP	ORT DA	ī A	L GATA A	T C.G.	FULL	FULL SCALE DATA		
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	.A\đ	RM/Q	YMZQ	
	0.02	0.02	=1.967	11.833	33,10	0.433	-1.60	1.93	
Ê	-1.99	0.02		12.027	47.22	0.527	=1.64	1 *23	
	-4.02	0.02	-14.433	12.460	64.02	0.600	-1.54	0 • 1 3	
4	=6.02	0 .03	=20.273	13.067	79 • 83	0.533	n1 +68	2 • 15	
· 8	€0.8	0.02		14.200	84 + 92	0 • 733	0 • 03	1.00	
<u> </u>	-9.99	0 .02	=29.967	15.600	83.17	1.133	1 • 16	· ≥1 •33	
7	412.02	0.02	-36.893	17.193	92.98	0 + 867	-0-17	0.03	
	=13.99	0.02	-41.380	18 + 667	96+35	0.407	₩0 ₩00	4.63	
	-15-01	0.02	-44.113	19.900	99.47	0.133	0.41	7.24	
10		0.02	=2.100	11.800	32.80	0.433	=2.57	1.87	
1.1		0.02	3,233	11.833	26.01	0 + 433	=1.39	0 + 7 4	
12		0.02	8.033	11.933	20.79	0 • 400	m0.82	=0.31	
		0.02		.12.133	19,20	0.400	· -0.71	-0.11	
14		0.02	The state of the s	.12.600	20.99	0.733	-1.48	-1-10	
		0.02		13.300	28.55	1.100	-3.23	-1-15	
16		0.02	24.567	-14-233	45.53	1.140	=3 *25	0.39	
17		0.02	27.513	15.313	70.70	1.233	=3.27	3.16	
18		0.02	29.747	16.707	70.38	1.833	=5.12	7 • 85	
1		0.02		19:873	=5.66	0 • 7 4 7	#0.88	0.55	
20		0.02		21.993	=30.10	0.433	0.57	-1.28	
Ž		0.02		24.567	-51.57	0:133	2.65	=5·56	
22		0.02	43.633	27.360	=70.51	0.460	0 ,62	%5•21	
23		0.02	46.093	28 • 967	¤79 ∗65	\$ * 223	-1.67	· @# 45	
24		0.02							
Σ,-		U 1.U Z	=1.967	11.800		Costa		<u> </u>	

WIND AXES

RUN 56 11/19/81 0907 RUN 56

TEMP 70.

PO 14.6857

؞؞ <u>ڹۼ؞؞ٷ؞ڂٷ؞؞؞ڔڔٷٷٷؠڔؠڔ</u> ؞؞؞؞ۄٷؠڔٷ؞ٷڿ؞ٷڿڿٷڿٷڿٷڿ	SIN	BLE SUPPO	RT DAT	<u> </u>	DATA	T C.G.	FULL SCALE DATA		
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	DAA.	. RM/Q · YM/Q	
	1	0.01	0.02	·=3,367	11.980	52+13	1.167	=0.48 : =8.86	
	2	-2.01	0.02	-9.567	12:153	68+50	. 1.173	1+14 = -7+58	
	3	:=3.99	0.02	=16.133	12.527	92.09	1.287	1.70 -7.83	
	4	=6.03		=22,233	13.267	107.12	1 - 133	1.59 -5.57	
	5	-8.00	0.02		14.200	118.08	1,220	2.53 =4.83	
	6	=9.99	0.02	-32.300	15.667	114.65	1.627	2+046-70	
	7	-11.98	0.02	×37.633	17.207	104.80	1,573	3-94 =7-54	
	* 8	-13.98	0.02	-42.687	18 . 887	108.87	1.000	4.21 : =1.50	
	9	-15.00	0.02	-44.400	19+867	106+80	0.880	4.83 . =3.81	
	1,0	0.00	0.02	#3,400	11.867	51.67	1:167	=0.31 =9.99	
	11	: 2.01	0.02	2.033	12.000	42.47	1:333	=0.35 =11.10	
	12	· 4 • 02	0.02	6.700	12.067	35.10	1.367	=0.31 =13.21	
	13	6.02	0.02	11.567	12.333	30.92	1.233	=0.69 =13.79	
	14	7.99	0.02	15.767	12.700	31.59	1.467	-2.39 -12.20	
	15	10.03	0.02	20.633	13.533	32.18	1.600	-3.69 =10.02	
سينه المجانب المحانث التأثيث في إنه الله من منتجاب محابب الإستان	16	:12.03	0.02	25.567	-14-500	31.56	1.533	=3.92 =6.61	
	17	14.02	0.02	29,833	15.633	25.63	1.753	=5.38 =4.81	
	18	16.01	0.02	32.060	17.147	23.80	5.580	=9.39 =3.15	
, , , , , , , , , , , , , , , , , , , 	19		0.02	33,460	20,033		1.333	=5.17 =8.40	
	20	20.03	0.02			≈23·13			
				36,600	22.413	-48.05	1.167		
	21		0.02	39,720	24.767	<u>=65.13</u>	0.767	-1.23 -11.52	
	22		0 (02	43.673	27.567	=76+48	1.160	=1+74 #12+56	
	23	25.00	0.02	46.393	29 • 433	#84+32	1.900	=6.16 - =9.18	
· · · · · · · · · · · · · · · · · · ·	24	=0.01	0.02	=3.367	11.967	51.27	1 • 133	0 • 0 4 • 9 • 53	

WIND AXES

RUN 57 : 11/19/81 0907 : RUN 57

TEMP 70. PO 14.6759

QPSF 75.00 VFPS 254.16 RNFT 1572087. MACH 0.2252

TC1 TC2 TC3 TC4 TC5 TC6 TC7 TC8 TC9 T10

0 0 32 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

0 0 32 32 0 0 1 0 0 0

SING	LE SUPP	ORT DAT		DATA A	T C.6.	FULL SCALE DATA			
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	·Y/Q	RM/Q	. AW\ð	
	> = 0+01	0.02	=2,733	8 • 833	43+63	0.600		8+04	
# 1	-2.00	0.02	-9.133	8.500	63 • 93	0.513	0.87	-7+45	
3	-4.00	0.02	-15.867	9.100	90.83	0.680		· =7×96	
4	=6.01	0,02	-21.433	9.833	110.22	0.687	1 +39	-7.34	
5	=8 + 01	.0.02	=26.373	11:000	116 + 11	0 • 933	1 • 23	=8∗73	
6	49.99		-31.193	12.547	112.69	1.533	2.58	=11.84	
			-37.313	14,227	119.13	1.367	3 • 66	* =6+64	
하다 그리, 의사를 걸었다면서 그 👪	-14+00		-43.073	16:067	132 . 92	1.047	4.21	-5.91	
	-15.00		#45 : 667	17.200	137.67	0.600	4.41	- 3.69	
10	=0.01	0.02	.=2.867	8 • 207	43+66	0 + 633	= 0 •25	7.90	
11	2.02	0.02	2.333	8 167	33 • 94	0.707	-0.29	-10+80	
.75		0.02	7.100	8.300	24.10	0.700	= 0.50	=11:69	
13	6.00	0 1/02		8+567	18.22	0.633	-2.10	.=12.29	
		0.02	16.200	9,000	19:02	0.833	=3.65	-12-12	
15 The Control of the		0.02	20.700		19.18	1.100		7 =9.15	
16		0.02	25.700	10.733	18:40	. 1.113	-5+14	-5.35	
	.14 . 00	0.02		12:067	11:48	1 4667	=7 ∗03	4 - 86	
18	15.99	0.02	32.393	13.700	7 • 87	2.593	=11:07	· -3 -95	
19		0.02		16.607	-41:02	0.787	-5.22	-7.58	
		0.02	The second secon	19.160	-64:45	0.253	-2.76	-8.55	
in The Haller 21		0.02		21.593	-83.41	-0.013	-0.76	-12.24	
:22		0.02		24.473	-96+14	0.500	-3.23	-10.11	
23		0.02		26.313	=103+42	1: 333	=6+74	=10+52	
24		0.02		8.300	43.95	0 . 460_	-0.09	· =7 •50	

H. Commence of the second	RUN	58			11/	19/8	05	07	سائشچمان س		•	RUN 58	
		· TEM	P 7	۰ ۵					PO	14+	6660		
	QPSF	75.00	VF	PS 2	54.2	5	RNF	1.57	7156		MACH	0.2253	
	#	701	102	T03	TQ4	T05	T06	T07	708	TOS	T10	9	ė,
		. 114 . 114	0	32 713	0	0 T15	0	0	0	O	0	•	

<u>, , , , , , , , , , , , , , , , , , , </u>	SING	LE SUPP	ORT DAT	A	DATA A	T C.G.	FULL	SCALE DA	TA	<u> </u>
	PNT	ALPHA	.PSI	.F\đ	.D\d.	PM/Q	Y/Q	RM/Q	· YM/Q	
	1	0.00	.0.00	-3,40 0	8.767	48 + 35	6+567		=161.81	
- 19 1 전 1 전 1 전 1 전 1 전 1 전 1 전 1 전 1 전	. 5	:=2.00	0.00	-9.800	9.067	67.72	6.213		□162·01	
	3	-3.99	0.00	=15,927	91480	93.64	6.633		-164-10	·
Ti (4	-6.00	0.00	=22.267	10.333	115.91	. 6+893		-167.61	
L	5	-8 - 01	0.00	=27.033	11.520	117048	ア・433	50.91		
	6	-10:00	0.00	=31.433	12.873	112:39	8.213		€179•97	· · · · · · · · · · · · · · · · · · ·
	7	-11-99	0.00	₩37.387	14.567	120,45	8.080		#176.32	
	8	-14.00	0.00		16.533	132.35	7.467	74.31	=169 *00	
		-15.00	0.00			136,93	7.433	78,97	=169.64	,
	10	0+00	0.00	=3.500	8.760		6.527	23 • 90	=162.05	
	11	: 2.01	0.00	2.267		36.72	6.353	16.69	≠157 •92	
	:12	. 4.01	0.00	7.093	8.767	27.13	6 • 053	9 + 84	=153.72	
	13	6.00	0.00		9.000	19.82	5.767	3.08	-148.73	
	14	7.99	0.00	15,753	9.367	21.44	5 . 767	=3.97	-141 · 80	
	15		0.00	20.400	10.167		. 6 . 100	=10.94	-139.51	
	16	:12.01	0.00	25,133	11.100	21.23	. 6.000	=16.75	=133.57	
3	17	-14-00	0.00	29.280	12.487	13,66	6.287	-23.80	=128 -52	
	18	15.98	0.00	31.427	14.033	10.78	7 . 167	=31.90	₩123 · 16	
	19		0.00	32.407		=41.29	. 5 . 167	-30+45	=131.31	
	20		0.00	36.120	19.547	-66.38	4 . 800		4135.40	
	21	the contract of the first of the contract of t	0.00	39,893	22 . 100	-84.16	4.500		-148-02	
	22		0.00	43.780	25+033	=101%83	5.953		-150.37	
	23		0.00		26.800	=109.17	. 6.767	=56+35		
	24		0.00	-3.667	8 • 800	47.39	6.333	23.17		

AUN	:59			#1 /3	1/3/8	1 0:	707				RUN 59
	TEMP	7	0.					₽ð.	14*	6660.	
grsf	75+00	VF	PS 2	54 • 2!	5	RNF	r 15	7156	1,	MACH	I 0√2253
	T01	TOS	703	T04	T/05	T06	TOT	708	TOS	TLO	
•	Q	Q		0	٥	Q	0	0	0	Ó	
	T11	Ţ12 0		T14		T16	T17	T18	719 0	OST O	

	SIN	LE SUPPL	ORT DA	T <u>A</u>	DATA A	T C+G+	FULL	SCALE D	VTA
	PNT	.ALPHA	PSI	L/Q	.D\Ø	PM/Q	Y/Q	RM/Q	YM/Q
	1	*0.01	0.00	-3.533	.12+567	56.23	6,033	18.63	=139 *99
	: 2	-2.01	0.00	-9.600	12.633	71,96	6.147	, 24.70	-142-45
<i>/*</i>	3	4.02	0.00	-16.500	-13 - 100	96 • 67	. 6.347	31.36	=144.66
	- 4	-6.01	0.00	=22:367	13.833	111.59	6 : 433	. 37 486	=148+20
	5	-8.03	0.00		14.800	121.94	6.787		=151 +39
	6	-10.02	0.00		16.067	116.27	7.700		=161.62
		-12.03	0.00		17.607	110.07	7.327		-154+16
	8	-14,02	0.00		19.327	105.36	. 6 . 953		=158•76
		-15 - 27	0.00		20.647	107 - 88	6 • 767		=151+9 0
	10	0.02	0.00	≈3,33 3	12.400	54.73	5.500		=141·07
	11	: 2 - 17	0.00	2.300	12.467	45 • 86	5 . 767		=136.63
	12	. 4.03	0.00		12.500	38.44	5 633		≈1 35•46
	13		0.00		12.733	32.99	5 + 700		=133+14
	14	8.01	0.00		13.133	33.67	5.913		=134 • 19
	,15		0.400		13.800	34.55	. 6 . 267		=134.96
	.16	.12.01	0.00	25.133	14.800	34+04	6.247		≈133 •28
•	17	14.01	0.00	29.473	15.900	27:33	6 433		=129.71
	18	15.98	0.00	32.027	17.427	26 • 14	7.333		-125.67
	19		0.00		20.200	≈16.39			=130.93
	20	19.99	0.00	35.820	22.353	=49.03	5 • 8 6 7		=137×10
	21		0.00		24.693	=66.15			=146.64
	.22	24.03	0.00		27.933	=80·69	6.933		=159.07
	23.		0 .00	46.353	29.500	=88.50	7.833		=161+45
	24	=0.01	0.00	=4.067	12.533	56.97	5.873		=139.97
	<u>₩7</u>			<u> </u>	16,000	70.3/	U 1 U / S	47407	-133.31

and the second	()	97 45		
<u> </u>	RUN 60	11/19/81	0907 : RUN	60
	· TEMP	70•	PO \$4.6660	
	QPSF 75.00	'VFPS 254.25	RNFT 1571561. MACH 0-22	53
	T01	102 TO3 TO4 TO5	TO6 TO7 TOS TOS T10	
Statement of the statem	0	0 59 0 0	0 0 0 0 0 0 T16 T17 T18 T15 T20	
	• 70	0 32 32 0	0 1 0 0	

	INC	LE SUPRO	RT DAT	<u> </u>	PATALA	T C.G.	FULL	SCALE D	\TA
F	TN	.ALPHA	PSI	1/0	.D\0	PM/Q	Y/Q	RMZQ	. AW\@
	1	-0.02	0.00	-3,633	12.667	53.38	5 • 833	18.78	
	. 2	-2.01	0.00	-9.833	12.800	70+88	- 6.073	25.21	=139.10
그 전체 이 대학 및 실취 화학생	3	-4.01	0.00	=16.267	13.267	93.83	6.233	30 × 73	m142 = 60
	. 4	-6.01	0.00	=22.333	:13.840	109.09	6.257	37 • 90	=143+92
	- 5	=8.00	0.00	=27.867	14.833	119+78	6.767	46 • 63	≒150 • 03
	6	=9.97	0+00	≡32.040	16.167	115.94	7.507	53 • 46	=158.31
	7	m12.00	0.00		17.720	106.05	7.513	60 473	-159.59
	. 8	-14.01	0.00		19.360	106.57	6.853	67.01	H151 · 81
나는 그 시간에 가면 바로 맞았다.		-15.00	0.00		20.553	105.48	6.700	70.77	=147.26
	10	0.00	0.00	=3.900	.12.667	53,57	5 . 867	19+19	≈137 +64
	11	1.99	0.00	1.767	.12 . 667	44.91	5.707	12:92	4132+85
	.12	4.00	0.00	6.800	12.667	35.98	5 4 6 0 0	7472	≈130.58
	13	5.99	0.00	11.033	12.833	30.99	5.600		-130.72
	14	8.00	0.00		13.280	31.87	5.900	-3.69	
	15	9.99	0.00	19.933	13.960	32.67	6 - 180	-9.97	
	16	12.02	0.00	25.300	14.933	1 31 197	6,100	=15+54	
•	17	14.01	0.00	29.493	16.127	25 • 28	6.367	=22:42	- '
	18	16.00	0.00	32.173	17.767	23.56	7.087		=122+43
	19	18+00	0.00		20.527	-25.39	5.887	=30 ×18	
	50		0.00		22.567	-46 • 39	5.567		-130.88
	21.		0.00		25.300	-72.04	5 • 733		=141 + 10
	52	24.02	0.00		28 • 233	=87.97	6.700	=48,69	
							7.500	=56+94	
	23	25.01	0+00	46.307	29.780	=96·20			4136•60
	24	=0.02	0.00	-3.733	12.700	52.94	5•733	70 400	<u> -130.00</u>

e de la companya de l	FUN	61	· V	11/19/8	0907		RUN 61	
		TEMP	70+		b	PØ 24•6	566Q	
	GPSF	75.00	VFPS 2	154+25	RNFT 157	1561.	MACH 0+2253	
		101	TO2 TO3	T04 T05	TOS TO7	708 TU9	T10	
	25.1	Q	0 59	0 0	0 0 T16 T17	0 0	O	
		Ó		:32 0	0 1	0 0	<u> </u>	

and the second s	SINC	BLE SUPPO	ORT DAT	<u> </u>	· DATA A	T C.G.	FULLS	CALE DATA
	PNT	ALPHA	PSI	٩/١٩	פֿעם	PM/Q	Y/Q	RM/Q YM/Q
· · · · · · · · · · · · · · · · · · ·	1	-0.01	0.00	-3,600	.12.667	53.73	6.267	21+54 -148+76
	2	-4.00	0.00	#10 #167 #16 • 467	12.933 13.200	71+14 93+78	6.520 6.760	. 29+31 #150+65 . 35+60 #154+64
The second secon	4	=5.99	0.00	#21.967	13.833	108 • 86	6.867	42.51 -156.24
•	5	=8.01	0.00	=27.800	14.800	119:39	7.•233	50 +85 ×160 +18
	6	±10.00	0 • 0 0	<u>=32.267</u>	16.500	113.33	8 • 100	59.36 4169.72
	ን 8	=12.00 =13.99	0.00	=37.347 =42.233	17 • 867 19 • 533	105.72	8.000 7.467	67+34 =170+64 73+51 =159+70
	. 9	-15.00	0.00	=44.667	20.600	106.09	7.167	76.81 4158.15
A CONTRACTOR OF THE PROPERTY O	10	0.00	0 + 00	#3 ,600	12:667	53,54	6.300	21.62 -147.91
	11	2.02	0.00	2 167	12.633	44.47	6 • 167	15+19 =145+24
	12	4.01	0.00	6.900	12.600	35.93	5.967	10.22 ×140.43
	13	6.01 8.01	0.00	11.233 15.867	12.833 13.333	31.54 32.10	6.267	-3.32 -140.67
	15	10.00	0.00	20.267	13,940	33.42	6.533	=9.38 =141.18
	16	12.02	0.00	25.367	15.000	31,.63	6.500	-15+28 -137+04
	17	1.4 * 01	0.00	29.767	16 • 193	25.75	6 • 633	=22.87 =133.18
	18 19	16.03 17.99	0.00	32.040	17.633 20.333	22.63 -25.99	7.•267 6.113	=31.00 =128.14 =30.03 =133.62
**	50	50.05	0.00	32.633 36.667	22.907	=52.41	6.067	=34.64 =241.29
	21		0.00	40.213	25 • 167	=71.34	6 • 180	-39.57 -150.17
	22	24.01	0.00	44.000	28 + 233	#88+43	6.880	=49+24 =161+71
	53		0 0 0 0	46 • 667	29.933	= 95•99	7 4 9 6 0	=58+64 =161+99 21+56 =148+36
	24	0.00	0 + 00	=3.533	12.667	53 - 12	<u> </u>	

	· RUN	1 2			11/	19/8	10	207	يعمون والمار والمراجعة	and decimaling outrops		RUN 6	2	***************************************
		TEM	- 7	4 •					PÖ	14.6	6660			
37.00	GPSF	83.00	VFI	9 2	68 • 4	7	RNF	163	758	3 •	MACH	0.237	0	******
		701	102	тоз	T04	TOS	706	TOT	807	TOS	710	O-1 3-4 - 1 1 - 3 - 3 - 3 - 3 - 3 - 3 - 3 - 3 -	.,	
		711	0 T12	48 713	0 T14	0 T15	0 T16	0 T17	0 718	· 0	0 720			

heng ganda katalan da kalan katalan ka	SING	LE SUPP	ORT DAT	<u> </u>	DATA	T C.G.	EULL S	SCALE DA	TA
	PNT	.ALPHA	PSI	.L\0	D/Q	PM/Q	YZQ	RM/Q	YMZQ
THE THE STATE OF T	1	0.01	0.02	-3.645	12.620	54+33	· 6.235	20+89	m147.79
	: 2	Ø + Q <u>€</u>	-2.01	-3.675	12.470	56+02	: 2.139	22472	=135.55
	3	0.01	-4.00	-3.705	12.530	56:91	-2.048		-120-96
(4	0.01		3.193	12.922	49 + 85	₩7.078		=101+04
	5	0.01	≅8 . ∙03	-2.771	13 434	44167	H11+747	21.42	=76.03
	. 6		=10.00	=1.687	14 • 157	37.65	≈16.506	17.06	=47.35
	7		-12.02	-0.181	15.331	26.27	-21.928	12.60	m19.18
	8	0.01	-13.99	1.325	16.988	18+74	-26.928	10.78	13.26
	9		-16.00	2.861	18.976	14.41	•31·584	10.80	45.71
	10		=18.00	3.994	21.235	7:32	#36.386	10.52	77.72
	11	0.01	=19.99	5.151	23.861	=4+85	#41+C54	9.71	105+64
	12	0.01	=22.03	.7.440	27.048	=21.51	=46 · 181	7 * 86	133.40
	13	0.01	-23.99	9.608	30.241	=38·49	.50.873	3.10	156.03
	14	0.01	:#26.00	11.446	33.705	-45.87	m55+416	5.01	175+44
	15		-28.00	13.398	37.018	-55.56	≈ 59.398	7.11	185.63
	1,6	0.01		14.066	40.313	=53.61	#63:151	11 12	192.52
	. 17	0.01	0 • 0 0	≒3 ∗705	12.651	53.67	6 4 3 5 5	20.49	=149*19
	18	0.01	2.01	 #3.855	12.771	50 • 85	9.518		=143.76
i	19	0.01	4.01	-3.886	13.133	47.23	12.952	19.99	=156.70
*	20	0.01	5.99	-3.253	13.675	37+23	17 . 633	27.23	=195.49
	. 21	0.01	8.01	-2.440	14.319	23.88	21.626		=211.45
	22	0 * 0 1	10.02	-1,386	15.211	11.82	25 . 934	33,21	#230.68
	23	0.01	12.00	-0.331	16.265	0.21	30:181	34 432	=249.03
	24	0.01	14:00	0.994	17.651	=11.85	33.374		₩277.75
V.,	25	0.01	16.02	. 2.681	19.398	-25.24	39.570	34.92	=298.47
	26	0.01	18.00	3.765	21.476	=34.02	44.880	36.41	-320.58
	27	0.01	20.02	5,120	24.090	-40.99	50 - 554	39*13	4360 - 95
<i>t</i> :	28	0.01	. 22.01	6.837	27:036	=53.81	56.265	43.09	
l	29	0.01	24.00	8.705	30:181	*66.05	60.594	43.17	-421.79
	30	0 • 0 1	26.00	9.211	34.669	=48.51	62.494		≒362•11
	31	0.01	28.00	10.343	38.602	-49.72	66.717		-381 • 64
	32	0.01	30.01	10.518	42.380	-43 -68	69 675		4382+12
	33	0 + 0 1	0.00	-3.645	12.590	53.81	5.753		=147.32

WIND AXES

RUN 63 11/19/81 0907 RUN 63

TEMP 75. PO. 14.6709

GPSF 83.00 VFP8 268.68 RNFT 1633979. MACH 0.2370

T01 T02 T03 T04 T05 T06 T07 T08 T09 T10

0 0 48 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

0 0 32 32 0 0 1 0 0 1

	SIN	GLE SUPI	OCRT DAT		DATA 'A	T CAGA	PULL	SCALE D	
	PUT	.ALPHA	PSI	1/0	۵۸ď	PM/Q	Y/Q	RMZQ	· YM/Q
	1	. 0.00	0.01	=3.494	12.741	55+49	5 5 9 1 6	20.59	-144-45
	``2	0.00		=3.524	12.620	58 * 13	1.867	22.10	=134.37
	. 3		-4.02	-3.404	12.620	56.15			-175.68
(- 4	0.01	≈ 5∞99	=3.193	12.861	52.26	-6.747	20:97	-103.51
	5	0.01	-7,97	=2.681	13.452	45+74	411.777	19.01	'#75.30
	6		-10.01	=1.476	14.367	37.17		15+94	-45.27
	' 7	0.01	=12.03	0.120	15.602	25.62	w22.289	11.86	=16+24
	8	0.01	-13.99	1.416	17.229		m27.078	9.74	16.01
	9	0.01	-15.99	2.922	19.247		•31 • 558	9.75	. 47.17
	10	. 0.03	-18.00	3,976	21.524	8 + 99		7 • 61	. 80+36
	11	0.07	·-20+04	4.916	24,217	=0.87		9+16	109 12
	12	=0.01	:=22.03	7.108	27 + 289		= 46.380	5 • 67	137+34
	13	0.00	-24.02	9.301	30.602		*51.795	3.35	161 - 25
	14	0.01	25.98	11.175	33.916		#55.873	3.94	
그 요. 그림을 [생각성취]	15		-28 .02	13.193	37.4337		-59.892	4.51	·191 • 22
	16		=29.99	14.337	40.813	=53.98		10+25	199.50
<i>,</i>	17		- =0.01	-3.723	12.831	54.88	64295	19.75	
	18		2.01	=3. 765	12.952	52.57	9 • 639		=142.38
	19		4+03	-3,494	13.253	45.65	13.145		+155+05
그리지 않게 잃어 살씀	20			#3.133	13.633	37+48	17.500		-191+91
	21		8.02	-2.289		24.02	21.705		=211.60
And the state of t	:22			=1.054	15.211	10.53	25.402	32.09	
	.23		12+00	0.120	16.343	=1.89	29.570		=245.42
	24		14.00	1.627	17.831	=13.20	34.795		=271 • 15
	25		16.01		19,518	-26.71	39.898		-296-11
	26			4.295	21.355	#34.70	-44.548		-317.38
	27			5.663	24.126	=41.97			-356.91
<u> </u>	28		. 22+00	7.018	26.988	=52.96	55,873	43.25	
1	29	•		8.825	30.030	-67 · 64	60,723		#415 • 28
f	30		26.01	9.337	34 • 639	=46.87	61.958		=361 + 08
	31			10.512	38.524	49.09	66,434		<u>-381.52</u>
	32		30.02	10.139	42.265	-42.50	69+785		379.03
	33		0.00	=3.825	12.771				=1*4·99
	ټ پ		4100	-21050	16 1/1	56.75	<u> </u>	- T KOO	ニュママギフフ

A-66

Ap #		W SPEED WIND TU	NACE IEST, GAY	ig ig kentre grander om til 1916 i 1918 i 19
and the second s		WIND AXES		
	1 RUN - 64	44.746.79	1 0907	. RUN -64
da di dipatrajaran ya kada ayan ya maja da kada di di di da da 198		***	1 0307	, 1011 104
	TEM	50.	20 14 €	6955
	QPSF 75.00	VFPS 249+16	RNFT 1651425.	MACH 0 - 2251
				the second
نف نست شاند استور برسود بالمار والمساور والمساور والمار والمار والمار والمار والمار والمار والمار والمار والمار	TOI	TO2 TO3 TO4 TO5	TO6 TO7 TO8 TO9	<u> T10</u>

***	NIE	BLE SUPP	ORT .DAT	A	DATA A	T C.G.	FULL	SCALE D	\TA
	PNT	.ALPHA	PSI	L/G	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
	1	0.00	0.01	-4.033	12.767	55.72	6,200	20.82	
, · · · · · · · · · · · · · · · · · · ·	5	0.00		=4.067	.12 * 600	57.39	1.567		=135.13
	. 3		-4+04	-4.033	12.600	57 • 10			-118.26
*	. 4	0.00	≈5 •99	#3.600	12.900	51.02	-7. • 100	. 22.80	=101 =13
	5	0 • 0 0		=3 ∗167	13 • 400	45 • 28	+11 • 600	20.433	' =74
CDD-1001-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	6		=9.99	=2.153	14.367	36.38		16.26	·=47·73
	7		-12.98	-0.767	15.533	: 25.71	#21,933	12.99	=19.11
	8		-13.99	0.600	17.167	19.51	#27.067	11.68	14.05
	9	0.00.		2.067	19 100	15.98	#31.633	10.36	. 46 . 43
	10	≈0.0±	-17.99	3.533	21.353	10:13	#36.700	9.79	79.03
	11	-0.02.	=20+03	4.367	24.100	=1:03	841.713	9.01	110.71
	112	#0.02 :	-21.99	6.567	27.267		m46+600	6+40	:134 040
	13	-0.02	-23.99	8.600	30.640		m51+40	2.73	161 • 86
e e e	1.4	-0+02	-26.00	10.767	34.000	-43.96		3.83	.183.04
	15	MO.02	-28.01	13,467	37.700		-60·253	4.96	
Charles and the second	16	=0.02	=30.01	14.227	41.093		¥63+853	10.56	203.45
· ·	17	×0.02	0.01	=4 + 167	.12.900	56 + 03	6.567	19+34	
	18	-0.02	2.03	=4.200	12.967	53.72			=143.15
age (specification) (8th and a second se	19	-0.02	4.00	-3.933	19.267		13.660	19.17	
	20	#0.02	6.01	-3,233	13.767	36.54	17.933		=196.56
	21			-2.467	14,467	23.45	21.800		-211.64
	22		10,00	=1.233	15.280	9.26	25,933	32.83	
	,23	=0.02		0.067	16.400	=2.75	30:267		-247.63
	-24	=0.02	13.98	1.460	17.800	=15.37	34.913		= 273∙98
	25		16.01	2.900	19.600	-27-89	40.267		=302.42
	26	-0.02		4.167	21.667	=36+84	45-100		-324-65
,	27		20.01	5.400	24.267	-43.02	50 + 800		m363+83
gartest suplementarios superioris superiori	28	=0.02		6.767	27.200	=54.64	56.267		=400+66
(29	=0.02	24.00	9.133	30.300	=68.43	61.100	45.08	=418·31
,	30	*0.05	26.01	10.633	33.567	=81 · 30	66.300		=443+52
	31	-0.02		10.433	38 • 653	-49.35	67.080		=379+64
	32		29.99	10.433	42.107	=41+52	69.900		=375+54
	33		0.00						=145.92
	J J	0 1 0 2	0.00	#3.467	12.787	55.53	6.087	C (% 2) 0	-140.72

WIND AXES

RUN 65

TEMP 62.

PE 14.6955

PE 14.6955

PE 14.6955

PE 14.6955

TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 T10

O 0 59 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

O 0 32 :32 0 0 1 0 0 0

									. 1612 - 기타를 . 1213년 - 기타
81	NGL	ESUPP	ORT DAT		DATA A	T C.G.	FULL	SCALE D	NTA
FN	Τ.	ALPHA	PSI	L/Q	D/Q	PM/Q	P/Y	. RM/9	. AW\d
	1	0.01	0.00	-3.700	.12.833	54.68	6:120	. 21 . 62	-144.32
		-2.00	0.00	m10.033	13.033	72:17	. 6.273		=146.65
	3 .	-3.98	0.00	-16.367	13.400	95.30	6.520		≈151.67
1	4	-6.01	0.00	H22.533	14.067	111.02	6.620		≈153+53
•	5	×8 • 01	0.00	=27.633	14 + 833	119.74	6:853	50+61	
		10.01	0.00	=32.067	16.313	114.73	7.600		≈168•76
		12.01	0.00	-37.413	17.967	108+74	7.520		=165.79
		14-00		=41,667	19.467	101.84	7,053	71.76	₩157.73
		15.01		#42.033	19.533	110.49	6.787		=157.41
1	. 0	0.00	0.00	=3.767	12.867	54+18	6.053	21 = 66	-144-23
		2.02	0.00	1.833	12:733	45+58	5.753	§4.56	=141.08
	2	4.02	0.00	6.600	12.767	36.59	5 . 647	9.60	=138.88
		6.03	0.00	10.967		30.88	5.727	3+93	=140.38
	4	8.01	0.00	15.300	13.367	30.80	6.027		=138.65
		10.01	0.00		14.033		6.433	■9•75	-142.20
The second secon		11.99	0.00	25.100	14,967	32,31	6.267	=15.46	=135 - 89
<u> </u>		14.01	0.00	29.740	16.367	25.04	6 + 8 9 3	-24.26	m134+51
		16.01	0.00	31.947	17 • 687	21.88	7.373	=32.66	=128.93
		18.01	0.00	33,140	20.353	=23.67	6,300	-32-05	=132.91
and the second of the second o		20.03	0.00		22.700	=52.81		⇒34 • 73	=138.97
		21.99	0.00		25.333	=73.38	5.853		≈148 + 64
		24.01	0.00	43,653	28+400	=90+43	6.853	= 52.58	
		25.01	0.00	46.660	30.000	=98 • 49	7 . 687		#161·37
	24	0.00	0.00	=3:800	12 - 833	55 • 66	6.020		=145.64

 RUN 66	11/19/81	0907	RUN 66		
· TEMP	64.	PO 14+0	955		
QPSF 75.00	VFPS 252.55	RNFT 1595961.	MACH 0 -2251		
 * TO1	TO2 TO3 TO4 TO5	TOS TOT TOB TUS	710		
711 711	0 59 0 0 T12 T13 T14 T15 0 32 32 0	0 0 0 0 T16 T17 T18 T19	720 720		

		<u> </u>	0 32	<u> 132 U</u>	<u> </u>		У		
		0 7 04 5				em.	SCALE D	A ** A	
940	GLE SUPRO	KI DAT	Δ	LALA A	T C.G.		JUNEAU D	9.LA	
FNT	.ALPHA	.PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q	
	0.00	0.00	-3.733	12.867	55 . 68	. 5.713	18+85	=135+59	
			=10.300	13.060	73+44	5 . 880		4137.77	
	and the second of the second o		=16.793	13.433	96.44	6.180	A CONTRACTOR OF THE	-140-95	0.1
	=6.00		≈22.467	14.133	111.81	6:193	38 • 65		
<u>(</u>	and the second second		±27.800	14.967	119+94	6.513	46.08	200	
ě			=32.273	16.333	113.56	7: • 247		=155.98	
	12.00		=37.567	17.967	108.24	* 7.047		-154+23	· · · · · · · · · · · · · · · · · · ·
	13.99			19.633	103+87	6.680		=148.67	100
			#42.027	20.400	105.92	6.313		-144-76	
	-15.01		<u>-44.293</u>			5.680	18.76		*****
10		0.00	=3 ,900	.12.900	54+89	5 407	12.90		
.11		0.00	1.567	12.780	46+27		7 + 84		
.12		0.00	6.567	12.767	36.62	5.347		=131.71	
		0.00	11.000	13.033	31.82	5 - 413			
• • • • • • • • • • • • • • • • • • •		0.00	15.500	13.313	32.27	5.747	=4 • 63		
<u> </u>		0.00	19,900	14.120	32.87	6,180		≈134 • 22	
1.0		0.00	25.033	15.067	32.38	6:180	=16.46	-	
117		0.00	29.627	16.333	25 • 22	6.327	=22.98	*	
1.8	3 16 • 00	0.00	31.900	17.673	23.10	7 • 113		=124.11	
14.	17.99	0.00	33.180	20.547	=24.70	- 6 - 100		-127-34	11.0
20	19.98	0.00	35.873	22+713	≈53 ∗35	5.680		=131 88	-
2	1. 22.00	0.00	39.920	25 - 440	-72.02	; 5.780		-141.61	
.2:		0.00	43,460	28 • 080	=86+65	6 • 247		■150+39	
.23		0+00	46 - 673	29.980	-95+94	7. 280	=57 • 11	=153.02	
.24	4 0.01	0.00	=3.800	12.867	55.72	5.613	18:77	=136*10	

 RUN	67	·	<u></u>	11/1	9/8	<u> </u>	107	المنافضين المنافضين		1	RUN 'S)
	TEMP	65	5 ♦				•	Þø	14+6	955	•	
GPSF	75+00	VF	PS 2	52.79	•	RNF	159	2111	3•	MACH	0.2251	
	TOT	102	T03	T04	T05	T06	TOT	80Y	TOS	T10		
	O	0	'67	Q	0	0	Q	0	. 0	Ö		
	T11			T14			Ti7	T18	T19	T20		

NIE	SLE SUPPO	RT DA	FA 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	DATA 'A	T C.G.	FULL	SCALE DA	TA	···
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	. AW\d	
	0.00		=10.400	11.367	50.78	5.487		-135+64	
			-14.300	11.767	76.20	5.747		=138+41	
3			-18-133	12.293	105.38	6.020		=142.08 =149.89	
5	=5.99 =8.01	0.01	■22.000 ■24.700	13.000	132.55 146.63	6.763		=153 ×23	
	=10.02		=25 307	15.033	133 • 16	6.527		4156 • 15	
	412.01		-26.767	16.147	132,49	. 6.633		-152.66	
	-14:00		-28.233	17:367	129 82	6.247		-147.52	
	-14.99		=29.073					=143.58	
10		0.01	-10.433	11.333	50 + 28	5.367	18 • 87		
11		0.01	=6.700	11.000	25.38	5.333 5.133		≈132∗16 ≈130∗28	
12 13	6.02	0.01	0.000	10.700 10.567	4.38 -15.97	5,000		₩130.21	
	8.00	0.01	3.600	10.567	-39+74°			-133-85	
15		0.01		10.567		5.400		₹135.27	
16		0.01	11.233	11+100	=94·42	5.367		≒135 • 95	
17		0.01	14,233	12.000	-107+14	5 • 467		×135 • 71	
18		0.01	16.200	12.967		5.467		≈138.22	
19		0.01	18.133	14.167	-109-10	5.580		=141.63	
20		0.01	19.567	15.267		4.673		=134.86 =132.40	
21 22		0.01	22.033		=103.77 =101.95	4.547 · 4.340		=132 · 10	
23		0.01	23.167	18.800		4.567		=126+40	
24		0.01		11.400		5.367		w134 · 38	

-			OF POC	r qualti	7	A-70)	
	The second	JGHT LA	W SPEED	WIND TUN	INEL TES	630		
			WIND A	AXES				
	RUN 68			11/19/81	0907		RUN	· 68
		TEMP	74.			PØ 14+6	955	
	apsf 10	701 0	0 67	T04 T05 0 0 T14 T15	0 0	TOS TOS	0	2599
SING	LE SUPP	ORT DAT		DATA	AT C.G.	FULL	SCALE D	ATA
PNT	.ALPHA	PSI	L/Q	DVG	PM/Q	Y/Q	RM/Q	· YM/Q
	=0.01 :=2.00 =4.02 =5.99 =8.00 =9.99	0.02 0.02 0.02	-10.500 -14.075 -18.550 -21.975 -24.200 -25.080	11.675 12.175 12.800 13.675	76*29 111:32 133.63 143:19	\$ 5.250 \$ 5.550 \$ 5.850 6.260 6.520 6.515	26 • 10 • 34 • 31 • 42 • 50 • 49 • 14	<pre>=134.38 =138.48 =143.57 =148.45 =154.18 =153.91</pre>
7 8	-0.01 -0.01 2.00	\$0.0 \$0.0	=26.395 =10.500 =6.600	16.085 11.325	130.80 . 51.51	6.200 5.165	60•49 19•45 12•30	=150.50 =135.08 =133.02

10.625

10.450

10.475

11.000

10

11

12

13

4.00

. 5**.**99

7.97

10.00

0.01

14. .11.99

0:02 =3,325

0.02 11.200

0.125

3.425

0.02 7.450 10.575

0.02 =10.300 11.230

0.02

0.02

7 - 48 = 129 - 34

2.87 =130.97

=2*76 **=133***78

18 - 80 - 135 - 40

6.07 . 4.925

. 5.010

#67.13 . 5.060 #7.97 #135.54 #91.70 : 5.375 #13.93 #136.28

=16+11 . 4+775

50.83 : 5.125

=37.13

in to a second s	· · · · · · · · · · · · · · · · · · ·	VEUGHT LE	W SFEED WIND T	UNMEL TEST 630	the state of the s
			WIND AXES	a ki i kanimus aling alikahaka kapus minja di kanimus pengala da pina da sa masa da sa kanimus anda da sa masa	and the state of t
	RUN	69 .	11/19/	81 0907	RUN 69
		TEMP	75.	Fa	14 • 6955
	QPSF	75+00	VFP9 255+19	RNFT 1554537	MACH 042251
tering the second se	·		TO2 TO3 TO4 TO		TU9 T10
		T11	0 59 0 T12 T13 T14 T1 0 32 32	0 0 0 0 5 T16 T17 T18	T15 T20

appillangs and the supply of the last the second	SING	LE SUPPO	RT DAT	<u> </u>	DATA 'A	T Cag.	FULL	SCALE DA	TA
	FNT	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RMZQ	· YM/Q
·	1	-0.01	0.00	-3.700	12.833	56.86	. 5.380		#132+34
	2	:-2.02	0.00	-9.667	13,033	74.34	5 647		-134.75
	3	-4-01	0.00	m16.067	13.367	96.40	5.733		×138.36
	4	-6.00	0.00	*21.867	14:000	110.57	5 • 7 4 7	38.38	=140.75
\	5	-8.00	0.00	=27.467	14.867	119:25	5.993		=140+36
	6	=10.02	0.00		16.247	113.70	6 • 493	53.01	-152.01
	7	H12.01	-0.00	-36.833	17.993	101.53	. 6.333	58.67	-148.73
•	8	-13.99	0.00		19.493	103.94	5 . 687	65.37	-142+53
		=16.02	0.00	-45.527	21.700	103.79	5.213	73.77	=140.39
	10	=0.02	0.00	=3.633	12.800	56.50	5,373	19.86	H133.95
	11	2.02	0 + 0 0	2.367	12.767	47+68	5.193	13.22	=131+04
	12	4 • 01	0.00	6.800	12.767	40.09	5 - 113	8.62	■129•18
The state of the s	`13	6.01	0.00	11.467	12.900	34.37	5.200	3 * 65	-129 - 74
	14	8.02	0.00	15.633	13.300	34.13	5.613	#3.08	-128+75
	15	10.01	0.00		13.933	35.59	5.967		≈131.58
ساعب والمتحدد	16	.12 • 02	0+00	25.333	14.833	35.22	5,680		≈128.85
,	17	14.01	0.00	27.920	16 • 660	13.29	6.547		=123:06
	18	16.00	0.00	30.987	18 133	13.59	7 • 1 4 7		=120:15
	19		0.00	33.313	20.467	-21.10	5,580		=127.39
	20	20.01	0.00		22.633	-51.56	5,547		=132.42
	21	22.03	0.00		25.360	-72,57			×139.09
	.22		0.00		28.213	-89:05	6.700		×150 · 23
		25.00	0.00	46.467	30.500	=96 157	7.347		*155+82
	23					57 · 04	5.313		=133.71
~~~	24	0.00	0.00	±3.533	12.867	5/104	21212		7197164

*10.54 *128.40

=14.23 =125.80

=24091 ×118.01

-31.57 -147.61

-31.51 -127.10

.=34.06 =130.18

--41+74 ×136+39

#48+45 #150+97

≈53+94 ×152.62

18.13 -129.91

37.38 5.867

36 - 23 > 5 - 567

16.47

=68,77

-83.91

-92.37

59.26

16+64 . 6+633

-20.66 · E.953

-47.89 : 5.567

7.000

> 6 . 100

6 4 4 8 0

7:133

5.200

·	₩8 • U €	A CONTRACTOR OF THE CONTRACTOR	A-72	
· · · · · · · · · · · · · · · · · · ·	SUGFT Law SPEED	WIND TUNNEL TEST	630	,
3, 5				
	WIND A	XES		-
RUN 7		<u> 11/19/81 0907</u>	RUN	70
	TEMP 78.		P6. 14.6857	
GP8F	75.00 VFPS 25	5.99 RNFT 154	3036+ MACH 0+	2251
de la companya de la	0 0 59 T11 T12 T13	0 0 0 0 T14 T15 T16 T17 32 0 0 1	0 0 0	
SINGLE SUP	PORT DATA	DATA AT C.G.	FULL SCALE D	ATA
PNT .ALPHA	PSI L/Q	D/Q FM/Q	Y/Q RM/Q	. AW\d
1 0.00 2 =1.99 3 =4.01				=128 • 66 =130 • 67 =134 • 02
4 =5.98 5 '=7.99 6 =10.01	0.00 =22.000 0.00 =27.633	13.767 112.15 14.633 121.14 16.067 110.16	5 • 733 37 • 79 5 • 867 44 • 46	=138+02 =140+03 =150+03
7 =12.01 8 =14.01 9 =15.01	0.00 =37.100 0.00 =41.400	17.613 106.91 19.187 104.65	. 6.180 59.96 . 5.713 64.78	*145 •63 *142 •62 *138 •88
10 0.00 11 1.99 12 4.00	0.00 =3.767 0.00 2.100	12.467 58.43 12.500 50.03	9.200 18.13 5.060 12.25	#129•11 #126•41 #124•99
13 : 5.99 14 8.02	0.00 11.333	12:633 35:38	; 5.020 2.06	=124.76 =125.12

15 10.00

20 20.01

23 -24+98

24 . 0.00

16

17

18

19

21

22

:12.02

14.01

15.99

.18.02

22.02

.23.99

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.00

0.000

0.00

19,933

25.300

28 . 187

31.187

33.360

36.567

39,373

43.440

46.100

<u> =3.767</u>

.13.633

14.567

16,293

17.873

20.267

22.313

24.860

27.867

29.533

12.467

, 57 k#1-6 a =

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND :AXES

	SING	LE SUPPL	SRT DA	A	DATA A	T. C.F	FUL	SCALE DA	LTA
	PNT	.ALPHA	PSI	L/0	.D\d	PM/Q	.Y/@	. RM/Q	· YM/G
	1	-0.01	0.00	=3,633	13.567	62.05	. 5.700		-132.90
현실에 보고 이 사람들이 보고 말았다. 생물과 보고 있다. 그 사람들이 보고 있다.	2	3-5.05	0.00	-9,633	13.933	78.91	5.807		=133.62
	, 3	-3.99	0.00	-14,900	14.600	101.96	5.487		=131.80
7	· 4	=5.98	0+00	=20 ±000	15.733	116.72	5 • 467		=131.96
	: 5	-8.02	0.00	24 9547	16.967	124.59	5,313		=129+25
	- 6	-10.01	0.00	-27.640	18 • 840	109.70	5 • 173		=131.74
	7	412.01	0.00	-31.533	20.500	110.28	4.500		=133.26
	. 8	-14:02	0.00	-35.560	22 • 253	110.57	4 . 827	60.66	4132.46
	. 9		0.00		23.293	112.24	4.867	64.41	#132.28
	10	:=0.01	0.00	⇒3 ,567	13 + 533	60+65	5 . 667	18 - 24	=132.71
	11	: 2.05	0.00	2.167	13 . 267	馬1 - 63	5.667	11.45	=132.05
	12	. 4.01	0.00	7.067	13.300	42.36	5 • 667	6-19	=131.46
	13	6.01	0.00		13.467	35.92	. 5.700	1.11	=131.78
	-14	8.01	0.00	16.967	13.900	35.02	5 . 833		=130-14
	15		0.00		14.600		. 6 • 133		=133.86
	16	11.99	0.00		15.467	38.61	5.720		≒130•39
,	17	13.98	0.00	29 140	17.033	19.29	6.467		=121 .86
	18	16.00	0.00		18.667	17.60	7 • 187		=118+92
	19		0.00		21.000	-11+64	6.533		=127 • 86
그리고 하는 이번 바다 살아.	50		0.00		23.060	-44.49	and the second of the second		4132.85
	The second second	21.99	0.00		25.647	=69.94	6.073		=136.88
	22		0.00		28.500	=87·18	6.467		=147.75
			0 • 0			=97 :17	6 • 833		-155.91
	23			, -	30.467		5 • 6 6 7	· ·	±132 · 21
	24	0 • do	0.00	=3.967	13.533	61.58	<u> </u>	101/4	-13C1

WIND AXES

TEMP 84. P8 14+6562

QPSF 75.00 VFPS 257.67 RNFT 1519934. MACH 0.2254

T01 T02 T03 T04 T05 T06 T07 T08 T09 T10

0 0 59 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

0 0 32 32 0 0 1 0 0 0

	INC	LE SUPPL	ORT DA		DATA A	T C.G.	FULL	SCALE D	MA .
P	NT	.ALPHA	PSI	L/Q	·D/Q	PM/Q	Y/Q	RM/Q	' YM/Q
	1	0.00	0.00	=3. 700	13.600	61:58	5 . 707		#130·96
	. 2	-1.99	0.00	-9.467	-14.067	78.98	5.787		=134.00
	3	:=3.99	0.00	-14.700	-14-733	101057	5.653		=132.93
	. 4	-6.03	Q • Q Q	=19.967	15.867	116.31	5 • 253	35 87	#130 • 37
	5	-8.01	0.00	=24.567	17:060	124+85	. 5.020	41+20	#126 • 16
	6	=9.96	0.00	-27.113	18.880	109.39	4 * 7 4 7	45 • 77	=127•31
		-12:01	0.00	=31.540		107.52	. 4,353	52+84	=127.01
		-14+00	0.00	#35.900	22.340	110.86	. 4 . 167	59+79	=127.49
		-15.00		-37.467		109.73	4.247	64.02	=130.30
	10	0.00	0.00	=3.467	13.520	60.59	5 • 687	17+69	=131.28
	11	: 2.00	0.00	1,933	13:400	50 + 35	5.547	11.17	-130•91
	12	4.00	0.00	7.133	13.300	41.39	. 5 · 460·	. 6.39	#130 • 69
	13	5.99	0.00	12.067	13,433	34.32	. 5,653		=129+58
	14	8 + 00	0.00	17.367		34.51	5 . 887	-4.91	=127.53 ·
	15		0.00	22.067			6.053	and the second s	m131.48
The state of the s	16.		0.00	26,633	15.567	37.59	5 + 463		=130+06
,	17	14.02	0.00	29.220	17.267	16+43	6.613		
•	18	15.99	0.00	32.000	18.533	21.11	7.320		=118.56
	19		0.00				. 6 . 7.53		=126.53
	50	20.02	0.00	37.800		-42.78	i 5.587	and the second of the second o	=131 • 64
	21	:55.05	0.00			=66.06	5 . 900		-141.21
	22	.24.02	0.00			=86 • 75	6:120		=152.44
	23.		0.00	45.733	30+300	=98+47	6.720		=154 • 74
	24	=0.01	0.00			60.83	5.533		=131 • 13
					~				

WIND AXES

sī	NG	LE SUPPO	ORT DAT	^	DATA A	T C.G.		FULL	SCALE D	VTA
PN	T	.ALPHA	PSI	L/G	D/Q	PM/Q		'YZQ	RM/Q	' YM/Q
	1	0+00	0.00	-3,100	9,833	53.30		6.233		-153+09
하다 그 전에 살아 있는 그는 바람이 나는 그리 회사를 다 먹었다. 그리 없다 나는 그를 다 살아 없다면 살아 싶다면 살아 없다면 살아 싶다면 살아요. 얼마나 살아 싶다면 살아 싶다면 살아 싶다면 살아 싶다면 살아 싶다면 살아요. 얼마나 살아 살아 살아 살아 싶다면 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아요. 얼마나 살아 살아요. 얼마나 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아요. 얼마나 살아 살아 살아 살아요. 얼마나 살아 살아 살아	2 3	=1.99 =3.99	0.00	-8.933 -14.633	10.333 11.107	72+37 99+5 <u>4</u>	•	6.133	. 29 • 04 34 • 44	And the second s
• (4	-6+00	0,00	=19.707	12.313	121 • 11		5,667	39 • 76	
.	5 6	-7.99 -10.00	0 + 0 0 0 + 0 0	= 23.220 = 26.940	14 • 033 15 • 767	120 • 77 111 • 65		5 + 5 6 7 5 + 233	52 • 25	
그 것 : 그는 그는 그는 그는 이 시 의 전 경기가 있는 사람이다.	Tr. 100	-11.98 -14.00	0.00		17.513 19.467	122.47		5.020 4.760		=149.47 =144.62
	9	=15.01	0.00	=38.88 0	20.460	.137 • 49	•	4.500	70.49	≈153•13
	0	2.01	0+00 0+00	#3.167 2.633	9.800	51 ± 91 39 ± 45		6 • 167		=152°53 =150•61
. 1.	2	4.00	0.00	7.900	9 • 600'	30.00		5 • 833	6 . 78	=147+04
	3	6.01 8.00	0.00	12.700	5.800 10.233	23.05 23.46	* *	5.760	≈ 5∗66	=142.40 =136.76
	5	10.00	0.00	22.500	11.000		Ŧ	5.733		≒135∗44 ≒129∗07
	6	11.99 14.01	0 • 0 0	26.500 30.567	11.967 13.400	23 · 21 13 · 71		5.793	=22.37	=124+84
	8	.16.01 .18.00	0.00	32.567 35.200	15.327 17.873	9.11	•	6 • 173 4 • 860		*121 • 17 *127 • 59
	0.	-20+03	0.00	38.020	-20-153	-57.80		4.300	-32.16	=131.89
	1	21.99	0.00	41.333. 44.533	22 • 667 25 • 893	=83.04 =105.23	·	4.367 5.100	=44+94	
.2	3.		0 + 0 Q 0 + 0 0		27.327 9.873		i	5.500		=144.38 =152.51

original page 13 of poor quality

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										,			
	Yeug	iht L	DW SP	FED	WINI) TUN	NEL	TES'	r 63	0			
			WI	ND :	AXES								
	RUN 74				11/	9/81	1:	146			. RU	N .7	
		TEMP	P 64	•				ť	PØ.	14+	6464		;
	gesf 75.	00	The second						1985 1998 1998		MACH 0	*235	
ada situa _{nanan} nya sirantsia sistemata di disembalan di di teribulah di	ekali ili sasa ya mili alama ugu sa	7.02	0 T12	.74	O	0	Ø	0	Q	, 0	0		
AMER	SATYPE BUF			EL_	0.	NTA Z	AT C	.6.				DATA	
PNT	ALPHA	PSI	<u></u>	_/ Q	. [Q/Q		1/0	• ·	 Y/Q			YM/Q

PN	T .ALPHA	PSI	[一/四	D/Q	PM/Q	Y/Q	RM/Q	. AW\ d
	-0.00	= ♥*76	-2.033	11.300	26.48	. 6,213	22.70	=158.20
	2 -2 - 05	-0.76	-8.167	11+733	46+10	6.367	. 26.08	=158.55
	34.02	-0.76	-14.700	12:367	70.29	6 . 147	33.45	-153.59
	4 =6.05		=20.40C	13.333	89.37	5.867	39.50	=145+94
	5 -7.92		⇒25 • 467	14 + 333	100.50	5 1 6 0 0	47 #40	=136 . 62
	6 -10.04			15.900	75.91	6 * 167	56 (31	=144.96
	7 -11.98	-0.76	-33.133	17 • 600	73.16	6.533	74+15	#153·44
	8 -0.00			11.347	26,75	5 . 867	23.27	=157:02
	9 . 2.01	-0.76	· · · · · · · · · · · · · · · · · · ·	11.100	15.36	5 . 667	15.57	=153.52
1	0 . 4.03	= 0.76	7.900	11.000	7+69	5 • 533	7.69	=148.32
1	1 5.98	= 0.∗76	12.033	11.000	3.90	5,507	1.88	=140.70
.1	2 : 8 . 01	=0.76		11.300	6 • 55	6:033	-7 • 30	=136.78
	3 9.99	-0.76	20.667	11.767	9,27	6,013	-13.58	=131.41
	4 :12.00	-0.76	24.093	12.913	≈3.48	5 9 5/67		=121.56
				11.433	25 • 15			=157.59

WIND AXES

RUN 75

TEMP 73.

PU 14.6464

QPSF 75.00 VFPS 255.14 RNFT 1559320. MACH 0.2254

TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 T10

7.02 0 75 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

. %:			ere e								y 1.
. ندست		AME	SETYPE	SUPPORT	+MODEL	DATA AT	C.G.	FULL	SCALE DA	TA	
		PNT	.ALPHA	PSI	L/Q	.D\d	PM/Q	YZQ	RM/Q	. AWN	
		1	0.01	· =0;77	-1.767	11.000	20+54	0:167	1.65	⊃13∙50	
e Satisti		2			-8.047	11.400	39 - 25	0.167	0.31	- =9+64	1. 1.
•		3	-3.99	= =0.77	m14.300	11.933	62.75	0.133	2 • 18	=6.27	
•		4	.=6 e 0 6	0.77	-20,233	12.967	82.00	=0 • 1 0 0	3.28	· - 5+39	
Altern 1		5	-7 . 90	=0.77	=24.873	13.980	93,51	=0 ±347	7.33	#1 • 32	
		6	=10,05	-0.77	#27.880	15.753	69.38	■C • 16 7	13+04	- =3.93	
		7	H12,01	-0.77	-33.333	17,487	71.95	0,133	14.61	3-71	.*.
4		8			-1.567	10.967	20.56	0.100	1.96	=11.69	•
1/2		5	3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		3.367	10.833	10.03	6.133	0.16	-15.80	
سبنيد	***************************************	10				10+733	5 : 87	0 + 487	=1.71	:=21:17	
		.11	5 . 96		12.300	10.733	1.78	0 : 767	=3 ∗06	=24+14	
	•	12				10,933	4.78	1.500	=7+34	=27.30	
		13		The Contract of the Contract o	and the state of 	وبالمراوعة بالمراوع ووجوات والمراجعة فأناث فاستباطع والمالة	6.72		-8.65	:=25.77	· · · · · · · · · · · · · · · · · · ·
						- 10 - 177 - 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			= 9÷44	=13.61	11,114
*		14					1 21		2+34	-11.81	1.5
		15	=0.00	-0.77	-1.567	11.000	22.25	0.000	. <u></u>		

A	VOUGHT LOW SPEED WIND TUNNEL TEST :630
gyayan miney yagaddirii isti amii filmilaya aada ka qaaqaysha biriya ayaa iya ka saabiilii a	WIND AXES
X	
444	RUN 76 11/19/81 1346 : RUN 76 TEMP 75. PO 14.6464
	TEMP 75. PO 14.6464 OPSF 75.00 VFPS 255.62 RNFT 1551937. MACH 0.2254
	TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 T10
	7.02 0 75 0 0 0 0 0 0 0 0 T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

	AMES	TYPE 8	UPPORT	HODEL	DATA A	T C.G.	FULL	SCALE DA	IA	
	PNT	.ALPHA	PSĮ	٠٢/٥	D/Q	PM/Q	.A\đ	RM/Q	YMZQ	•
	1	. 0.01	-0.77	-0,633	10.920	1.07	-0.273	0.75	: 42,48	
	. 2	2.03	-0.77	-6.667	11.300	16+10	-Q:167	#1 * 59	· -1 • 11	
	3	-4.02	-0:77	m12.633	12.033	33.65	-0.200	-1.07	-0+29	
-	. 4	=6 · 05 ·	=0.77	=18.367	.12 .800	51.21	-0 + 460	1 + 65	3.87	
	- 5	¥7∗91	= 0.77	=22.600	14.033	53+39	-0.520	6 . 42	6+35	
	6	=10.04	=0.77	=26.467	15 • 633	42.47	=0.200	9.06	1 • 14	
	7	-11:98	+0.77	æ31.933	17.100	50 • 75	0.100	11.22	-0+94	
	8	-0.00	-0.77	-0.433	10.900	1.06	-Q . 333	0.21	=2+44	100
	9	2 2.01	-0.77	4,433	10+633	-6.78	-0.453	0 452	: =4.66	
· ·	10	· 4 • 04 ·	=0 477	9.067	10.567	=8.77	-C+167	=0.25	=8:64	
	11	5 . 98	#0.77	13.100	10.600	=10+57	0.047	#0 • 48	-9.78	
	12	8.01	=0.77	17.367	10.967	=7.37	0.733	=3.60	=12 • 12	
	13	9.99	=0.77	21.233	11.400	0.94	0+967	-6.30	=12.68	
	14	11.99	-0.77	.24.493	12.533	11.77	0.533	=6.70	-8+87	
	15	0.02		-0.533	11.067	#0+56	≈ 0.767	1.81	-2.89	Right.

There are a second and a second	and the second s	OF POOR QUALIT	rY A→75	
-22.	VOUGHT LO	W SPEED WIND TU	NNEL TEST 630	45.5-habita (1-2-habita) 1-2-habita (1-2-h
		WIND AXES		
	RUN 77	11/19/8	1 1346	RUN 77
	TEMP	90.	· PÖ 14:	6071
<u> </u>	QPSF 75.00	VFP8 259.52	RNFT 1496366.	MACH 0+2257
a sidden hag had his had been been a second and the			TO6 TO7 TO8 TU9	
	702 T11 0	0 77 0 0 T12 T13 T14 T15 0 1 1 0	0 · 0 · 0 · 0 T16 T17 T18 T19 0 1 0 0	n+
	AMES-TYPE SUPPORTS	+MODEL DATA	AT C.G. FULL	SCALE DATA
•	PNT ALPHA PSI	L/Q D/Q	PM/Q 'Y/Q	KW/d . AW/d
CANADA CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONTRACTOR CONT	1 0.02 0.02		≈136.66 ₩0.587	
			-158+87 0+767 -181-33 0+833	
Co.	# =6.06 0.02 5 =7.91 0.02	#2.933 9.833 #6.267 10.300	=200.62 =1.340 =216.25 =1.967	4.59 6.69 8.27 13.56
And the state of t	6 ±10.04 0.02	<u>-10.133 10.953</u>	<u> </u>	

9:12 7 -12.02 0.02 -15.200 12.067 -541.49 :-2.167 16.61 4+04 0.01 -1.000 3.12 8 0.02 8.233 9.167 -139.14 5 .02 3.61 9 1.99 0.02 11.500 9.200 -116.05 -1.100 1.93 · =0.19 10 · 4.07 0.02 14.530 9.333 **493.91** =0.833 2.25 . =0.93 9 4 4 6 7 **≈0:633** 11 5.97 0.02 17:267 'm71 .73 =1 -69 =2.15 12 8+00 0.02 50.300 9.900 49.21 0.007 ×4.97 0.500 13 9.98 0.02 23.567 10.507 -1.74 -26.19 :12.03 -6.27 1.46 . 14 .0.02 26.273 11.433 -3.63 0.487 3-84 2.92 15 - WO . OO 0.02 8.200 9.200 #136.93 =0.967

	VI	SUGHT	LAW	SPEED	WIND	TUNNEL	TEST	630
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WIND AXES

TEMP 94. PC. 14.6071

OPSF 75.00 VFP8 260.47 RNFT 1482623. MACH 0<2257

TO1 TO2 TO3 TO6 TO5 TO6 TO7 TO8 TO9 T10

7.02 0 75 0 0 0 0 0 0 0 0 0 0 0 0 0 1111 T12 T13 T14 T15 T16 T17 T18 T19 T20

0 0 1 1 0 0 1 0 0 0

PN	Ţ	ALPHA	PSI	L/Q	.b\d	PM/Q	DAA.	. RM/Q	YMZQ
	1	-0.00	0.02	-0.600	10.433	12.41	=0.733	3,47	3.63
고 있는 것이 되었습니다. 그 사람이 되었습니다. 그런 것이 되었습니다. 그 것이 없습니다. 	2	-2.04	0+04	-6,633	10.867	15.06	-0:467	2.72	1.80
	3	-4.01	0.04	#12.333	11.487	30.31	-0.453	4.18	1.36
	4	=6.05	0+04	m18.333	12.400	49 425	-0.833	3.59	5.76
,	5	=7.91	0.04	=22.640	.13 + 467	53.94	-1.460	7 +93	10 • 79
	6	=10.03	0+04	-26.867	15 • 133	46.90	=1.987	7.68	14.82
	7	-12.01	0.04	-32.200	16.800	60.34	-1:767	9,08	. 11.59
고, 기계 대한 왕이 남자 현기를 보려가겠다고 있는 것인 발표시 나는 사람들이 아니라 하는 사람들이 되었다고 있다면 하는데	8	0.02	0+04	-0.300	10.367	1.41	-0,767	3,38	1 *83
레이탈하다. 그모든 하면 존재하다.	9	: 2.00	0+04	4.533	10.167	4.96	-0.867	3 • 5,9	1.72
1	0	. 4.03	0+04	9,167	10+167	=8 - 57	-0.767	1. • 45	1.37
1	1	5 • 98	0+04	13.367	10 • 133	=8+94	-0.50Q	1 443	· =0 *00
1	2	8 * 00	0.04	17.633	10 • 433	=5.75	0.033	=1.36	0 (37
	3	9.98	0.04	21.600	11.033	1.28	0.500	-4-12	· =0.56
	4	:12.00	0+04	-24.453	11.967	13,85	. 0.413	-3.96	2 • 48
	5	0.01	0+04	=0.633	10.367	-0.25	=0.833	3.52	2+94

		•	WIND	AXES				
, the second of						· · · · · · · · · · · · · · · · · · ·		
ila etainini interiore eta eta eta eta eta eta eta eta eta et	RUN	79	·	11/19/8	1 1346	·	: RUN 179	
		TEM	94.			PO 14+6	5071	
and for a transfer of the first of the first of the first of the second section of the first of	GPSF	75.00	VFPS	260.47	RNFT 148	12623.	MACH 0.2257	
		T01	T02 T0	3 TO4 TO5	T06 T07	TO8 TO9	TIO	
		7.02	T .		- m	0 0	0	
		Tit	T12 T1:	3 T14 T15	T16 T17	T18 T19	T20	

	AMES	S-TYPE 8	UPPORT	9+MODEL	DATA A	T C.G.	FULL	SCALE DA	TA
	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	. RM/Q	· YM/Q
- Mark Carlos de Constantes d	1	0.13	0.01	1 -1.433	10.533	19.30	·=0 · 133	6.45	: ≠9+75
	. 5	E0.5=	0.01	-8.067	11.000	38.52	0 . 040	6.48	8.32
	3	-3.99	0.01	-14.267	11.600	60.75	0.133	6.65	-8-14
7	· 4	=6+06	-0.01		12.533	80.81	= 0.533	7 • 4 4	· =3+54
L ,	5	-7.90	= 0₩03	=24.967	13.567	91.98	=0.900	9+56	2 + 79
	6	=10∗04	₽0+03	=28.480	15 + 300	111.09	≈1 ,533	10.95	4+82
- 1	7	-12.01 ·	-0.03		16.967	.118+09	-1.033	11+84	2 • 26
; f	8	0.02	-0.03		10.600	18.95	-0.333	6.38	· #8 · 13
$v = \frac{v}{v}$	9	1.99	-0.03		10.333	12.41	-C.420	5.90	.=10.97
<u> </u>	10	. 4.01	=0.03		10.233	6,60	=0:167	1+69	=12.93
	11	5.98	=0.03	12.600	10.333	3.08	0:033	1+24	=13:47
	12	8 • 01	=0.03	17.000	10 + 633	4.93	0.633	=1 *77	=12.78
	13		-0.03	the party of the p	11+167	6 . 53	0.800	=3.72	#8.49
No.	14	:12.02	-0.03	Andrews and the second	12.167	3.78	. 0.167	-0.71	. 44.46
	15		-0.01	-1.633	10.540	18.90	-0.473	5.91	. 48.61

ORIGINAL PACE IS OF POOR QUALITY

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VOUGHT	LOW SPEEL	WIND TUN	VEL TEST 630

WIND LAXES

RUN	80		11/1	9/81	1346	, sila Marinda	· ·		RUN 80	
	. TEMP	90.				PC	14+	5973		
qPSF	75.00	VFPS	259.61	RN	FT 14	95863	•	MACH	0 • 2258	
	TO1 1	102 TO	3 704	T05 T0	6 TQ7	T08	109	T10		1,450
	7.02	0 7	4 0	Q	0 0	0	0	Ö		
	Tity	r12 T1	3 T14	T15 T1	6 T17	T.18	715	T20		
	·" O	0	1 1	0	0 1	. 0	1 0	0		

AME	SETYPE	SUPPORT	B+MODEL	DATA AT	C+G.	FULL	SCALE D	NTA
PNT	.ALPHA	A PSI	L/0	D/Q	PM/Q	YZQ	RM/Q	. AW\o
	0.0	2 -0.01	-1.700	11+033	22.81	5.133	28.34	-156.99
	: =2.03	30.01	8.067	11.433	41.48	5.367	34+24	=158 = 59
	-3.9	9 -0.01	-14.400		65 . 40	1 5.393	41.50	=158.52
. 4	F =6+0;			12.987	85 . 08	5 140		-158+51
	7 -7 -94	4		14.033	95+33	4 680		*155 • 74
6	=10.04	4 -0.01	=28.300		74 • 55	. 4 . 100		=145.25
	-12.04		-33.200		77.29	4,827		-149+30
	0 . 0 :			11.067	22.54	4 . 833		=155+86
	2.0	The state of the s			12.76		and the second of the second o	=153.09
1 (10.733	6+76	. 4.600		=147.42
11			12.500	10.833	2.75	4 633		=142 • 70
12			16.900	11+167	5.97	5.233	-2.80	
				11.633	8 • 08	5.547		=139.91
			्राम्यक्तिर (क्रांटर ग्रा	12.573	4+06	4 4667		=134+53
					22.77	4.667		-155.30

original pace is of poor quality

A-83

				4	•			
		•	······································				والمرابع وا	ajang in niangan kapangan panahin spinahin nadi b
S	Yau	GHT Le	W SPEED	WIND TUN	INEL TES	r (630		
4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4 (4						,		, ,
			WIND :	AXES				
Maria Ma			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			,		
\(\text{\$\cdot\text{\$\cd	RUN B1		·	11/19/8	1.346		: RUN	81
		EMP	90.			PO 14.5	5973	
tarian da anti-anti-anti-anti-anti-anti-anti-anti-	GPSF 75	•00	VFPS 2	59,61	RNFT 14	95863,	MACH OF	2258
		tor	T02 T03	TO# TOB	T06 T07	T08 TU9	Tio	
Marka Marka (1945) and a single		7.02	0 81	0 0	0 0	0 : 0	Ö	
		T11	T12 T13	T14 T15	T16 T17	T18 T19	T20	
Carlos Ca		<u> </u>	<u> </u>	1 0	0 1	0 . 0	9	year in land in this transport when the first transport
	Ç	•			e e e e e e e e e e e e e e e e e e e			
AME	S-TYPE SU	PPORTS	S+MODEL	DATA	AT C.G.	FULL	SCALE D	ATA
PNT	ALPHA	bsi	L/9	D/Q	PM/Q	PVY.	RMZQ	PVMV
	0.02		7,900			. 4.700		

34Mlu46944411		<u> </u>		<u> </u>									
	PNT	.ALPHA	bsi	L/9	D/Q	PM/Q	'YZQ	RM/Q	DVMY				
	1	0.02	. =0.01	7,900	9+600	=130-85	. 4.700	: 26.30	~150.83				
	2	-2.04	-0.01	4.000	9 • 633	m154+44	5 . 067	31,38	×154+86				
<i>y</i>	. 3	-3.99	-0.01	0,433		-173.00	. 5 . 133	38-05	=153.98				
	. 4	≠6 • 05	₩0.01	=2.967	10 - 113	=191 . 86	4 4 9 6 7	43.29	m153 • 16				
	5	′=7 • 92	≠0 • 01	=6.30 0	10.633	=209.71	4 + 500	52+00	*144+49				
	6	m10:04	#0 • 01	-10.300	11.400	=228 • 07	4 : 333	59 + 58	H143.77				
	7	-11.98	-0.01	#15.100	12.267	#234.96	. 4.533	68.00	= 144 + 59				
	8	-0.00	40.01	7.800	9.567	#134+83	4 • 653	26.20	*152.89				
	9	2.00	=0.01	11.000	9 • 633	-114.00	4+220	20:51	#146 eQ9				
	10	4.02	₩0.01	14.000	9.700		. 4:067	12.72	M139.43				
	11	5.98	≠0.01	16.867	9 • 933	=69.54	· 4 • 033	7.80	#132+95				
	.12	8 * 01	=0.01	19.967	10.333	= 46.21	4 . 700	⊭2 ∗38	≈129.70				
	13	9.98	-0.01	23.087	10.933	=23.71	5.120	w9.73					
1	14	:12.02	-0.01	25.533	11.833	11.00	4,500	F12+97	-128 . 47				
	15	-0.00	-0.01	7.800			. 4.667		=151+32				

200.7	•	Ye.	UGHT Le	W SPEED	WIND TUN	INEL TES	r 630		
				WIND .	XES				
1		RUN 82			11/19/81	1346		RUN	
			TEMP	80+		,	PO. 14+	5973	
		GPSF 7	5.00	VFPS 2	57.24	RNFT 15	31157.	MACH OF	2258
			701 702 711 0	0 82	704 TOS 0 0 T14 T15	T06 T07 0 0 T16 T17	TOS TOS 0 0 T18 T15	T10 0 T20 0	
	ANE	3≟TYPE 8		#MODEL	DATA	Vizana.		SCALE D	
	PNT	.ALPHA	PSI	L/ Q	.D/@	PM/Q	P\Y	. RM/Q	· YM/Q
	1 2 3	-0.03 -2.05	=0.01 =0.01 =0.01	=1.067 =1.800 =2.500		=123.38 =139.96 =157.79	- 4.500 4.967 5.167	33+05	=148.72 =155.81 =161.05
	# 5 6	=6:05 =7:91 =10:03	=0.01 =0.01 =0.01	=3.200 =3.967 =5.000	8 • 700 9 • 067		5+500 5+673 5+887	50 • 62 62 • 15	=165.35 =174.17 =183.41
	7 8 9	-0.00 -0.00 1.99		=6.033 =1.000 =0.067	8.133	=205+56 =120+93 =106+79	. 5.633 . 4.433 . 4.133	27 • 11 19 • 90	=178•12 =150•76 =142•93
THE RESIDENCE AND ADDRESS OF THE PARTY OF TH	10 11 12	. 4.02 : 5.98 : 8.02	=0.01	0 * 833 1 * 700 2 * 667	7.900 7.700 7.700	=92.20 =76.30 =57.85	3 • 9 0 0 3 • 6 6 7 3 • 8 3 3	. 0.21	=134.30 =133.27
No. 10	13 14	9.98	=0.01 =0.01	3.600 4.500	7.700 7.833	=39.36 =21.20	44500		=136+05 =142+40

<i>P</i>	and the same of th	And the same		Vaught I	OW S	PEED	WIND	TUN	NEL	TES	630	<u></u>			
					W	IND A	XES								
	1.		***************************************	, , , , , , , , , , , , , , , , , , , 			ur Ur			4		, n			
	- Micardon distriction		RUN	£ 3			11/1	9/83	13	146	·		: 5	N	.83
				ŢE,	MP 7	7 •		.·		i.	PØ.	14+5	5973		
		1.	GPSF	75.00	ΥF	PS 2	56,52	. 45	RNF	15	2019	•	MACH	0 42	258
	2						704	T05	T06	TOZ			T10	<u> </u>	· · · · · · · · · · · · · · · · · · ·
				7.0 T1	2 0 1 712 0 0		0 T14 1	0 T15	716 0	T17	718 0	T19	0 T20 0		
		1 450	. .					.				eln e	SCALE	E DA	1
			.ALPH	SUPPOR A PSI)/Q		1/0			RM/		YMZQ

ТИЯ	.ALPHA	PSI	L/Q	.D\d.	PM/Q	Y/q	RM/Q	· YM/Q
	0+01	-0.01	-9,567	9.553	10.22	4.833	. 29.18	~153.46
	-2.03	-0.01	-13.033	10.133	37+63	5:067	35.22	-157.31
	-4.01	-0.01	-16.900	10.733	70.99	5.313	42.17	=162.28
4	.=6 ⋅ 05 ·	#0.01	#20.733	11.480	99 + 42	5 • 473		-164•15
5	-7.92	#0.01	=22.433	12.607	105.87	5 4 4 6 0		=167 • 15
6	-10:05	0.01	■23.600	13.800	101.90	5.667	75 • 23	=173.26
	-12.01	0.01	-25.733	15.080	109.05	5.833		=181 • 27
	0.01	0.01	-9.433	9.500	10.45	- 4.700	28+44	=154.61
9.	: 2.00	0.01	-6.000	9 • 100	-15.77	. 4.533		4150.62
10	. 4.03	0.01	=2.600	8 + 833	≈ 37 • 66	4.367	13 * 25	=144.88
11	5.98	0.01	0.600	8.567	= 57 • 97	4 4 3 6 7	5 ∗73	=145 • 17
:12	8 • 01	0.01	3.800	8.353	= 78 • 22	. 4 . 467	=1.08	=144·12
1.13	9.99	0.01	7.500	8 • 333	#100+54	5,007	-8+79	=147.37
	:12.00	0.00	11.167	8 • 667	-124.33	5.300	.=15+99	#152.63
15	-0+00	0.00	-9.567	9.533	and the second s	4.700	: 28-50	-153.76

Company of the Compan	OUGHT L	JW SF	PEED	WINI) TUN	UNEL.	TES	r 631	2	.	7 ·	
		W	IND	AXES								,
AUN -		•		11/	19/8	1 1:	346				RUN 84	
	TEM	7:	L e				;	PB	14.	5973		
QPSF	75.00 . 701 . 702	T02	TO3	TO *	T05 0	*70 <u>6</u> 0	T07	708 0	709 0	T10 0	0 * 2 2 5 1	
AHES-TYPE	• 0	0	1	1	0	716 0		0	· C	<u> </u>	E DATA	

AMES	-TYPE	SUPPORT	S+MODEL_	DATA	AT C.G.	FULL	SCALE DA	\TA
PNT	.ALPHA	, PSI	L/Q	ĎΛď	PM/G	Y/Q	. RM/Q	. AWNd
	0.01	0.00	-0.933	7.667	=124+60	=i.233	6+14	-3:68
2	-2.04	0.00	-1.667	7.933	=143*62	-1:000	5.46	-5.08
- 1974 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 198 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 1985 - 198	-4.08	0.00	-2.300	8 • 167	-159.86	=1.027	6.99	=6.61
. 4	=6.05	0.00		8 • 433	=178+73	-1.220	8 • 18	=3.52
5	7-7.91	0.00	=3.633	8 . 833	-193.00	-1.567	11.80	0.61
6	-10-05	,	=4.573	9.233	-206.55	:=2.033	13.41	3 ÷09
7.	-12.01	The second secon		9 . 800		:-2,300	14.05	7.02
	0.02				a123.58	-1:233	6.54	-3.82
	2.00	And the control of the control of		The second secon	-108.31		5 • 45	. =3.02
10	. 4.02			7.400		=1.400	3.97	-2-52
11	5.96			7.+267	=74.96	-1.500	3.29	41 •32
.12	8.00			7.167			1 • 35	: =0 •54
	10.02			7.200		-1:167	0.36	-1.21
		Daniel Albert III		7.367		-0,993	-1-09	2.71
1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1			and the state of t		-124.92		6.40	

OR	GINAL	PAGE	3
OF	POOR	QUALI	TY

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Company of the second						**************************************
	Ye	UGHT LAW SPEED	WIND TUNN	EL TEST	30	aparatagana da arang da jawa arang da
		WIND W	XES			
	RUN 8		11/19/81	1346		N 285
•		TEMP 73.		P. 6	14,5973	•
	apsr 7	75.00 VFPS 25				*2258
The second section of the second section of the second section		702 0 82 T11 T12 T13 0 0 1	0 0	0 0	0 , 0 0	
	AMESATYPE E	DUPPORTS+MODEL	· DATA 'AT	c.c.	FULL SCALE	DÀTA
	PNT .ALPHA	PSI L/Q	D/Q	PM/Q	Y/Q RM/G	YM/Q

	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
	1	0.02	0.00	-0.900	8 • 467	-123.86	- 4.647	. 28.28	=149+76
	. 2	:-2.03	0.00	-1,633	8.600	-141+71	5,233	33.13	=160.38
	3	-4.01	0.00	-2.333		=158.01	. 5 . 467	42.41	=165+24
	4	=6.06	0 + 0 0	-3.067		=176+80	5 : 733	52+04	=170 •15
	5	7-7-90	0.00	=3.833	9.433	=189.16	5.980	63.36	=178+25
	6	=10.04	0.00	4.833		=196.66	6 • 167		=186 • 03
	7.	-11.98	0+00	-5.867	10.507		5 . 633		=180+74
	8	0.01	0.00	-0.933		-124.35	. 4.50C		=151 · 26
	9	2.02	0.00	0,033		-109.05	49147		=145.76
	10	· 4 • 63	0+00	0.900	8 • 167	-92.9 4	3 . 887		w139.46
	11	5.99	0.00	1.800	7 • 933	=77+08	3.700		=138 • 21
	.12	8 • 01	0.00	2.667	7 • 933	-59.17	3.900		⊭139•57
•	13	9.98	0.00	3.667	7.967	=40+87	. 4,300		=144+11
	14	112.00	0.00	4.567	8.033	-24.55	4,633		=148.00
	15		0.00	-0.833		=125 • 37	. 4.500		+152.42

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VEUGHT LAW SPEED WIND TUNNEL TEST 630

WIND .AXES

RUN 86			11/	19/8	<u>.</u> 13	346				RUN B6
TEMP	7	∵ •					PO	14.	5875	·
그리는 이 경찰되었다. 그 살로 살아 얼마를 생겨가 되는데										0 * 2259
TOL	TOZ	103	704	T05	T06	TOT	7.08	TOS	T10	
7.02	Q	81	0	. 0	. 0	0	0	. 0	0	
₩ 4.	712	713	T14	T15	T16	T17	718	Tis	T20	
0	0	1	1	O	<u> </u>	1	0	0	Ó	

	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	YM/Q
	1	0.03	0.00	8.533	9 • 933	=133+79	. 4:453	. 26+30	*152*33
	2	:=2.05	0.00	4.567		=157.09	· 4+733	30 €92	=154.48
	3	-4.01	0.00	1:100		-176.08	. 4.800	37.41	=153°19
(4	-6+05	0.00	=2.633	10.567		4.500	45 - 15	
Sec.	5	=7.92	0+00	=5,833	10 . 880		4.020	52,59	*144*11
	6	-10.04	0.00	=9.933	11.793		4.033		=143.70
	7.	-12.01	0.00	m14,400	12.633		4,033		=144+45
	8	0.02	0.00	8.567		=136.38	4,427		=150.73
	9	2.01	0.00	11.767		-114.41	4.033		□145•14
	10	4 . 04	0.00	14.700	10+167	-93.47	3.800	14,28	
	11	5.97	0.00	17.200	10:173	=71.97	3+980		≈135 - 12
	12	8 + 01	0.00	20.367	10.567	=47.18	4 • 633	=2.09	
	13	9.98	0.00	23.667	11.300	-25.70	5 • 113		#133.03
	14		0.00	25.760	12.267	=3.05	- 4.633		×133.97
	15		0.00	8.467	10.033		. 4.400		=150+49

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	.VOUGHT	LOW SPE	ED WIND	TUNNEL	TEST	630
_						

WIND AXES

RUN 87 11/19/81 1346 RUN 87

TEMP 56. PO 14.5973

QPSF 75.00 VFPS 251.46 RNFT 1621816. MACH 0.2258

TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 T10

702 0 75 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

AM	E.S.	TYPE E	<u>IUPPORI.</u>	#HODEL	DATA	T C.S.	PULL	SCALE DAT	A
Ph	17	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	YM/Q
	1	0.02	≈0₹02	-0.100	10.733	-1.64	*1.1 53	5.37	=2456
	2	-2.04	-0.02	-6.233	11 • 153	12+25	#0.827	4 • 53	-0.48
	3	-3.99	-0.02	-12.067	11.733	29 - 72	-0.920	4 • 87	*2.09
	4	=6:05	≈0.02	=17.900	12 + 607	47 + 95	=1:120	7.08	3.13
•	5	-7.90	=0.02	=22.333	13.800	49.72	=1.0853	11 - 49	7 • 53
	6 .	10.05	=0.02	-26.733	15.393	45.35	-2.120	11.20	9 • 05
	7 .	12.00	-0.02	-32.353	17.120	53 • 65	:=2.253	14.76	10.83
크리	8	0.01	-0.02	-0.033	10.767	=1 + 31	-1.087	4.59	- 2 - 83
	9	2.01	-0.02	4.900	10.500	=7.78	-1.367	5.69	-1.98
	.0	. 4.03	=0.02	9.300	10 + 400	=10.09	≈1 • 120	4 + 6 4	-4+11
1	1	5.98	=0.02	13:467	10 + 467	=11.81	#Q.767	3+04	■4 • 9 4
1	12	8.01	=0.02	17.900	10.767	=8∙27	=0 • 120	=1.45	=5 ∗71
	3	9.98	-0.02	21.900	11.400	=0.37	· 0:247	=3.87	· -3.72
• • • • • • • • • • • • • • • • • • •		:12.02	=0.02	25.060	12.233	13.20	0.047	=2.97	=1.26
	15	0.01	-0,02	0.000	10.767	-2.32	=1 . 187.	5+64	-0.72

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A-90

4.68 - =2.41

4 . 48

3.86

#0#80

5.42 . -2.96

-5.70 - =5.00

- =5.74

228.3		/BUGHT L	JW SPEE	D WIND TU	NNEL TES	r:630		•
	Sage 1		WIND	AXES				
	RUN I			11/19/8	1 1346		: RUN	88
		TEM	60.			PO 14.	5973	
	GPSF	75.00 T01 702 T11	T02 T0	252.43 23 TO4 TO5 8 0 0 3 T14 T15	0 0	0 ' 0 108 104	0	258
AM PN		SUPPERT	B≠M o del L/0		AT C.G.		SCALE DA	TA 'YM/Q
	1 0.02 2 =2.03 3 =4.03 4 =6.05 5 =7.9	2 -0.01 -0.01 -0.01 -0.01 -0.02	=0,60 =6.60 =12.30 =18.20 =22.66	00 -14-533 00 -14-833 00 -15-273 00 -16-100	5.93 18.31 31.31	=0:787 =0:433 =0:467	5 • 85 3 ° 42	
	6 =10.00 7 =12.0	E0.03	≠27.65 •33.03	3 18 633		=2.047		14.31 12.80

13 9.99 -0.03 -3:32 : -5:65 21.733 15.200 .9.29 0.833 14 :12.00 -0.03 *2.87 = 2.44 24.800 16.193 22.63 0.567 0.02 -0.03 -0.633 14.600 4.98 5.46 -C+800

14.533

14.267

14 . 167

.14.200

14.600

6+14

-0.41

-3.79

1.05

·#0 . 707

#0:633

0.500

-Q:267

1.52 #0.900

-0.500

4.467

13.100

17.567

9.067

. 8

9

10

.11

12

-0.00

4.03

8.01

: 2.01

. 6.00

m0.03

₩0.03

#Q#Q3

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A-91

							SEL TES			
Tel Nelson and Section 1988	A17-1-	og posport i vision a	and the same to t		WIND.	AXES			the state of the s	
	estandining the state of the st	<u>؈ۦڋڔڋڞڟڿڂڛڔڂڴڔؙڿڴ</u> ڬ	RUN I	19		11/19/8:	1 1346	to the state of th	: RUN	489
				TEM	63,			Pd 14+6	5071	
***************************************	(1 		QPSF	75.00	VFPS 25	53+07	RNFT 15	14997•	MACH 0+2	257
				TOI	T02 T03	TQ4 T05	T06 T07	TOS TUS	TIO	
	-	, delenia, e terretat per	· · · · · · · · · · · · · · · · · · ·	7.02	0 88	Ο Ω	0 0	Q , C	O	
				T11	T12 T13	T14 T15	T16 T17	718 T19	T20	
1.91				Ö	0 1	1 0	9 1	<u> </u>	Ó	
	1.1	AME	SETYPE	SUPPORT	RAMONET.	DATA	AT C.G.	±្នារ i	SCALE DA	\†* <u>\</u>
ensul (sevol	***************************************				SALINDER	<u> </u>	<u> </u>		000000	\
		PNT	.ALPH	A PSI	170	D/Q	PM/Q	D\Y'	RM/Q	· YM/Q
		1	-0.0	5 · =0+ 03	~1.933	14.700	26-12	=0,267	7+34	-12 - 23
		5	:=2.0		-8.000	15.000	40 +83	0.100	6+29	-11-99
P"	***************************************	. 3	×3.9		=14.367	15.533	62,93	-0.133	7 < 12	1 -9 -89
.		· #	=6 • 0			16.333	74 • 43	=01600	10.25	#3+45
		5	·=7.9		-25.200	17.327	83.51	=1 • 160	11.85	3.02
nysanana		6	=10.0		=28.640	18.907	65.24	<u>=1.567</u>	13.81	6 • 6 (
		7.	#12.0	0 =0.03	#33.333	20.340	59.10	#1.487	14+24	6+96
	1	8	0.0		-1.600	14.700	24.77	·=0+160	7.01	-12.5
نجسينس	***************************************	9 10	2.0			14 • 487	17.81	·=0.133	6+05 4+39	=17.0
		11	5.9		8,100	·14 • 367 14 • 433	14+65	0•133 0•633	2 : 82	=18+3/ =18+8(
		:12	8 • 0		16.567	14.733	11+42 13+88	1.233	#1.73	=18.71
	, 	13	9.9		21.500	15.300		. 1:433	#4 o 4 6	=14·98
			12.0	2 -0.03	25.027	16.240	12.66	0.800	=2·14	* #8 • 7
		15		E0:03		14.633				=12 • 1
***************************************	ar marakat maraki tabun ma r	- in proceedings		B						
	•									
***********	,			······································	, H				teri — transferite de la companya d	
			2.		*	A.	Angela D			
	سرن و مساوعات المراض المسام	عهان سيسين		,				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		

ORIGINAL PACE IS OF POOR QUALITY

A-92

-0.567

-0.533

-0,433

15.71

7.56

E6.E

7.21

6-14

5 + 15

-10-16

=14.51

=16.34

	airong the grains of human palayan payers and he had no high quality before his payers the common the grain appear	Or Foots &		A-92	· · · · · · · · · · · · · · · · · · ·
a	Yaugh	T LOW SPEED WIND	TUNNEL TEST 6	30	
		WIND .AXES			
	RUN 90	11/1	9/81 1346	: RUN	90
	•	TEMP 68.	P ਦੌ	. 14.6071	
والمراقبة والمراقبة والمستقبة والمستقبة والمنافقة والمراقبة والمستقبة والمستقبة والمستقبة والمستقبة والمستقبة	QPSF 75.0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		. 4	257
dan disember, mengerina dikadah diangan kemindisi sebebah didik beba		701 702 703 704 702 0 75 0 711 712 713 714	0 0 0	0 0	The state of the s
والمرافقة	AMES-TYPE SUPP		TA AT C.G.	FULL SCALE DA	T)
igi mingiya di karan di panganan pangana panganan panganan pangan di Salahan (2) di pangan			PM/Q	.A. KW\o	. AW\6
	2 -2.03 -0	+03 =7.639 11	367 34.45 -	0.533 7.34 0.327 6.86 0.333 7.27	=10.60 =11.47
(4 =6.06 =0 5 =7.90 =0	*03 ±19.933 .12.	900 77+36 = 100 83+67 =	0:933 10:60 1:367 11:76	=8.72 =2.60 1.61
And the second distances and the second				1.787 12.80 1.400 13.92	5 • 8 6 0 • 4 8

11 5.99 E0.03 12.600 10.567 0.033 3.11 -16+60 0.36 8.01 12 **#0**∗03 17.133 0 . 567 =1.08C 10.933 -17.56 2 . 65 13 9,99 -0.03 **-3.79** 21.633 0.733 11.547 -13.03 2+24 14 12.00 -0.03 25.467 -1.71 -4-20 12.400 0.533 -6.82 15 0.01 E0 003 7 - 28 . =9.46 -1.267 10.967 -0.600 16.21

20.967

10.700

10.633

. 8

9

10

-0.00

4 . 02

2.00

#0.03

#0.03

₩0.03

-1.467

. 3.700

8.413

		୍ଦ . V8	UGHT L	AW SPFED	WIND TU	NNEL TES	7 :630		
				WIND	AXES				
			· · · · · · · · · · · · · · · · · · ·	W	a juli			**************************************	
		RUN 91	كان وجا كسور مساول فيمانس كاما		11/19/8	1 1346		RUN	91
•			TEM	5 . 45 t		,	PO 14.	6071	
		GPSF 7	5.00	VFPS 2	55 • 2.4	RNFT 15	60937.	MACH O.	2257
			TOT	T02 T03	TO# TO5	TO6 TO7	108 TOS	T10	
			7.02	0 74	0 0	O O	0 3 0	Ó	
			T11	T12 T13	T14 T15	T16 T17	718 T19	720 0	
	AME	S-TYPE S	UPPORT	SAMEDEL	SAYA	AT C.G.	. FULL	SCALE D	ATA
	AME:	S-TYPE S	UPPORT PSI	S&MODEL_	P\Q.	AT C.G.	FULL:	SCALE D	ATA YM/Q
		.ALPHA	•	L/Q			P/Y	: RM/Q	
	PNT 1 2	.ALPHA 0.01 :=2.04	PSI =0.03	L/Q =1.300 =7.667	'D/Q .11.360 .11.767	PM/Q 21:05 40:47	'Y/Q 5+173 5+400	: RM/Q : 29+16 : 34+84	*YM/Q *159*17 *161*59
	PNT 1 2 3	.ALPHA 0.01 :=2.04 =4.02	PSI =0.03 =0.03 =0.03	1.300 -7.667 -13.900	11.360 11.767 12.267	PM/Q 21:05 40:47 64:45	'Y/Q 5+1/73 5-400 5-513	: RM/Q : 29.16 : 34.84 41.26	-159+17 -161+59 -163+33
	PNT 1 2 3	.ALPHA 0.01 =2.04 =4.02 =6.05	PSI =0.03 =0.03 =0.03	1.300 -7.667 -13.900 +20.000	.11.360 11.767 :12.267 13.333	PM/Q 21:05 40:47 64:45 82:05	Y/Q 5+173 5+400 5+513 E+267	: RM/Q : 29.16 : 34.84 : 41.26 : 50.18	**************************************
	PNT 1 2 3 4 5	0.01 -2.04 -4.02 -6.05 -7.90	PSI =0.03 =0.03 =0.03 =0.03	1.300 =7.667 =13.900 =20.000 =24.887	D/Q .11.360 .11.767 .12.267 .13.333 .14.333	PM/Q 21.05 40.47 64.45 82.05 94.45	Y/Q 5+173 5-400 5+513 E:267 4:900	: RM/Q : 29.16 : 34.84 : 41.26 : 50.18 : 59.35	YM/Q =159+17 =161+59 =163+33 =163+13 =154+95
	PNT 1 2 3 4 5 6	.ALPHA 0.01 2.04 2.04 2.05 2.05 2.90 2.005	PSI =0.03 =0.03 =0.03 =0.03 =0.03	1.300 =7.667 =13.900 =20.000 =24.887 =28.200	D/Q 11.360 11.767 12.267 13.333 14.333 16.180	PM/Q 21.05 40.47 64.45 82.05 94.45 71.30	Y/Q 5+173 5-400 5+513 1 5+267 4+900 4+567	29.16 34.84 41.26 50.18 59.35 67.09	YM/Q =159+17 =161+59 =163+33 =163+13 =154+95 =152+69
	PNT 1 2 3 4 5	.ALPHA 0.01 :=2.04 =4.02 =6.05 =7.90 =10.05 =11.98	PSI =0.03 =0.03 =0.03 =0.03 =0.03	1.300 -7.667 -13.900 -20.000 -24.887 -28.200	D/Q 11.360 11.767 12.267 13.333 14.333 16.180	PM/Q 21*05 40*47 64*45 82*05 94*45 71*30	Y/Q 5+1/73 5+400 5+513 日:267 - 4:900 - 4:567	29.16 34.84 41.26 50.18 59.35 67.09 75.45	YM/Q =159*17 =161*59 =163*33 =163*13 =154*95 =152*69
	PNT 123 456 78	.ALPHA 0.01 2.04 2.04 2.05 2.05 2.90 2.005	PSI =0.03 =0.03 =0.03 =0.03 =0.03 =0.03	1.300 -7.667 -13.900 -20.000 -24.887 -28.200 -33.033	11.360 11.767 12.267 13.333 14.333 16.180 17.500 11.373	PM/Q 21*05 40*47 64*45 82*05 94*45 71*30 74*00	7/Q 5+1/3 5+400 5+513 5+267 4+900 4+867 +5+000	RM/Q 29.16 34.84 41.26 50.18 59.35 67.09 75.45 29.56	*159*17 *161*59 *163*33 *163*13 *154*95 *152*69 *154*70 *158*54
	PNT 1 2 3 · 4 5 6 · 7 8 9 10	.ALPHA 0.01 :=2.04 =4.02 =6.05 =7.90 =10.05 =11.98 0.02 1.99 4.02	PSI =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03	1.300 -7.667 -13.900 -20.000 -24.887 -28.200 -33.033 -1.433	D/Q 11.360 11.767 12.267 13.333 14.333 16.180	PM/Q 21*05 40*47 64*45 82*05 94*45 71*30 74*00	7/Q 5+1/3 5+400 5+513 5+267 4+900 4+867 +5+000	RM/Q 29.16 34.84 41.26 50.18 59.35 67.09 75.45 29.56 22.43 14.32	**M/Q =159*17 **161*59 **163*33 **163*13 **152*69 **152*69 **158*54 **156*00 **150*20
	PNT 1 2 3 4 5 6 7 8 9 10 11	.ALPHA 0.01 :=2.04 =4.02 =6.05 =7.90 =10.05 =11.98 0.02 1.99 4.02 5.98	PSI =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03	1.300 =7.667 =13.900 =20.000 =24.887 =28.200 =33.033 =1.433 :3.800 8.400 12.500	D/Q 11.360 11.767 12.267 13.333 14.333 16.180 17.500 11.373 11.167 11.067 10.873	PM/Q 21.05 40.47 64.45 82.05 94.45 71.30 74.00 20.22 12.26 4.89 0.90	Y/G 5 * 173 5 * 400 5 * 513 日 * 267 4 * 967 4 * 867 4 * 867 4 * 887	RM/Q 29.16 34.84 41.26 50.18 59.35 67.09 75.45 29.56 22.43 14.32 8.34	**M/Q = 159 * 17 * 161 * 59 * 163 * 33 * 163 * 13 * 154 * 95 * 152 * 69 * 154 * 70 * 158 * 54 * 156 * 00 * 150 * 20 * 145 * 02
	PNT 123 4 5 6 7 8 9 10 11 .12	.ALPHA 0.01 :=2.04 :=4.02 :=6.05 :=7.90 :=10.05 :=11.98 0.02 1.99 4.02 5.98 8.01	PSI =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03	1.300 -7.667 -13.900 -20.000 -24.887 -28.200 -33.033 -1.433 -3.800 8.400 12.500 17.000	D/Q 11.360 11.767 12.267 13.333 14.333 16.180 17.500 11.373 11.167 11.067 10.873 11.400	PM/Q 21.05 40.47 64.45 82.05 94.45 71.30 74.00 20.22 12.26 4.89 0.90 4.37	Y/Q 5 173 5 400 5 5 13 5 267 4 19 67 4 18 600 4 18 600 4 18 600 4 18 600 6	RM/Q 29.16 34.84 41.26 50.18 59.35 67.09 75.45 29.56 22.43 14.32 8.34	**M/Q = 159 • 17 • 161 • 59 • 163 • 33 • 163 • 13 • 154 • 69 • 154 • 70 • 158 • 54 • 156 • 00 • 145 • 02 • 144 • 19
	PNT 123 4 5 6 7 8 9 10 11 .12 :13	.ALPHA 0.01 :=2.04 :=4.02 :=6.05 :=7.90 :=10.05 :=11.98 :0.02 :1.99 :4.02 :5.98 :8.01 :9.99	PSI =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03	-1.300 -7.667 -13.900 -20.000 -24.887 -28.200 -33.033 -1.433 -3.800 -8.400 12.500 17.000 -21.167	11.360 11.767 12.267 13.333 14.333 16.180 17.500 11.373 11.167 11.067 10.873 11.400 11.867	PM/Q 21.05 40.47 64.45 82.05 94.45 71.30 74.00 20.22 12.26 4.89 0.90 4.37 5.57	Y/Q 5 173 5 140 5 151 5 151 6 151 6 151 7	RM/Q 29.16 34.84 41.26 50.18 59.35 67.09 75.45 29.56 22.43 14.32 8.34 -1.93	**************************************
	PNT 123 4 5 6 7 8 9 10 11 .12	.ALPHA 0.01 :=2.04 :=4.02 :=6.05 :=7.90 :=10.05 :=11.98 0.02 1.99 4.02 5.98 8.01	PSI =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03 =0.03	1.300 -7.667 -13.900 -20.000 -24.887 -28.200 -33.033 -1.433 -3.800 8.400 12.500 17.000	D/Q 11.360 11.767 12.267 13.333 14.333 16.180 17.500 11.373 11.167 11.067 10.873 11.400	PM/Q 21.05 40.47 64.45 82.05 94.45 71.30 74.00 20.22 12.26 4.89 0.90 4.37	Y/Q 5 173 5 1613 5 1613 7 1613	RM/Q 29.16 34.84 41.26 50.18 59.35 67.09 75.45 22.43 14.32 8.34 -1.93	**M/Q = 159 • 17 • 161 • 59 • 163 • 33 • 163 • 13 • 154 • 69 • 154 • 70 • 158 • 54 • 156 • 00 • 145 • 02 • 144 • 19

64-22 - 4-087

14+35 . 4+747

15.70 : 5.447

17.41 6.067

. 4,213

4 4 3 3 3

15.167 : 28.42 - 4.467

20.78

16.21

69 402 -134 80

19.16 =134.83

12+35 =131+65

· =2.90 =134.95

-11.76 =140.86

5.88 m134.20

. 24×10 =139×84

		OE BOOK GOVERS		, <u>b.,</u>
(,	Vellour 1	OW SPEED WIND T	MARINER MEAN 420	minera menera andre meneraliste in blade effette eil ▼ verget i.
Andrew Commission of the Commi	Y A O O H I	OM SHEED WIND I	UNNEL TEST OGU	na katana ka
		WIND AXES		
ng () () () ng		:	:	
Hale parable and an appropriate of the second and t	RUN '92	11/19/	81 1346	RUN 92
	TEN	IP 74+	PB 14+	6071
apanaga i piperaganaga da a ""	QPSF 75+00	VFPS 255.72	RNFT 1553535.	MACH 0 2257
	TO:	TO2 TO3 TO4 TO	E 'TOE TOT TOE TOE	T10
	7.02		0 0 0 0	Ö
			5 T16 T17 T18 T19	
		4. 19	0 0 1 0 0	
MS(direding) in the second	AMES-TYPE SUPPORT	S+MODEL DATA	AT C.G. FULD	SCALE DATA
	FNT ALPHA PSI	L/Q D/Q	PM/Q Y/Q	RM/Q YM/Q
eraki eraktu arta arta arta arta arta arta arta ar	1 0.01 +0.01			. 25.32 4139:19
	2 =2.06 =0.01		0 45.32 41767	30.59 -142.21
op warming		. w14.333 15.93 . w20.200 16.70		35.40 =145.51 44.58 =144.62
1		. #20.200 18.70 . #25.067 17.43		
		. ≥23.007 17.43 . ≥28.447 19.26		
			· · · · · · · · · · · · · · · · · · ·	70 00 10 10

-0.01 21.300 15.800 14 .12.03 =0.01 25.167 16.567 14.31 5.633 =14.10 =139.89 =0.01 =1.567 15.100 27.78 4.367 24.52 =139.70 -0.01 25.167 16.567 15 0.01

14.933

14.833

14.867

15.100

7 -11.98 -0.01 -33.047 20.507

3.300

12.500

16.680

8.133

0.02 = 0.01 =1.533

-0.01

=0.01

=0.01

MO.01

9

11

.12

13

2.00

5.99

4+00

8 • 01

10.00

				WIND 'A	XES					
a paga ang ang ang ang ang ang ang ang ang	4	RUN 93			11/19/81	1946		; RUN	.93	
			TEMP	81.			PO 14+	6071		
		opsf 7	Tot	VFP8 25	7.39 70* T05			MACH 0 42	257	11,
			` 7.02 T11 0	0 .92 712 713 0 1	0 0 T14 T15	0 0 T16 T17	0 0 718 719	0 720 0		
	AMES	S≓TYPE S	UPPORTA	*MODEL	DATA 1	T C.G.	FULL	SCALE D	MA.	
	PNT	ALPHA	PSI	'L/Q	,D/d	PM/Q	Y/Q	RM/Q	YM/Q	
		:-2.05	-0.01	-7.700	15.347 15.633 16.133	42.91	4.340 4.567 4.733		=135.48 =136.85 =139.37	

	PNT	.ALIPHA	PSI	.F\d	,D\d,	PM/Q	.A\6	RM/Q	· YM/Q
	1	-0.00	-0.01	-1.567	15.347	27.67	4.340	: 24:47	=135.48
	. 2	:-2.05	-0.01	-7.700	15.633	42.91	4 . 567		=136.85
그 중에 가는 경기 선택했다.	. 3	-3.99	-0.01	-14.100	16:133	62.51	4,733	35 462	=139.37
	. 4	-6.06	-0.01	19.933	16.853	77.20	4.560		-142.50
	5	·=7 • 91	₩0.01	=24.767	17+767	84 • 41	4.200	51.7%	■137 • 9 4
	6	-10.03	=0.01	w28.640	19.400	78.58	3 . 500	60 • 35	=133.07
	7.	-12.00	-0.01	#32,953	20.960	60 87	. #+033	68+29	=133.36
	8	-0.00	-0.01		15.400	27.22	4.207	24.33	=135*56
	, 9	1.99	-0.01			20.00	4.033	18.74	m131.93
	10	· 4 • 03	#Q € Q 1	8,233	14.947	15,49	4 . 167	11.81	=132.58
	.11	5.97	#0.01	12,500	15:067	12.24	. 4 . 540	5.71	=130.01
	12	8 • 00	=0.01	16.800	15.333	14.22	5.333	=3.01	≈133 •02
	13		#0.01	21.367	15.967	15.53	6.000	=11.46	=137 •33
	14	:12.00	-0.01	25.233	16.873	12.47	5 433	-13-73	≈133∗16
		. 0.01	-0.01	-1.733	15.333	25.87	. 4.193	24.35	-134-55

	·	Will East		
	.Veudht Lew s	PEED WIND TUN	NEL TEST 630	•
	Н	IND .AXES		
	RUN .94 &	11/19/81	1346	RUN 94
	,	14.	· PØ 14+6	071
	PSF 75.00 VF	and the second second	RNFT 1517285.	
	7.02	0 0 92.0	706 TOT TOS TOS 0 0 0 0 T16 T17 T18 T19	Ò
	0 0		0 1 0 0	
deletar para la la la referencia de la companya de	TYPE SUPPORTS+MO			SCALE DATA
PNT	.ALPHA PSI 0.14 +0.01 +1	L/Q D/Q (+183 15+333	PM/Q 'Y/Q	RM/Q YM/Q 26+05 =146+26
	=2.04 =0.01 a	1.900 15.667 1.267 16.100	41.35 4.993 62.82 5.000	31.64 =147.55 39.63 =149.61
		0.000 16.933 4.867 17.800 3.333 19.487	74.10 · 4.900 81.51 · 4.573 62.07 · 4.220	47 • 76 = 149 • 58 57 • 12 = 147 • 37 65 • 74 = 142 • 41
7.8	-12.00 =0.01 m3	2,933 20.833 4,600 15.433	61.28 4.300 25.39 4.567 19.97 4.373	72.96 =141.28 26.92 =145.72 20.48 =142.22
10 11	4+02 =0+01 : 5+99 =0+01 1:	3.267 15.000 2.467 15.100	14.39 · 4.433 12.25 · 4.807	13+04 =139+15 6+75 =138+23
	9.98 -0.01 2	6.900 15.333 1.367 16.033 5.373 16.900	14.92 5.667 14.95 6.220 11.78 5.567	=1.85 =141.52 =10.57 =144.50 =13.81 =142.91
,	0:02 =0:01 =	1.633 15.433	24.93 . 4.587	. 26+84 =145+05

WIND .AXES

RUN 95 11/19/81 1346 RUN 95

TEMP 86.

PO. 14.5973

AME	SATYPE	SUPPORTS	*MODEL	DATA	NT C.G.	FULL	SCALE DA	AT A	
PNT	.ALPHA	PSI	L/Q	.D/G	PM/Q	Y/Q	: RM/Q	· YM/Q	
	1.0.02	0 + 0 0	-0,994	21.325	=3.01	5.259	26442	4139.67	
		+1+99	-0.964	21.223	-2.47	1.084		-128-05	offic.
	0.02	-4.02	-1.145	21.355	-4.27	-3.193		-112-69	
4	0.02	6+00	-0.512	21,620	=9 ₹47	7.1669	21:82	=94,17	
5	0.02	≖7 ∗99	0.608	21.898	=18.42	#13+307	19 • 49	·=63 · 61	
6	0.02	=10:02	1.446	22.964	=19.18	≈18.765	21.09	=35 +54	
	0.02	=12,00	1,807	23.735	-23.34		19.36	=13.21	
	0.02	-14.00	2.440	25.211		#27.199	21.05	17-06	
	0.02	-15.99	3.464	26.988		#31:446	23+94	45.51	
10	0.02	-18.02	. 4.337	29.398		#36+789	29.38	77+82	
1.1	0.02	.=20:02	5.512	32.319	-47 ×59		33 * 53	110 + 70	
:12	0.02	.=21.99	7.639	35.572		#46 · 837	33,09	133.42	
	0.02	-24.01	8.675	37.590		#49+843	35,18	277.41	7
	0.02	-26.02	10.542	40.964		₩54×102		169.76	
		-28.01	13.175		-102.81		41,87	180.11	
, .16	0.02	0.00	=0.934	21.416	=3.60	5 : 392	. 23.82		
17	0.02	2.01	-1.114	21.572	=4+00	9 157		- =138 +49	
1.8	0.02	3+99	~0.813	21.554	=9.82	13.199		≈153•49	
			-0.331	.22.133	-19.38	:18+343		-198-12	77.7
20			0.663	22,578	=31.90	.22.380		-213.99	
		10.01	1.837	23.560	-48.34°			-229.36	Market 1
22			3.042	-24-608	=58+20	31.837	31.489		***************************************
-23		14.01	4.337	26 • 114	≈68+52	37.1265		=282+63	
21		16.00	5.392	27 • 169	=67.44		26.26		
2:			6.024	29.367	-75.74			=337.59	777
20	0.02		6.898	31.958	=81.32	.51,976		#370·56	Ś
27			7.952	34.940			20.56		
. 28			9.066	38 • 102		.62:157	18+74		
25			8.705	42.440	=86 + 72	:62:355	=19.21		
30			9 • 4 6 4	45.934	=88∗38	66+608		4380.01	
3:			=0.904	21.536	=4.34	4:398		=139.75	

WIND .AXES

RUN	96		·	11/	/19/81 1346 RUN			RUN 96			
	TEM	85	5 •					Pđ	14*	5678	
QPSF	83.00	VF	PS 2	72+1	+	RNF	15	039	5 •	MACH	0.2378
	TOT	702	703	T04	T05	T06	T07	T08	TOS	T10	
	. 7.02 . 111	0	95	0	0	0	0	0	0	Q	

, PA					4.4.50	이 하지만 살이 봤던	4 (1867) A.	10 mg 2	
	AMES	STYPE	SUPPERT	+MODEL	DATA 'A	T C.G.	FULL	SCALE D	LTA.
	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
1	1	0.01	0.00	-0.873	22.470	4+95	4.307	26.59	=133.97
	; 2	0+01		-0.723	.22 • 199	7 . 68	HO:452	24.25	=116+35
	3	0.01	-4.00	-0.331	22.380	2.03	-5.024	. 22.82	-99.52
1	- 4	. 0 . 01	=6.01	0,392	:22.530	=6+88	-10,380	. 20.20	=77+14
	5	0 + 0 1	- =8.00	1.386	23 • 163	=13 . 70	#15 + 705	. 22.32	-47 62
	6	0.01		2.072	24 • 006	=18 • 13	=20+873	. 22.00	=23.12
	7	0.01	-12.00	2,892	25 - 181	-24.46	=25,572	22.73	2.56
en e	8	0.01	=14.00	3.584	26.319		-30.Q12	. 25 - 74	27.96
	9	0.01	-16:01	4.639	28 - 410	=27.75	-35 · C66	30.97	56.18
	10	0.01	.=18:02	5.633	31.066		=39,880	- 33 € 05	. 89 • 36
	11	0.01	.=20.02	6.867	33.319	=49+00	単44+639	36 • 13	118.36
	12	0.01	-22.01	8.042	35 • 470	=60 • 16	# 46 • 566	31+74	127 • 15
70 SH48100	13		24.01	4.675	38.964	-78+40			150.27
	14	0.01	-26.01	12.440	42.199		#55.9U4		170.56
	15		-28+00	14.934	45 • 663			34+30	
- this remains a second of the	16	0.01	0.01	=0.843	22.440	6.40	4 4 4 5 8		=134+41
'	17	0.01	2.00	=1.145	22.560	7.12	8 . 825	21.28	
	18	0.01	4:02	=0.904	22.819	0 • 83	13.313		=152 • 14
 	19	0.01	6.00	-0.181	23.193	-9.74	.18.530		-193.21
	20	10.0	8.00	0.783	23.614	-21.78	23.373		-217.00
* 0	21	0.01		2.048	24.548	=38.65	27 . 952		=232.33
<u>سروم سروم با ده شمه مسوره و بساوی به خدید با آنی مقالی نی باید و پاکستان می باید با</u>	.22	0.01	12:01	3.373	25.331	=51.+75	.32.380		≈255•10
	23	0.01	14.02		26.416	-62.24	36.639		=279∙42
	24	0.01	16.01	5.289	27.922	=71 +24	40.504		=304.08
	25	0.01		6.639	29.518	=70+73	46.325		=331 • 92
	26	0.01		7.651	32.289	=76.97	51.717	25.52	×368+35
	27	0.01		8.705	35.392	=90.04	57. 223		=400+68
	28	0.01		10,265	38 • 620	=102.88	62.030		=426.22
P	29	0.01	26.00	10.723	43 • 127	=84.17	.62 : 633		-362.17
į	30	0.01	28.00	11.205	46 819	=84.88	66 175		=377 ∘66
	31	0.01	0.01	-0.843	22.440	7 • 69	3.735		=134 • 17
	~ *	4.74	# T W	-0:070	E E R T T U	/ * 0 7	01/30	ELC A C. A.	コキラエ・ドリ

WIND .AXES

RUN	97		11/19/81	1346		: RUN :97	
	TEMP	80.			PO . 14+5	1659	
gps	70 ‡ • 7.02	0 92 702 703	T04 T05	T06 T07	708 TOS	Q	
AHESATY	0 PE SUPPORTS	0 1 3+MODEL	1 0 DATA 7	0 1 T C · G •	- 0 · 0 -FULL	O SCALE DATA	
PNT .AL	PHA PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q YM/Q	

PNT	.ALPHA	PSI	١٢٧٥	D/Q	PM/Q	Y/Q	RM/Q	YM/Q
	-0.00	0.01	-1,567	15.367	27,53	, 5,113	. 29.22	-143.51
	:=2.05	0.01	-7.867	15.720	43.22	5.527	35.40	-147.45
3	医乳腺性溶液 医氯化二氯化甲烷	0.01	-13.800	16.267	61.61	5.913	42+24	-151.77
- 4	=6:05	0.01	=19.767	16.900	78+65	6 • 047	49.23	4156 • 41
. 5	'=7 + 92	0.01	-24.733	17.820	85.58	6.080	56 • 49	M158+64
6	=10:04	0.01	=28.533	19.367	74 • 18	6 4 4 5 3	65 • 92	≒161•28
	-12.00		432.933	20.987	62.09	, 6,613	70,52	≈158•55
		0.01		15.400	26.83.	5.113	30.55	-142.68
		0.01		15.233	20.55	4.787	. 22.70	=139+40
10	4.01	0.01	8.367	15.133	13,57	4.713		m136+34
11	5.99	0.01	12,633	15.087	11.55	· 4 • 8 47	7+90	4133.97
:12	8 • 01	0.01	17.033	15 + 400	13.81	5 . 5 4 7	=1.61	■139 • 74
1.4.2.2.3.3.4.3.3.3.3.4.6		0.01	21.533	15.967	15.95	. 5.880		-142+14
	11.99	0.01	25.900	16.700	16.60	: 50267		-143.92
		0.01	=1.667	15.400	26 + 65	3.813	30+04	-143.64

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4.5	**	the state of the s	
1	1	and the state of t	TUNNEL TEST 630

WIND AXES

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AMES-TYPE SUPPORTS+MODEL DATA AT C.G. FULL SCALE DATA RM/Q YM/Q PSI D/Q PM/Q .A\a PNT ALPHA L/Q 27.37 -134.26 0.01 28:02 . 4:807 0.01 15.367 =1.367 0.01 -7.467 43.44 1 5.000 32.86 -136.25 2 :-2.06 15.727 39.39 -142.09 0.01 -13.900 60.69 5.367 16.267 5.533 45.78 =145.79 0.01 =19.900 16.967 77.25 -#6 · Q6 52.15 =146.31 0.01 #24.667 17.87 5 . 767 **-7.** •90 84 . 40 61.49 -150.53 0.01 =28.600 19.3 70.41 6.067 $6 = 10 \cdot 04$ 66 * 45 = 151 - 27 #12.01 0.01 -32.700 20.980 62,86 6 6,200 . 27.75 -134.74 - 4.707 . 8 0.02 0.01 -1.300 15 . 467 27 25 20.64 =127.99 0.01 9 2.00 3.667 15.120 19,57 . 4.333 12.37 -128.33 . 4:467 10 · 4 • 01 0.01 8.333 15.013 13.89 . 4.733 5.66 -127.00 11 5 . 97 0 01 12.667 15 . 067 11.51 =3.06 =131.55 0.01 5 . 273 8.00 17.100 15.367 14022 5 . 787 =10.56 =136.09 13 9.99 0.01 21.633 15.933 17.47 : 5.133 =15.02 =139.78 24.267 16.900 14 :12.04 0.01 16:05 27.61 . 4.733 . 26.70 -135.10 0+01 .15 -0.00 -1.433 15.367

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	41			u Bacen	WIND TUN	WEL TEST	430	<u> </u>	
garantina g	<u></u>		John Fr	WIND :		DIE.L. 1.E.3.1			
		RUN 39		A A	11/19/81	1346		RUN	.99
			· TEM	73,			P6 14.5	531	
		QP8F	T01 702	702 703 0 83	704 TO5 0 0 T14 T15	TOS TOT	708 TUS	0	
	AMES	-TYPE	O SUPPORTS	01 1•M¢del	1 0 DATA	01_ \T_C:G.	O O	SCALE DA	
	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	. RM/Q	· YM/Q
	2	0.04 -2.03	0.01		13.733 14.233 14.887	16.29 40.75 69.14	, 41967 5.607 6.100	33.73	=130.61 =136.93 =143.86

	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
	1	0.04	0.01	-9.600	13.733	16.29	41967		≈130•61
	2	:-2.03	0.01	#13.300	-14+233	40.75	5.607		=136≠93
	. 3	4-01	0.01	-17-100	14.887	69.14	6.100		=143.86
7	4	-6+05	0.01	-20.967	15 • 667	97 + 89	61767	47.91	
C	5	·=7 • 90	0.01	-22.993	16.587	101 • 44	7.073	55 13	=160+49
	6	=10.03	0.01	-24.267	17.567	98.57	7 • 433		=169+82
	7	-12.00	0.01	-25,467	18.833	97.24	7.500		-172.70
	8	0.02	0.01	=9.580	13 . 667	15.85	4 . 967		#129+33
	9	1.99	0.01	-6.067	13.300	=7.06	4.780	18.55	=129.39
	10	. 4.02	0.01	=2.667	12.933	≈29.66	4 633	10.55	=129+42
	11	5 • 9 6	0.01	0.567	12:667	47.48	4 9 6 6 7	4 / 97	=132+63
	12	8.01	0.01	4.067	12.500	≈68 ∗20	4.800	-2,93	=137 ∗53
	13	9.98	0.01	7.400	12.700	≈90.94	: 5,600	=9 <22	≈136+16
	14	11.99	0.01	11.133	13.200	=115.04	5.300	-16.20	=138.60
	15	0.01	0.01		13.913	22.14	7.200	25.35	=131 • 16

S. ...

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

RUN 100 11/19/81 1346 RUN 100

TEMP 84. PO 14.5482

GPSF 100.00 VFPS 298.64 RNFT 1748585. MACH 0.2612

TO1 TO2 TO3 TO4 TO5 TO5 TO7 TO8 TO9 T10

' 702 0 83 0 0 0 0 0 0 0 0

' T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

AME	8-TYPE	SUPPORT	-MODEL	DATA	T C.G.	FULL	SCALE DA	
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	RM/Q	. AWNO
	0.01	0.01	-10.750	-14-085	23.78	9.040	22,39	=128*02
	:-2.03	0.01	*14.500	14.825	50 + 51	10.115	31.36	≈136+64
		the state of the s	-17.850	15.540	73.41	11.270	38+64	-149.96
4	=6.06		=20.915	16.430	93 • 10	12:480	45.71	=163.57
5		•	=23.245	17.460	103+36	13,215	54+84	=180+65
6		7.	-25.780	18.550	118.35	13 . 7.65	75.16	=196∗32
7	-11.98	The second secon	-27.680	19.725	124.91	113,690	73.94	-196.26
4		1004 HOAT MARK 15 A	-10.625	14,075	23 - 24	8:365	. 23-84	-128.91
	: 2.00			13.600			17.35	-124.19
10			=3.450	13.350	=26.04	7.115		#124 · 13
11			=0.150	.13 + 120	=48+04	6.950	1 +96	#1126 · 42
. 12				13.025		6.900	≖5 •38	#129.89
		age of the later of	6.975	13.000	The second secon	6.590	10.97	#130.58
	and the first transfer of transfer of the first transfer of tran	Paragraph of the control of the cont	The first that the fi	13 400		6 . 265	-18.07	#135·25
		The state of the s	223 12 00 00	14.175				#129.98

WIND AXES

AME	SETYPE	SUPPORT	S+MODEL_	DATA'A	T CeG.	FULL	SCALE DA	NTA.
PNT	.ALPHA	, Psi	٢١٩	.ס/מ	PM/Q	YZQ	RM/Q	· YM/Q
	=0.00	0,01	-2,473	15.800	32.35	9,300	26+45	=135.30
	:=2.04	0.01	-8.667	16.267	44.93	10.433	33.46	=142.47
	3.99	0.01	-14.367	V 10 1 10 10 10 10 10 10 10 10 10 10 10 1	57.97	11.273	40.81	=151.04
(4	=6.0!				72.85	.12 + 433	47 * 76	=164.84
5	=7+92		#24 . 793		77.60	13.500	56 +98	=184.92
6	-10.0	• •	-30.133		86.28	13.933	71 647	194 • 06
	-11.98		#35 ,393		90+24	-14:967	80.36	*210.26
	-0.00		-2.633	 * (1) * (2) * (2) * (3) * (4)	32.04	9.033		=134,20
그는 소문에 가게 되는 것이 되었다. 중요한 경기 문화가 하는 물을 보고 하는데, 연결하게 되었다.	1.9				21.08	8.013		=127.61
10	4 • 0		7.700		13.71	7 . 7.33		=121+82
11	5.9		11.800		10.09	7 . 840	4 . 49	
12	8.00		16.367		10.50	8 • 053		=121.20
15		A STATE OF THE PERSON NAMED IN COLUMN 2 IN COLUMN 2	20.740		13.04	8.200		=127.06
	:12.0	** A second of the second o		and the first of the contract	12.07	7. + 233		=128+69
			The second of th		32.70	9.033		=134.76

WIND :AXES

TEMP 67. PO 14.5875

QPSF 75.00 VFPS 254.21 RNFT 1578645. MACH 0.2259

TO\$ TO\$ TO\$ TO\$ TO\$ TO\$ TO\$ TO\$ TO\$

702 0 .92 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

PNT	.ALPHA	PSI	.L\@	D/Q	PM/Q	Y/Q	RM/ a	· YM/G	
	0 * 0 2	0.00	=2.567	15.400	36.05	: 8 + 933	25.10	=130.31	
	:-2.05	0.00	-8.633	15.833	48.86	9.967	32.65	4138.32	Rp.
(-4.02	0.00	#14.600	16.433	. 64.60	11.000	39.06	=148.78	
4	=6.06	0.00		17.320	75.74	:12,293		=162.33	
5	=7 • 90	0.00	m24.740	18.547	77 • 81	13:200		=175.58	
6	=10:03	0.00	-29.900	19.973	86 • 66	13 . 867		-191 - 15	
	-12.00	0.00	-35 ,300	21.473		15.233		-208:37	
	0.02	0,00		15.467	35+66	THE STATE OF THE STATE OF THE STATE OF		=129+14	and Sala
	1.99	0.00		15.200		8.060		=124.13	
10	4.02	0.00		15.067	16.33	7,733		□118+44	
11	5 • 97	0.00	11.967	15+100	13.56	7 # 667	2-19		
12	8.01	0.00	16.433	15.433	13.81	8 • 073	=5.98	=120 •62	
13	9.99	0.00		16.067	14.93	8 9 0 6 7		=120+27	1777
	11.99	0.00	25.400	16.933	14.68	7.,200		-123.81	
		0.00		15,433	34.49	8 993		=131.99	

	Cariffic desirabilità di magnificiale di Pro-		ودفنا فوذ مددن برنيين الانتفاد المحمدادي	A GNIW	XES	and the second s	<u></u>		
		RUN 103	<u> </u>		11/19/81	1 1346	ن مرحد سر بر بر حاسل هی موماندوس ی	. RUN	103
			TEM	71.			PO 14.5	875	•
والمستحدد والمستحد والمستحدد والمستحد والمستحدد والمستحد	Qualify	QPSF 7	5+00	VFPS 25	55 • 17	RNFT 15	3608+	MACH 0+2	259
			TOI	T02 T03	T04 T05	TO6 TO7	708 709	710	
	· · · · · · · · · · · · · · · · · · ·		7.02	0 92	Q Q	0 0	0 . 0	Ò	
v						T16 T17		124	
	-		<u> </u>	0 1	. 1 0	0 1	<u> </u>	<u> </u>	
		-							
	AME	SETYPE E	UPPORT.	8+MODEL	DATA	AT C.G.	FULL	SCALE D	NTA
		•					•		
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	YYU	. RM/Q	' YM/Q
	1	0.01	0+00	-3.000	16.173	35.73	: 9:367	23.54	=133+99
	: 2	-2.04	0.00	-8.700	17.000	48 - 45	10.353		-142.55
	. 3	-4.02		-14,133	17.767	62+68	11.267		=150.55
-	. 4	-6.07	0.00	-19.427	18.767	77 • 68	12:167		-162.94
Van.	5	-7.91	0 • 00	H23.307	20.073	80:55	12.700		=173.69
	6	#10:05		=27.980	21 • 833		:12 967		=186.69
,	7	H12.00	0.00		23.473		13,407		-188 - 78
	8		0.00		16.267		5.300		=135+01
	9	5.05	0.00		15.887		8,633		-129.48
	10	. 4.04	0.00		15.867		8.333		=125 •23
	11	5.98	0.00		15.900		8:307		123.24
	.12	8 + 00	0.00	18.033	16.367		8 • 5 <u>0 0</u>		=122.39
-		10.00	0.00		16 . 833	16.99	8+433		-127-87
	13				خسيف ششاست دور				
	14	11.99	0,00	27.033 =2.967	17.867 16.233		7,533 002,0		#129°33

0.00

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•	OF PONK (Imania.	A→106					
	YOUGHT LAN	Y SPEED WIND TU	NNEL TEST 630					
		WIND .AXES		,				
	RUN 104	11/19/8	1 1346	: RUN 104				
	TEMP	75 •	. PO · 14	•5875				
Hart de la constitución de la co	· QPSF 75.00	VFPS 256+13	RNFT 1548811+	MACH 0.5529				
	TOT 1	102 TOS TOS TOS	TOS TOT TOS TO	9 T10				
	7.02	0 92 0 0		o o				
region to the second	AMES-TYPE SUPPORTS	+MODEL DATA	AT C.G. FUL	L SCALE DATA				
·	PNT .ALPHA PSI	L/Q D/Q	PM/Q Y/W	ŔM/Q YM/Q				
	1 0.03 0.00	-2.067 16.100 -8.033 16.660		3 27 €72 =134 •40				
	. 3 ≈4≪02 0.00 h	13.667 17.227						
	5 =7.50 0.00	#19:000 18:367 #23:300 19:600 #26:113 21:513	83.44 5.03	3 43.59 -125.08				
Accession of the Control of the Cont	7 =12+01 0+00 8 =0+00 0+00	#30.233 23.400 #1.933 16.060	72.27 5.00 25.76 5.46	0 56*10 =126*23 3 21*89 =134*32				
Address Maria Company	9 . 2 . 00 0 . 00	3.200 15.733						

23.200 16.700 12.77 6:067 . -15:67 -134:12 0.00 27.460 17.500 15.20 14 75.05 24.51 : 5.533 . 21.75 =134.34 15 0.00 -2.133 16.047 0.02

8.767

13.633

18.600

15.687

15.633

16:067

10.90 5.707

10.20

9.90 . 6.053

6.493

6 • 633

8.08 4131.34

HO +75 H132 .42

#6 #25 #132 *54

-11+65 -134+97

WIND AXES

: RUN 105	-,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		9/81	1346	· income and a constant	بنبنده	<u>, , , , , , , , , , , , , , , , , , , </u>	UN 105	
TEMP	76•	•			PØ.	14+5	875		
QPSF 75.00	VFPS	256.37	,	RNFT 1	545145) <u>k</u>	MACH	0-2259	ř.
tor	T02 T0	03 TO4	T05	TO6 TO	7 708	709	T10		
. 7.02	0 7	74 0	0	Q	0 0	O	Q		
' T14'	T12 T	13 T14	T15	T16 T1	7 718	T19	720		

AME	S-TYPE	SUPPORT	+MODEL	DATA 'A	T C.G.	FULL	SCALE D	NTA	
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	.A\đ	RM/Q	YM/Q	
	0.01	.0.00	-1.567	12.233	18.13	5.900	25.70	⊲152∙95	
2	:=2.05	0.00	-7.667	12.927	37.60	6.007	32+35	-152-69	
· 3			#13.467	13.673	62.34	. 6 . 047	37 +63	a150.92	
4			=18.533		82+09	5 . 887	42+06	≒147 • 00	
5			22.867	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	86+84	5:733	· 47 • 22	≈144 €38	
6		=	-25.753		71.59	5.240		=141 .66	
7	H12.00	والمراب والمستحدد المستحدد المستحدد	-30.033	معدنها وسنب كتفاهران كماني	75.20	5.700		=143.01	
		•	-1.367		19.61	5 • 833		=152 -80	7. 2. 3
g e	110000		3.967		8 • 65	5 • 833		-153-43	
10			9,100		1+69	5 . 827	9.08		
Ĩi	5.9		14.000		=1.38	5.967	1 +90		
12			18.833	(1.43	. 6.260		=141.37	
13			23,200		3.53	6.367	-12-19		بسيد
4.4			27,600	44 4	5.29	5.767	-15.77		$f_{i,j} \in \mathcal{I}_{i,j}$
15		•	-1.400		18.14	5.833		=153·17	

WIND AXES

the control of the state of the	RUN 106	11719/8	1 1346	RUN 106
	TEM	P 88.	P6. 14	•5875
****	QPSF : 83+00	VFPS 272.70	RNFT 1580400+	MACH 0.2376
	TOE	702 TO3 TO4 TO5	TO6 TO7 TO8 TO	9 T10
	702		0 0 0	U Q
	_			

and the second s	AMES	-TYPE	SUPPORTS	+MODEL	DATA 'A	7 C.G.	FULL	SCALE DA	TÀ	
	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y\@	RM/Q	· YM/Q	
	1	0.08		-0.904	21.837	-7+04	5.030	27.33	-141.93	::
어느 그 아들이 빨리를 받았	2	0.02		-0.964	21 . 705	-7.99	0.307	27.59	=124.88	
	3	0.02		=1.024	21.669	■7+73	=3.795	27 • 13	=109.48	
(;	4	0.02		=0.633	.22:018	=13.71	7.922	25.21	×91 + 24	
	5	0.02	=7 •99	0.090	:22 + 440	-19.22	£12:590	. 22+64	·=64+29	
	6	0.02	-10.01	1,506	23.072		■18 • 223	18.80	:=33.91	
	7	0.02	-11.99	2.259	24 • 187	=34+27	#23:253	20.21	- =9.60	
	8	0.02	-13.99	2,651	24.880	-25.55	#26 · 807	20.57	14.98	
	9		15.99	3,633	26.867		#31.476	25 e 35	42.11	·
	10.	0.02	#18±01	4.277	29 4 4 1 0	×41 • 41	#36 £12	27.77	75.99	-
	11	0.02	:=20 ·05	5,693	.32 + 434	=51 · 16	#41 #687	30+44	107.37	
•	12	0.02	.=21 +99	7.892	35.560		#46 ± 506	28.48	128 - 23	
	13	0.02	-23.98	10.422	39 : 187		#51 . 759	29,38	152.73	
	14.	0.02	-25.99	12.669	.42 . 892		=56.657	31+64	172+10	
	15		=27497	14.464	46.620		#59 904	38.56	176.17	
Contractive to the second seco	16.			-0.843	21.693	=6.74	6 : 295	21.49	=140+16	
	17	0.02		-0.994	.22.018	=7.31	10:169	17 480	=141 .08	
	18	0.02		-0.452	22.349	=16.96	14.669		=160.33	
	19	0.02		0.060	22.801	=25.44			-203.99	
	20	0.02		1.295	23.422	=39.41	24.247		-219-17	G.
	21	0.02		2.620	24.434	=53.08	29 . 157		=239.22	
ىيىزى يىرى ئىرىنىلىدى مىلىدى دېرىيىدى بىرىيى ئىرىنى يىلىنى ئىرىنى يىلىنى ئىلىنى بىلىنى بىلىنى بىلىنى بىلىنى بى ئىرىنى ئىرىنى ئىرىنىلىدى ئىلىنى ئ	:22	0.02		4.066	25.602	=61.87	32.910	30.11		
	23	0.02		5.301	27 • 133	=70.73	38.855	25.90	=292.76	
	24	0.02		6.386	28 • 223	=72.58	43.024		=310.60	
	25	0.08		7.139	30.422	-81.20		26.10		
•	26	0.02		7.892	33.133	=87.37	52.741	27.20	- 4 -	
*	27	0.02		8.602	35.843	=101+35	57.356		=408+29	
	28	0.02		9.970	39 • 114	=114.58	.62:422	24.55		
1 ···	29	0.05		10.482	43 • 813	=89·29	63 • 133	=16 .09		
<i>i</i>	30	0.05		10.217	47.771	#87+31	66 + 898		±373∙37	
	31	0.02							=140+35	
× .	27	V • V &	0.600	-0.693	21.783	-6+04	5.633	ETIEP	-140130	

γ	BUGHT	LAW	SPEED	WIND	TUNNEL	TEST 630

WIND AXES

Pres .

RUN 107			11/	1,9/8	L_13	146		5 %	<u> </u>	RUN 107	::
TEM	p 8	38,					Po	14+	5875		
그 모든 물이었다면 하다면 사용한 그를 가고 생각하다면 하다면 살았다.	300 H	PS 2								0 • 2259	
	T02	EOT S	T04	T05	T06	T07	BOT	105	T10		
7.02		82	Ó	0	0	0	0	0	0		
T11	T12	713	T14	T15	T16	T17	7:18 0	T19	720 0		

P	TN	.ALPHA	PSI	<u>L</u> /Q	D/Q	PM/Q	Y/Q	RM/Q	. AWNO	
	1	0.01	0.00	=1.033	8 • 6 6 0	*123*62	- 4.233	25.27	=147.52	-
에 그 나는 사람들이 하는 그런 사람들을 모르는데 함께 살아보다는 그런 사람들은 사람들이 되었다.	2	-2.04	0.00	=1.867	9.067	#138.16	3.920	. 29.22	=142.99	
	3	4.02	0.00	=2.567		=153.79	3.067	31.22	=129.62	
\	4	=6:07	0.00	=3.367	9 • 813	=172,07	. 2:380	33.71	-111+64	
•	5	-7.92	0 + 0 0	=3.800	10 - 167	=188.20	: 2:380		-103.16	
	6	=10+04	0.00	=4.500	10.500	=203.72	. 2.700	44.81	=107+14	
	7	-11.98	0.00	=5,467		-216+64	; 3,300	51.78	-118.18	1.5
가는 사람들이 되었다. 그는 경우 전혀 전혀 되었다. 전 대학생들이 보고 전혀 보고 있습니다.	8	0.03	0.00	-1.000	8 • 673		. 4.167	24+14	-146.99	
	9	1.99	0.00	=C-167		-110.28		18:37	-147.03	174.4
	10	. 4.04	0.00	0,767	8:167	=94+87·			=143+05	
<i>*</i> .	11	5.97	0.00	1.700	7.967	-80,80	4.367	4+26		
•	12	8.01	0.00	2 . 667	8.000	=62 + 47	4 + 540	-3 423	=136+66	
	13	9.98	0.00	3.600	. 8 . 100		4.800	=8+45	=138.06	
	14	:12.03	0.00	4.500	8 • 267		5 . 167		=141.74	445
	15	-0.00	0.00	-1.100		-124.53	- 4.200		≈148·93	

		MIN	1D (AXES							
// 1/2 				······································			 			
RUN 1	.08		11/	19/81	13	46				RUN TOR
	. TEMP	88	,				PO	14.5	875	
CPSF	75+00	VFPS	259.2	3	RNFT	150	2306	•	MACH	0 - 2259
	. Tor	T02 1	103 TO4	T05	T06	TOT	708	T09	T10	
			20	^	~	^	0.		0	
	7.02	0	₹2 0	Q	Q	Ų	Ų	· 🗸	Ų	
		QPSF 75.00	RUN 108 TEMP 88	RUN 108 11/ TEMP 88. QPSF 75.00 VFPS 259.2	TEMP 88.	RUN 108 11/19/81 13 TEMP 88. QPSF 75.00 VFPS 259.23 RNFT	RUN 108 11/19/81 1346 TEMP 88. CPSF 75.00 VFPS 259.23 RNFT 150	RUN 108 11/19/81 1346 TEMP 88. PO OPSF 75.00 VFPS 259.23 RNFT 1502306	RUN 108 11/19/81 1346 TEMP 88. PO 14.5 QPSF 75.00 VFPS 259.23 RNFT 1502306.	RUN 108 11/19/81 1346 1

****	AMES	S-TYPE	SUPPORTS	+MODEL	DATA	AT C.G.	FULL	SCALE D	NTA
	PNT	.ALPHA	PSI	L/Q	D/Q	PH/Q	YZQ	. RM/Q	. AW\đ
	. 1	0.01	0.01	=1.000	8 • 833	=124+89	3,847	. 20.93	-148-37
	2	2.04	0.01	-1,933	9.113	#139 +59	3,500	24+05	-140.75
	3	-3.99		-2.633		-155.18	2.367	26.29	≈120¥69
	. 4	=6.Q#		3.400	9 • 933		1.540	: 27.90	=104 • 65
V .	5	•		=3.800	10+300	=188 + 43	1.367	30 + 76	m96+44
		-10.05		4.533		-205.37	1.800		=101.51
	7	-11.98		-5.433		-219.02	: 2,633		=112.95
en e	Ŕ	0.03		-0.967		-123.82	3 . 833		=145.45
and the second of the second	. 9		and the second second	-0.067	A CONTRACTOR OF THE CONTRACTOR	=109.11	3.967		=147.66
was a sure of the	10	. 4.00		0,833	8 • 233	=94 ;43	. 4.060		=141.05
	11	5.96		1.800	8.000		4.000		≈137.38
	12			2.767	8.000		4 • 167		=137∙89
White the state of			the same of the sa	3.700			* 4+347		=139.77
	13			and the second of the second o	8+067	#45+24			=144+06
	14			4.533	8 • 167	=26.78	4 667		
كأنا كالمتابيب والمتحاك المحافة وقفيات بتمانيات التناه والمالية	15	0.01	0.01	=1.000	8.727	<u>=124 × 73</u>	3.867	61116	=148.01

•

VOUGHT LAW SPE	ED WIND	TUNNEL TE	ST 630
WIN	D .AXES		

RUN 109			11/	9/8	13	46			:: :: ::	RUN 10	<u> </u>
•	TEMP 8	8 •					Pe	14+	3580		
GPSF 75.	00 VF	PS 2	59,45	3	RNFT	150	0789	} •	MACH	0.226	1
	TO1 TO2	T03	T-04	TOB	T06	TOT	7.08	TOS	T10		
	702 0	.82		0	0	0	O	, 0	Ó		
	T11 T12										

AME	S-TYPE	SUPPORTS	+MODEL	· DATA	T C.G.	FULL	SCALE D	ATA
PNT	ALPHA	PŚĮ	Ľ/Q	D/Q	PM/Q	·Y/Q	RM/Q	' YMZQ
	0.02	0.01	=1.067	8 • 8 6 7	=123+16	: 2,940	21.47	=127+46
T	3-2.01	0.01	.=1.900	9.220	-138,38	: 2.360	25.31	-118.86
	-3.99	0.01	-2.667		=154+34		27.44	-101.93
4	·=6.08	0.01	=3.467	9.967	=168+93	0.827	28+13	≈88+23.
, 5	™7 • 9 4	0.01	=3.900	10.367	=188.53	0.667	30 +50	-82 • 11
6	=10.05	0.01	=4.633	10.733	-205 • 10	1 • 027	38+19	.=84·51
7	-12.00	0.01	=5.600	11.167	=216*33	. 1.427	. 40.21	487*10
121 - Jan Harriston (1888) - 122 - 123 - 123 - 123 - 123 - 123 - 123 - 123 - 123 - 123 - 123 - 123 - 123 -	0.03	0.01	-1.000	8 • 8 6 7	-121.97	: 2:860	21.71	-127+00
선생들이 한 사람이 있었다. 내일 내	2.02	0.01	-0.100	8.700	=107+99	. 3.027	15.53	=122.67
10	. 4.03	0.01	0.867	. 8.500	-92+78	: 3+247	7.96	=119.53
11	5.97	0.01	1.833	8 • 100	=75 + 65	3 427	3.86	=120.66
:12	8.00	0.01	2.800	8 • 133	=58+84	3 . 827	-2.78	=122.77
13	9.99	0.01	3,800	8 * 200	-41.56			=130.11
	:12.02	0.01	4.700		-27.36	4,547		#135.08
15	0.03	0.01	=0.967			and the second of the second o		-125.20

GENOMAL PAGE 18 OF POOR QUALITY

-A-112·

VOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630
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WIND AXES

RUN 1	10		11/19/81 1346							: RUN 110			
TEMP 90.								PØ	1,4 •	14.5383			
gpsf	75.00	VF	P9 2	60 • 1	+	RNF	1 143	9284	Q •	MACH	0 - 2263		
	T01	TOZ	T03	TOF	T05	T06	T07	708	TOS	T10			
	7.02	0	81	Ó	Q	Q	0	. 0	Ç	0			
		gPSF 75+00 . T01 . 702	TEMP 9	TEMP 90. QPSF 75.00 VFPS 2 T01 T02 T03 702 0 81	TEMP 90. QPSF 75.00 VFPS 260.10 TO1 TO2 TO3 TO4 702 0 81 0	TEMP 90. QPSF 75.00 VFPS 260.14 T01 T02 T03 T04 T05 702 0 81 0 0	TEMP 90. QPSF 75.00 VFPS 260.14 RNF T01 T02 T03 T04 T05 T06 702 0 81 0 0 0	TEMP 90. QPSF 75.00 VFPS 260.14 RNFT 14:	TEMP 90. P0 QPSF 75.00 VFPS 260.14 RNFT 1492840 T01 T02 T03 T04 T05 T06 T07 T08 702 0 81 0 0 0 0	TEMP 90. PO 14. QPSF 75.00 VFPS 260.14 RNFT 1492840. TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 702 0 81 0 0 0 0 0	TEMP 90. PO 14.5383 QPSF 75.00 VFPS 260.14 RNFT 1432840. MACH TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 T10		

	AMES-TYPE SUPPORTS+MODEL				DATA	AT C.G.	FULL SCALE DATA			منتبده
	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q	
	1,	=0.02	0.01	8.400	10.400	=132.90	2.700	: 21 • 05	=118.55	
The second of the second	2	-2.04	0.01	4.767	10.467	-152.39	: 2.533	23.94	=110.18	
	3	-4.01	0.01	0.967	10.767	-174.53	: 2 . 000	27.66	-99 × 32	
(4	≈6 + O4	0.01	=2.733	11.267		1:493	. 29 . 26	=92.75	
**	5	-7.90	0.01	≃6,133	11.767	=213:68	. 1:533	33.10	=91 +91	
	6	-10:05	0.01	=10.133		≈229 • 11	1 . 833	42-14	=94.99	
	7	H12.02	0.01		Mark 11. 10. 10. 10. 10. 10. 10. 10. 11. 11.		: 2,907	43,17	=98+97	
" " " "	8	0.02	0.01	8.567	10.433		2.673	21.11		N.
	9	1.97	0.01	11.533		-114-10	: 2.740	and the second second second second	=121 -70	21
	10	- 4+02	0.01	14.600	10 - 433	=90.62	. 3.033		#118.93	
	11	5 • 98	0.01	17.400	10.533	=69+64	1.453	7 . 80		
	12	7 . 99	0.01	20.333	10.767	=47.49	4.173		=118.63 .	
	13	9.98	0.01	23.800	11.333	-24+49	4 633		=121 07	
	14	:12.00	0.01	27,200	12.200		4.733	-16.77		
	15	-0.02	0.01		10.407	4133.75	2.700		=118+15	

ORIGINAL PACE TO OF POOR QUALITY

A-113

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

PNT	ALPHA	PSI	L/@	0/0	PM/Q	'Y/@	RM/Q	, JW\G
• • • •		*						,
	0.02	0.01	-7.280	11.593	-120,25	5 467	17.93	-140-19
	-2.03	0.01	-10.367	11.800	-134+16	5 . 487	- 1 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-143:03
	-4+01	0.01	w13.233	12.133	-156.84	- 4.733		=137.32
. 4	-6.06	0.01	#15.400	12.533	=177 · 05	3,033	34 € 09	=118 s48
5	-7.90	0.01	s17.653	:13 - 140	=196+41	. 1:567	38 48	=103.08
6	=10∗04	0.01	-20.433	14 • 100	-213.56	0.333	44.52	. = 90 ∗53
	-12.01	0.01		the state of the last of the l	-228.54	. 0.033	45.03	3≈83·80
- 15 kg kg 3 4 4 5 5 3 5 3 5 3 5	0.01	0.01	-7.187	11.667	-123.86	5 433	17616	=140 -47
	. 2.01	0.01	-4.267	11.733		5,433	11:62	-134.32
10	4.02	0.01	=1.573	11.733	=85.54	. 5,300	4+24	H133+43
11	5.98	0.01	1.567	11.833	≈66+32	5 • 267	=2.48	=129+14
:12	8.00	0.01	4.707	12.000	=46·40	5 • 0.00	=6 +83	=124.37
13	10.02	0.01	the second second second second second	.12.327		4,867	-12.77	=120+84
	:12.00	0.01	11.493	12.900	The second secon	4,567	-17:11	=122.70
16 16 18 18 18 18 18 18 18 18 18 18 18 18 18		0.01			=12 .68	A Committee of the Comm		-140.73

WIND .AXES

	RUN 112	s - International	11/	19/81	1346	L		. RUN 112	
	· TEM	88.				Pō.	14+	5283	
	QPSF . 75.00	VFPS	255 6	6	RNF1' 1	49977	5 •	MACH 0 2263	
	TOT	702 T	03 TO4	T05	TO6 TO	7 708	TOS	T10	
The second se	7.02	Q	81 0	Q	Q	0 0	+ Q	0	
	T11	T12 T	13 T14 1 1	T15	T16 T1	7 718	T19	0	

AMES	SATYPE SUPPORT	S+MODEL	DATA A	T C.G.	FULL SI	ULD SCALE DATA		
PNT	ALPHA PSI	L/Q	D/Q	PM/Q	'YZQ	RM/Q YM/Q		
<u> </u>	0.01 0.03	=2.487 1	0.86%	×122+16	5 : 667	17.97 -143.43		
	:-2.04 0.03	-5.700 1	1.067	*142-99	4.967	25-19 =140-27		
	-4.02 0.03	-8.333 1	1.367	=162-35	36689 ·	30 +85 =125 +10		
	6406 0+03			×177.31	2.067	33.31 =110.51		
5	-7.92 0.03			=201.20	1.353	34.78 =98.49		
· 6	-10:03 0:03			=221 • 05	1:700	42.21 m101.01		
7.	-11.98 0.03			≈231.93	: 2.200 .	44*40 =100+08		
8	0.05 0.03			*123·30	5 • 667	17.86 -143.37		
	: 2.00 0.03			#104.13	5 + 907	10.31 -138.08		
10	4.04 D.03		1.267	=84.36	. 6:107	0.60 =133.50		
11	5.99 0.03		1.500	≈65 t 68	5 . 933	=5 •70 =128 •98		
:12	8.00 0.03		11.893	=45.35	. 5 . 387	=9.76 =123.05		
13	10,00 0.03		2.233	-26.76		-13.98 -117.52		
and the second s	12.00 0.03		3.067	-6.22		-19+70 -115+97		
15,				=124.21	5 • 733	18+49 =143+59		

V	OUGHT.	LOW	SPEE	DWI	I DA	UNNEL	TEST	630

WIND AXES

	ES-TYPE	SUPPORT	3+MODEL	DATA A	7 C.G.	FULL	SCALE DA	TA
PN	T .ALPH	A PSĮ	L/Q	D/Q	PM/Q	'YZQ	RM/Q	· YM/Q
	1 0.0	1 -0.01	-10,333	11.567	=7.62	i 5:867	and the second s	-145.69
	2 :-2.0	5 -0.01	#16 · 167	11.933	13.87	5,493		=147c16
	3 -3.9			12.700	38 - 55	· 4.067	28.19	=141.76
	4 =6+0		=27,267	.13.607	62.43	: 2,833	31:07	=124 . 20
No.	5 '=7.9		=31.700	14.733	77 67	1 . 967	35.02	=114.92
	6 =10.0		=35.700	16.567	71.19	1.533	45 +53	=100 + 76
	7 -11.9		-36.833	18.967	34.26	: 2,400	48.13	×108.79
그 경기 가는 사람들은 사람들이 가장 하는 것이 되었다. 그런 사람들이 가장 하는 것이 없다면 하는데 되었다.	8 0.0		-10-300	11.600	-7.43	5.700	18.63	*145.49
그는 그 사람이 되었다. 그는 그 아이들이 가게 되었다면 그렇게 되었다면 모르는 그 없다.	9 : 2.0			The state of the s	3.1.444 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 . 607	13.18	≈135∗81
	0 4 0			11.593	:=39,41	5.533		<133+41
•	1 5.9		3.727	11.700	=49.29	5.233		=127 • 11
	2 8.0			12.033	=54 • 03	4 + 833		=121.67
and the second s	3 9.9		the state of the s	12.500	=51+36	. 4.833		=119+69
	4 12.0		16.400	13.267	-45 +41	. 4.500	****	-118.79
	5 0.0			가게 하게 하는 것은 것이 없는데 없다.	=7.98		The second secon	=144+36

VOUGHT		 and a six and a second at a	 / ~ ~

WIND AXES

RUN 114				11/	9/81	<u> </u>	146	e A Colonya dan	: 	1	RUN 114	
	. TEMP	7	4 •					PØ	14.5	5187	,	
GPSF ;	75+00	VF	28 2	56.50)	RNF	15	882	5 •	HACH	0.2264	
	TOT	102	7.03	704	T05	T06	T07	7.08	109	TIO		
	7.02 T11	0 T12 0	·74 713	0 T14	T15	716 0	717 1	718 0	T19	0 02°F 0		

AMES	SETYPE 8	UPPORT	+MODEL	DATA A	T C.G.	FULL	SCALE DA	TA
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	'Y/Q	RM/Q	. AW\ d
	0.02	*0.01	+11.867	11.700	20.12	6.247		-153.9 5
	:-2.03	-0.01	-18-133	:12:160	45.79	. 6,233		⇒159.56
	-4.02	-0.01	-23.833	12.753	77.41	. 4.787		-150-25
4	=6.05	=0,01		13.673	102.58	3 . 667		=140.33
5	-7.90	#0.01		14 # 900	109 + 84	: 2,333	39,67	=123.22
6	-10:05	=0.01	-37.400	16.660	101.09	1.833	49.26	=107.58
			±37.133	19.020	43,19	3,300	49+14	=122.68
	0.02	-0.01	-11.867	11.633	19.09	6.427	18.90	-155.71
	2.00	-0.01	-6.500	11.600	-2.25	6.260	11.28	-146.96
10	. 4.03	≈0.01	=1.900	11.633	=21+39	6:133	4,67	=141.97
.11.	5.98	=0.01	2.993	11.733	=36+25	5 . 867		=135+15
:12	8.01	=0.01	7.787	12.033	=46+25	5.600	=7.32	=133.86
13	9.99	-0.01	12.633	12.533	=52,26	5.433		=127.41
	11.99	-0.01	17,233	13.367	-58.04	5,200		=125.04
			-12,067		20+45	. 6.347	19.41	

WIND 'AXES

AME	S-TYPE	SUPPORT	HODEL_	DATA /	T C.G.	FULL	SCALE D	NTA	•
PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	'Y/Q	RM/Q	. AW\@	
	0.02	(1) 10.1 (1) (1) (1) (2) (2) (2)	*11·867	11.733	16.88	6.227	17 • 83		
	-2.03 -3.99		=18.067 =23.867	12.233	- 43 * 13 - 73 * 82	. 6.193 . 4.840		=158.57 =150.68	
- (4	=6.07		≠29.033	13.967	93+09	3,413	33 • 33 37 • 92	177	
5 6	=7 +90 =9 +94	- =0.02	#33.353 #37.133	15 • 013 16 • 767	104+75 97+34	. 1.940	48.66	-109.58	
7	-11.98		-37.967 -11.933	19:020 11:800	53.77 15.92	3/200 6167	And the second of the second o	=120.01 =152.68	
9	. 2.00	0.02	=6.533	11.700	=6+30	6.033	10.80	=144.54	
10	2 • 0 (=6.567 =1.433	11.767 11.867	#5+16 #26+19	6 1 133 5 1 8 0 0	10+85 =0:02	_ ,	
12	6.00		2.900	11.933	=39+94	5.733	=1.61 =8.21	=133 · 25 =129 · 09	-
			7.887 12.713	12.167	=49.07 =53.15	5.300	-13*25	-127-14	
15 16	12.00 =0.00		17.560 =12.040	11.833	*59.01 16.23	5.233 6.200	#18.52 17.89		-

WIND AXES

RUN 116 11/20/81 0911 RUN 116

TEMP 74. PC 14.5187

AME	S-TYPE E	IUPPORTS	+MODEL	DATA	T C.C.	FULL	SCALE D	LTA	<u> </u>
PNT	ALPHA	PSI	L/G	'D/Q	PM/Q	'Y/Q	RH/Q	' YM/Q	
	-0.00	-0.02	-9.800	11.533	* =7+64	. 5,313	18.62	=142+10	
	:-2.03	=0.02	-15.367	11.967	12.13	4 867	24.98	-145.20	
- 이 역가를 보고 밝혔다. 이 다 3	-4-01	-0.02	-20.367	12.833	27.51	3 400	. 29 • 40	=133.45	
- 4	6+05	-0.02	-24.580	14.213	40.52	: 2 + 400	32.71	=121 +79	
5	=7.94	· =0.02	-28.800	15 493	41+22	1.100	35.59	-102.92	
6	=10.04	=0.02	⊯32.467	17.220	32.17	1 • 187	42#28	94.57	
7		-0.02	=35.600	19.013		: 2,233	47137	₩107+24	15/5
		-0.02	-9.800	11+600	-8.35	5,353	18777	*143.73	4.39
		-0.02	=4.793	11.600	-25 • 66	5.500	11.57	=136.54	
10		=0.02	-0.600	11.660	= 40.55	. 5,533	4 • 61		
11	5.97	-0.02	3,433	11.760	=48.98	5 2500	-1.70	=126 · 78	
.12	8.00	=0.02	7.833	12.000	≒ 55•05	5 • 153	=7+14	=121.36	
13		-0.02	12.167	12 + 427	-53.17	5,000	-11466		-
14		-0.02	15.767	13.367	-48.96	4 900	-16:39		4
15		-0.02	-9.800	11.567		5.300	18#48		3.4

5.793

. 5,600

3407 ×131+24

=7.18 =127.46

			100	e doment				
genz			·	·····				
1	ya	UGHT L	SW SPEED	WIND TU	NEL TES	630		
								•
			WIND.	AXES			in the state of th	
£ , 6		187	2	1 2 2				ť ji
	RUN 117		**************************************	11/20/8	0911		. RUN	117
		TEM	87.			PO 14.	5187	
	GPSF 7	5*00	VPS 2	59.60	RNFT 150	2246	MACH OF	2264
		* TO+	702 703	TO4 TO5	TOK TOT	TOR TOR	710	
<u></u>		7.02	0 74		0 0	0 U	0	and the same of th
				T14 T15		T18 T19	T20	
		Ö	0 1		0 1	0 . 0	O	
	w.	.						
	C_TYPE R	UPPORT	o Manci	DATA		File	SCALE D	.
	3-11.14.4	OF CITY	SAMOUES	KALA	41		JUNEE D	7 I A
PNT	.ALPHA	PSI	م الراق م	D/Q	PM/Q	Y/Q	. RM/Q	YMZQ
	-0.00	0.00	68. 27	<u> </u>	-A.ka	5.727	21:07	=148·39
			*15.33 3					-149.61
, , , , , , , , , , , , , , , , , , , ,				113.593		3 967		-141+39
4		=0.01	=25.833	14.640	68+99			4130.11
5			≈31 •367		87 • 97	1,933		=116+40
6	⊭10.05	MO 01	≖35.367	17 • 647	78 • 40	2:000		= 108•91
	H12.01	-0.01	-39. 053	19.393	72.70	* 3,000		=118:57
	-0.00	-0.01	-9.647	:12.500	-8.97	5 • 667	The second of the second of the second	-148 · 15
<u>g</u>	. 2.00	-0.01	=4.900	12.367		5,500		=142.45
	. 4.02	#0.01	·	12:433	=37 * 66	6.007		■137 • 45
4.4		M M 4		4 24 54 2 199	1 1 10 4 4	E 700	~ 4 2 A W	-404 04

3.533

7.927

12.500

12 * 467 47 * 09

■54*77

12.500 13.133 =55.69 5.433 =12.95 =123.64 16.700 14.033 =61.35 5.400 =18.67 =122.68

#9.533 12.500 **8.25 5.633 20.80 *146.88

12.733

11 : 5.98 -0.01

14 :12.00 -0.01

9.99

8.01

15 -0.00

12

13

=0 :01

-0.01

-0.01

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A-120

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

0 0

TEMP 92. PO 14.5187 .

QPSF 83.00 VFPS 274.34 RNFT 1562144. MACH 0.2382

TO: TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 TI0

702 0 95 0 0 0 0 0 0 0

Ti1 Ti2 Ti3 Ti4 Ti5 Ti6 Ti7 Ti8 Ti9 T20

40 Administration des le Dalle militares	AMES	-TYPE	SUPPURT	S+MODEL_	DATA A	T C.G.	-FULL	SCALE D	NTA
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	DAY.	RMYQ	· YM/Q
er Marian Carlotte Ca	1	0.01		-8.886	22,801	=33 +60	5.855		=135+48
	. 3	0.01		=9.434	22 + 594	~28.63	: "+692	25.00	=134+69
, , , , , , , , , , , , , , , , , , , 		0.01			22.440	-23.40			
<u> </u>	4	0.01			22.560	₩20·71	#3·277	23.72	
•.	5		· #8.00	■10.223	22.976	=20+64	47 • 645	23.36	≈90.51
present the second seco	6	0.01		=9.458	23:825		×12.560	23.90	<u>=62.93</u>
	/		-12.01	8.855	24 • 699	-26.77	-17+139	24.55	-38.89
	. 8		-14.01	-7.759	25+181	+22.57	m21:440	25.48	-15.36
	. 9	0.01		-6.042	26.928	=32.89	#26+084	; 28.76	10.52
	10	0.01		=4.470	28 • 861	≈38 +98	#30:584	33+04	: 31.80
	11		.=20.00	-3.765	31.386	-47 • 16	=35:313	37.53	52.33
ACCRECATE TO THE RESIDENCE OF THE PERSON OF	12		<u> =22.00</u>	≈3.367	34 • 108		≈39.428	42192	. 66.79
	13		24 . 00	=3.771	37.458	*53.50	#44 + 247	49.79	86.05
	14		00.924.		41.319	-57 + 43	H49:428	64.93	.111+45
na an ann ann an an an an an an an an an	15		.=28.01	=2,488	45 • 458	-57 - 33	#55 · 211	92.28	133.98
•	16	0 * 0 1		=8.639	22:952	=33,32	5.512	23+89	∺133•06
•	えフ	0.01		=8°Q54	23.072	≈34.54	8 . 223	19,26	
. 6	18	0.01		-7 ∘ 741	23 • 169	=37.64	11:325		■127 • 65
	19	0.01		=6.946	23.699	#40 · 54	15,633	20.41	-149 - 18
	20	0.01	8.00	≈6.837	24.006	-43.65	18:084	21.15	-160-24
The second secon	21	0.01	10.00	-5.904	24.789	-49.47	21.958	20.62	=176+75
	22	0.01	12.00	=4.759	25+771	=57 •74	26.867	16.49	
	23	0 . 01	14.01	=3.843	27.108	=67+93	31.187	15.81	=231.50
	24	0.01	16:00	=2.566	28 • 705	F74+31	35.594	13.44	=256.24
čina pri i stali i koja se nimi i i i i i	25	0.01	18.00	=1.000	30.271	-74.67	41:114	12.15	=281 • 58
	26	0.01	20.01	0.102	32.855	-82.22	45 · St		-307 • 16
	27	0.01	22.00		35.596	-87.62			=307·45
والمستوارة والمستوار والمستوارة والمستوارية والمستورية والمستوارية والمستوارية والمستوارية والمستوارية والمستوارية	28	0.01			38.253	-78⋅65	:52+446	₩8.65	=305.09
i.	29	0.03		=3.458	41.367	=68+71	55 • 633		≠315.58
•	90	0.01			45.000	≒ 56⋅82	59,428		≈ 325.32
A CONTRACTOR OF THE PARTY OF TH	31	0.01			22.819	-34+39	5.512		H133.42
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A-121

CES. TEST JANNUT DNIW DESTE 630

WIND AXES

TEMP 84. PO 14.5089

OPSF 83.00 VFPS 272.44 RNFT 1590883. MACH 0.2383

TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TO9 TO

7.02 0 95 0 0 0 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T15 T20

	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	.A\d	RM/Q	. AW\0
	1	0.01		=8.910	22.681	=33+24	5:594	26.35	=145,68
	2	0.01		#9,458	22.452	:=28.60	: 3,283		-145-70
	3	0.01		=10.090	22.259	=24.71	-0.211		=136.17
7	4	0.01	=6.01	#10.307	22.434	=21 + 78	-3.193		=121.52
\	, 5		=7.99	#10.042	22.741	=21.88	-7. 259	24 * 35	≈98∗93
	6		=10.01	=9.699	23.524	=26.26	₹12.590	25 (32	≈69•11
	7	0.01	-12.01	-9.096	24.446	#30+14	-17,500	: 29+09	-43.37
	. 8	0.01	-14-00	-8.494	24.916	-21.01	-21:313	29 • 46	:=21 • 86
	9	0.01	+16.00	=6.446	26.807		=26.05 4	34 • 25	5.42
	10	0.01	=18.01	-4.970	29.006	= 40.59	431:681	44.31	30.61
	11	0 • 0 1	.=20:02	28.892	31.235	m42 · 48	#35.361	39.91	52 • 86
	12	0.01	-22.01	=3.964	34.247	=47 · 08	≡39:367	47.36	68.20
	13	0.01	-24.01	≈3. 795	37.861	=49.48	m45 + 151	65+30	89.46
	14	0.01	.=26.00	-3,090	41 + 825	-58.32	-51,295	92.68	113.85
	15	0.01	-28.00	-2.69	45.699	-59,33	=55,S34	106.95	134.13
	16	0.01	0.01	=8 • 645	22 0 8 0 1	=33+69	6 9 9 6 6	. 24.61	=144+42
	17	0.01	2.00	=8.313	22.861	=36,17	8,301	20 .72	=133.50
	18	0.01	4+00	=7.952	23.012	=38.72	11.247	19-74	■138 + 45
	19	0.01	6.00	-7.349	23,434	43.53	15.241	. 24+35	=171.03
	20	0:01	8.00	-6.777	23.976	-47.09	19,108	27 . 27	-188-02
	21	.0.01		=5,813	24,699	-55.31	168,52:		
	22	0.01	12.00	=4.735	25.602	=66,87	27.1289	23 12	-219.73
	23	0.01	14+00	≃ 3•747	26 • 687	= 79+33	31:446	23 + 75	
	-24	0.01	16,00	=2.380	28 • 133	=88,20	36,295		=268.09
	25	0+01		=1.169	29.518	=86+56	41 + 355		-290.80
	26			-Q.223	.32.078	-92.27	46.566	21.79	=327 • 17
	27	0.01		-1.018	34,711	-93.60	50.813	19.23	-346+39
	28	0.01	24.00	=3.584	38.313	=62.80	51.512		-291.13
<i>*</i>	29	0.01	. 26 • 01	=4.361	41 • 928	=51.07	55:018		=309.79
· •	30	0.01	28.00	= 5.633	45.735	=38 • 41	59 • 488		=327 +80
*	31	0.02	0.00		22.837	-33.99			=145.17

 VΦ	U(3 H	Ŀ	L	ЭW	S	PI	Έ	2	M.	Ih	ND.	1	U	NN	E	ΙE	SI	•	<u>3</u> ز	0
,	177																				. ,

WIND :AXES

. RUN 1	20	11/20/8	1 0911	RUN 120			
	. Tem	2 80.	P0 14+	4892			
GPSF	75.00	VFPS 258.20	RNFT 1525480+	MACH 0+2267			
	tot	T02 T03 T04 T05	TO6 TO7 TO8 TO9	710			
	7.02	0 89 0 0		Ó			
And the second s	Ö	0 1 1 0	0 1 0 0	Ö			

ومساور والمعارب والمعارض والمعارض والمساورة والمساورة والمعارض وال	AME	SETYPE	BUPPORT:	+MUDEL	· DATA '	AT C.G.	FULL	SCALE DA	ATA.
	PNT	ALPHA	PSI	.୮\፱	.ס/מ	PM/Q	Y/亞	RM/Q	· YMZ©
Andrew Co. and Marketon Conference of the Confer	1	0.01	0.00	-9,900	14.033	17.80	7,033	23.77	=128.73
	2	-2.04	0.00	-13.567	14.620	41.92	7 . 687	30147	=136.76
A	. 3	-3.99	0.00	#17.267	15.260	68.47	. 8,333		=146.69
	. 4	.×6 • 05		≈20.767	16.053	93 • 06	9,033		4156+90
	5	'=7 · 90	0.00	=22,400	16.940	93 67	9 493	52+80	=168.08
	6	m10.04	0.00	₩24.300	17.967	94 • 62	9 • 4 4 7	66 + 18	=177 + 81
	7	-12.00	0.00	-25.500	19.300	91.41	9 467	70+44	=183.27
	8	0+01	0.00	-9.733	13.993	17.23	: 6:867	24+40	-129 - 85
a to the state of	9	2.00	0.00	#6.500	13.633	-5.43	6.580		-126.56
	10	4.03	0.00	-3.033	13.300	=27.29	6,500		=125 • 15
	11	5.98	0.00	0.433	.12 + 967	=45.72	. 6:420	1 + 29	=124.77
	12	8 4 0 1	0.00	3.833	12.900	=64.57	6 • 467	-5+15	=129 +84
	13	9.99	0.00	7 . 467	12.800	EQ.88#	. 6+567		#133.64
	1.4	:12.02	0.00	11.333	13 - 187	-114+09	6.633	-19-54	=137.96
	15	=0.00	=0.02	-9.867	13.947	17.00	6.900		=129+14



WIND .AXES

5 5	RUN 1				11/2	20/81	09	11				RUN	121	
		TEMP	84	÷ •					PO	14+4	1892		,	•
	OPSF :	100.00 To1				245					er (Mad)	1.0.2	617	
<u> </u>		7.02	0	83	0	O	0 T16	0	0	U	Ö			<u> </u>

PNT	ALPHA	PSI	<u>L</u> /Q	'D/Q	PM/Q	YZQ	RM/Q	YMZQ
, 13.	=:	•	=; -	-, -		• • •		
	0.01	-0.02	-9.875	14.075	17:37	7.110	. 22.35	=128×23
	:-2.04	-0.02	-13.475	14.600	. 43.18	7,750	30 * 25	77
3.	4-02	-0.02	-17.325	15.275	72.01	8.350	37.71	=148.26
4	=6.05	-0.02	m20.450	15.950	94 . 23	9:075	43 *85	≈158 • 48
5	'm7.90	=0:02	-22,250	16.970	94 • 08	9,500	52.52	#266+51
6	'=7.90 ·	80.02	=22.275	17,025	94.15	9 • 430	52+74	=169·63
7	-9.57	-0.02	-23.825	17.710	98 • 16	9,430	62.47	■177 • 63
	0.02	-0.02	=9.725	14.075	16:18	6.950	22.72	-129.24
	: 2.00	-0.02	=6.275	13.605	-5+73	6.510	15.28	■125 • 36
10	. 4.02	=0 2.02	=3.000	13.325	=27+63	. 6,300	7 28	-125.37
.11	8.01	-0:02	3.750	12.950	= 65•35	6.385	=6.15	=131.57
12	10.00	-0.02	7.550	12,905	=88.69	6 475	=12.61	4135.40
4 3	:12.00	-0.02	11.325	13.250	-114-32	· 6 • 185	=17.90	
	-0.00	=0 .02	=9.875	14.025	17 + 43	7:050	23.53	-129.76
성공에 그 교회에 세칠었다였다.							 The state of the s	

WIND AXES

RUN 122			11/3	0/81	09	11		(<u> </u>	RUN 122	s.
	TEMP	80.					PO	14+4	892	••	
QPSF 75.	00	VFPS 2	58,20)	RNFT	152	548() .	MACH	0 . 2267	
	TO1 7	02 703	T04	T05	T06	T07	708	FUT	T10		
	7.02	0 92	0	0	Q	Q	0	0	Ö		
•	T11 T	12 T13	下14	T15	T16	T17	T18	719	T20		
	. 0	0 1	4	0	ń	4	0	0	a		

PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	. RM/Q	. AWNG	
	0.01	-0.01	-9. 933	16.180	3.70	7.233		=140.33	
2	:×2.03		-15.500	16.680	21.12	7 • 100		-145.53	
3			-20.967	17.273	45+04	· 6 • 3 4 7		=144+09	4
· 4	=6.05	=0.01		18.133	68.12	5 : 833	40 • 41		
5	-7.92	= 0 <u>0</u> 0 1	■30,667	19.193	76.16	5 • 5 6 7	44 * 80		
6_	=10+04	=0 + 01	=34.600	20.707	72.36	5 • 167	52 • 92		
	-12.00		■38 • 867	22.327	64+84	5.467	62.99		19.
	0.02	=0.01	=9.700	16.267	3.25	7.187		=139.77	6
9	: 2.00	-0.01	*5.033	16.067	≈9∙85	7,300		#134.56	
10	4 • 0 4	-0.01	=0.613	16 • 267	≈24•83	7 4 4 6 7		=130+24	
11	5.98	=0.01	3.767	16.300	=33.35	' 7.•300		=127.57	
12	8.01	MO.01	8.267	16.700	-42.28	6.920	=8.10	=124.25	•
13	9.99	-0.01	12.627	17 • 133	=43.08	7.100		=121.59	
14	12.00	-0.01	16.867	17.953	=49.09	6.567	-17.77	#122.06	32.4
15	0.02	-0.01	-9.933	16 4167	3.56	7 . 167	21.05	=140.53	2544 25. 1. 1.

WIND AXES

::: **********************************	RUN 1	RUN 123			11/20/81 0911							RUN 123			
		TEMP	8 8 6) •				v	PO	14+	1892				
	QPSF	75+00	VFF	S 2	58 • 20)	RNF	152	2548) •	MACH	0 . 226	7		
	ig to be the second of the sec	TO1	102	T03	T04	T05	T06	TOT	108	709	Tic	······································			
The state of the s		7.02	0	92	0	Q	Q	Q	Q	O	Q				
		111	712	T13	下14 1	(15	716	117	1.18	: 0	0				

والمتعارض	AMES	TYPE	SUPPORT	+MODEL	DATA A	T C.G.	FULL	SCALE DATA	
	PNT	.ALPHA	PSI	·L\Q	Ď∖Œ	PM/Q	Α\r	RM/Q YM/Q	
	1	0.02	-0.01	-9.95 3	16.300	4+58	7:173	20.81 =141.57	
and the first of the second	2	-2.03	-0.01	-15.333	16.753	21 + 43	6 887	28+84 -144+44	
profession of the dis-	3	-4.02	-0.01	-20.833	17.320	46 + 44	6 . 187	34.51 =145.63	}
		-6.06			18.200	67+90	5 4 6 0 7	39.98 =141.32	2
•		-7.91		#30.333	19.200	75.81	5:460	45.08 =138.37	7
		10.04		-34.200	20.733	69 19	5 . 107	54+20 =134+84	+
Company of the Compan		112.01			22.413	63.72	5.773	61+77 =141+89)
er en la	Ŕ	0.01		-9.633	16 • 233	4.29	7.007	20.93 #139.60	5
	Ğ	2.00		=4.967	16 • 167	≠9.98	7.273	. 11.95 m134.50	
was a superior of the superior	10	4.03		=0.633	16.307	=24+43	7.507	2#40 #130+53	
	11	5.98		3.667	16.333	=34+11	7. 240	#2.92 #127.64	
	12	8 • 01		8 • 267	16.800	=42.31	7.007	#9.07 #125.7	
	13	9.99		12.520	17.+280	-44.26	7:140	-15.21 -120.8	
4.参小		12.02		16.667	18 • 033	=51,60	6:453	#18.99 #122.4	
	14				-77		6.940	21.47 =138.7	•
	15	0.07	. =0.01	=9.800	16.267	3.20	0 2 3 4 4	LATTE TISSEE	

WIND .AXES

RUN 12	TEMP	80		11/	20/81	LAU	71.1	PO	140	4892	RUN 1	4	
OPSF		3 4 5 3									0 • 22	67	
406	7.02	702	<u>703</u> 74	704	105	T06	T07	801	<u> </u>	T10 0	<u>ي نسستندن</u>	مغارف موسي أرأس المحادث	
	T11	T12	713	T14	T15	T16	T17	718	T19	T20			

AME	3-TYPE	SUPPORT	S+MODEL	DATA A	T C.G.	.FULL	SCALE DA	\TA
ТИЧ	.ALPHA	PSI	٠٢/٥	D/Q	PW\0	'Y/Q	RM/Q	· YM/G
	0.02	-0.02	-8.800	13.193	≈1.29	7,733	: 23.15	×159.27
	:-2.03	-0.05	p13.767	13.800	21.39	7.040	31.85	≈160.03
	₩3.95		=18.767		50.58		37.40	=155.69
- (- 4	#6+05		#24 · 100	15.700	74 • 43	5,460	41.35	=149+49
5	`≈792		=28:167	16.867	88.31	5 . 800	48+10	=149.86
6	#10+0			18.993	72.66	5 . 9 4 7		=146.01
	=11.98	-0,01		***************************************	72,69			-157.99
			-8.767		-1.43	7.700		=158+65
	. 1.95			The state of the s	=18.09	and the second s		≈150•17
10	. 4.03		0.513	13:067	=33+40	7.900		m145.56
11	5.99	=0.01	4.500	13 • 167	#44.56	7.413		=140.51
12	8 • 00		9.033	13.367	=51 • 83	6 • 833		≈134+45
13.				13.987	#54+09	- 6,647		=127.41
	12.00		17,533	15.080	-62.22			=128.20
15				13.200	-2.81			=159∗ 09

PC . 14.5	FUN :32	
-	1187	
8131.		
	MACH 0 .2264	
- A		
0 0 0	0	
718 T19	,	
0 0	0	
RFERENCE FULL	EFFECTS SCALE DATA	
DYY.	. RM/Q · Y	/M/G
. 4.434	. 23+84 -15	4 Table 1 Tabl
. 4,454	30.45 =15	
. 4,561		
4+271	42 77 =15	
4 4 4 5 3	49+19 =15	
5 • 631	57 •89 =17 68 •54 =18	
6.666	71,51 =18	The state of the s
6.408	77.89 =18	
· 4.580	24.62 =15	
. 4.422	18 • 40 = 15	
· 4.213	12+94 =14	
4 259	=0.47 =14	
4,259 4,591	-8-23 -14	
. 4,591	=14 87 =13	
· 4,591		
· 4,591 · 4,500 · 4,869	=30+24 =12 =33+97 =13	
	4 9 8 6 9	4,869 =14,87 =13 5,779 =25,21 =12

0.00 39.774 17.159 457.44 4.556 -35.82 -137.51

25.346 =116.92 . 6.680

5 • 401 38 • 47 · 4 • 267

42.960 20.019 -82.33 5.047 -41.31 -145.66

23.492 =106.59 . 5.890 =49.41 =150.56

=56+04 =153478

24+79 =154+69

20 20.24

21: :22.24

22 24.28

23 25 24

0.27

24

0.00

0.00

0.00

0.00

46.618

49,393

-1.942

		,	Y	BUGHT L	W SPEED	WIND TU	NEL TEST	r:630	latiga - tuga kuntha nguni an	
					WIND.	AXES				
*		: 12 - 12 - 12 - 12 - 12 - 12 - 12 - 12	RUN -3	3		11/20/8:	0933		, RUN	:33
				TEM	86.		•	PE . 14.	5187	
- ar - ar		,	QPSF	75+00	VFP8 2	59.36	RNFT: 150	5745.	MACH O	2264
	3.			TOS	T02 T03	T04 T05	TO6 TO7	TO8 TO9	T10	
aliquita, ata instructiva de la constanti				O	0 33		31, 0	0 0	0	· · · · · · · · · · · · · · · · · · ·
				. T11	T12 T13	T14 T15	T16 T17	T18 T19	TZO	
· · · · · · · · · · · · · · · · · · ·				Ö	0 35	32 0	0 1	0 0	1	· · · · · · · · · · · · · · · · · · ·
		# # 3.3		CO	RECTED	FOR TARE				
		SING	LE SUP	PORT DA	<u> </u>	DATA	AT C.G.	FULL	SCALE D	ATA
		PNT	.ALPHA	PSI	L/Q	0/9	PM/Q	Y/0	RM/Q	YMZQ
· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	1	0.26	0.01	-2.017	5.230	· 44×73	. 6.021	. 28.05	#168+44
in the second		2	0.26		-2.088		47.53	2.041	27.90	
· · · · · · · · · · · · · · · · · · ·		3	0.26			5.395	45.87		24+84	=120÷92
(. 4	0.26		=1.706		41 + 21	=6 (195	23 • 88	
A		5	0.26		=1.027			910.230		•
***************************************	· · · · · · · · · · · · · · · · · · ·	6	0.26		0.002			≈14 • 656		
		7	0.26	-12:00	1,175	8 415	14.92	-19,710	14.25	-20+80

	· · · · · · · · · · · · · · · · · · ·									
	1	0.26	0.01	-2.017	5.230	· 44×73	. 6.021		m168+44	
	2	0.26	-2.01	-2,088	5,279	47.53	1 2.041	27.90	-147-38	
and the same of th		0.26	-4:01	-2.027	5.395	45 • 87	.m2.102	: 24+84	-120+92	حسنيد
(. 4	0.26	=6.00	=1.706	5.658	41 * 21	=6 (195	23 • 88	=104.23	
Marie Control	5	0.26	=7.99	-1.027	6.240	33,92	910.230	20+44	-76+34	
	6	Q . 26	≠9 ∗99	0.002	7.011		≈14 ± 656	16+74	·=46 · 65	
	7			1.175	. 8 • 415		-19.710	14.25	-20+80	
	8		-13.99	2.152	9.871	9+64	#24 c389	12,52		
	9	0.26	-15,99	3.189	11:466	3.75	m28+631	11.89	. 42.18	فسيند
	10	0.26	≈17 •98	4 877	13 * 411	≈6 • 85	#33,380	10.56	74 + 09	
	11		EO.05=.	7,027	15.853	=18+99	#37 927	8 : 17	113.80	
b	12		.=22.00	9.013	18.708	=36.12	■43 • 044	4 4 1 3	152.85	
A Comment of the second of the	13		.=23+99	11.508	21.846	-52+75	#47 .716	=3,21	181 + 98	
;	14		-26.01	13.923	25.057	=68,21	=52:118	-3.46	199.56	
	15	0.26	-28.01	15,826	28 • 195	-80.72	■55 • 775	#3 63	205 • 18	حنفد
	16	0.26	=30.02	16.418	31.051	=77+16	.58.819	0 .56	203+83.	
,	17	0.26	0 + 0 0	-1.684	5 • 297	43 - 65	6 6 6 9 7	. 25 • 80	-172+14	
,•	18	0.26	2.00	=1.948	5.429	43 + 74	10.422	27+19	-184.42	
,	19	0.26	3.99	-1.880	5.841	37.55	13.612	31.18	#196+25	area in the same
	20	0.26	5.99	-1.599	6.280	28.46	16,328	33.25	-197-29	
	21	0.26	7.99	-0.782	6.944	15.36	19.871	35.14	E8.405=	
	22	0.26	10.00	0.376	7 . 716	1 + 84	123 . 544	37.76	=218/91	
	23	0.26	11.99	1.556	8.902	≠9 86	28:129	40.76	=240.45	
	24	0.26	13+98	2.685	10.665	≃18 • 29	.32 • 959	40.73	=258+47	
	25	0.26	15.99	4.157	12.351	-30.32	38,229	42.73	⇒288 •13	
	26	0.26	17.99	5,930	14.233	≠ 45+83	:42.836	45.57	-316.57	
	27	0.26		7.926	16:627	≈58 · 84	48.338	48.98	-360.05	
	28	0.26	22:00	10,072	19 • 149	≖76+28	:53:678	52.81	#403.22	-
•	29	0.26		11.667	22 • 121	=87 ∗93	.58,423	53 - 77	431 •83	
,a	30	0.26	26.00	13.072	25.263	≈94 • 68	63+347		=465.66	
See NAME OF STREET	31	0.26	28 (01	13.271	29.927	357.40	63 141	13.72	=398+36	orientarionic?
,	32	0.26	30.01	13.183	32,925	=47.33	66:196		-405.28	
otherwise where the other time.	33	0.26	0+00	-1.451	5.230	44.88	6.037		=169.27	
									The same of the sa	

A-129

47.208

52.618

52 1709

57.604

62 1270

62.812

65,825

5.330 . 41.64 : 5.510 . 29.28 -164-04

=57.58

-72.66

-71:92

=86.31

-93 - 76

-48.04

29.803 - -56.82

· 49.65 =358.86

53+64 -401+74

53.77 -400.99

53:37 -433.94

53+00 =463+95

15.47 =404.87

3.39 -406.40

Co.						in a Turk of the extremely a second of the extremely and the extremely a second of the extremely a second of the extremely and the extremely a second of the extremely a secon		
	·γ	BUGHT LE	W SPEED	WIND TU	INEL TES	1:630	e Sy	······································
		i						
			WIND:	AXES				
			ga Nebesi (2)					
50 - 10 10 10 10 10 10 10 10 10 10 10 10 10	will 6	in the state of th					G. IA.	
	RUN 3	<u> </u>		11/20/8	0933	<u></u>	: RUN	
		TEMP	86,		ı	88. 14 m	5187	
	QPSF.	13. 00	VFPS 2	72.85	RNFT 15	34019.	MACH O .:	2382
				T04 T05				
,		0	0 33	0 :13	31 0	0 + 0	0	
		_		T14 T15	116 117		1-20	
	and the	<u> </u>	0 :32	.35 0	<u> </u>	0 0	National Property	
			ner de de la	EAG TIDE	chie Stan	TERCOCNA	- cdpcor	경우 다 그렇게 되고 않는 목록하다 사람들은 사람들이 되었다.
	NGLE SUPI	BART NA	KRELIEU	FOR TARE			SCALE D	
3.4	AGE POR	KUKI UKI	(A	DALA	AT C.G.		SCALE D	AIA
PN'	T ALPHA	.PSI	L/9	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
	1 . 0.27	0.01	=1.868	5 • 197	. 42,47	5 • 688	: 29.04	=165,78
	2 0.27	-1.99	-1,966	. 5.347	43.56			=138.16
I man a second a seco		4+00	-2.071	5.540	. 41.92	3.217	26.57	-114.02
	4 0.27	· =6+00	#1.732	5•937	36 ⊭23	*=ブ・401	25+40	=96.41
	5 Q.27	=8 ,07	=1 + 1 0 4	6.533	29 . 82	m11.802	21.80	=69.23
		=10+00	-0.207			≈16+241	17.71	
		.=12.00	0.942		10.91	#21:282		
그 그 씨는 그 그 그는 그 가장이 가지 그를 입었다. 그 그는 비를 가게 되었습니다. 어느의		-13.99	1.832			=25,699		15.70
		=15.99	2.938			-30.267	12+74	
1		-17 •99	4•465		=8.56		10 + 89	
1		: = 20.00	6.707		=18,29		9.78	
1:		:=22.02	8.931			#43 · 805	4 • 66	
		.=23.99	11.229			m48 9427	0.02	
		'-26 KO2				452.281		195 • 67
	5 Q.27		15.694			■55 •568	1 • 1 4	
1			16.086			m58:231	4 • 88	
. 1			=2.230		38+96	6.111		=167 • 08
1		2,02	=2.137		38+63	9,650		≠179+64
			-2.024	5.945	32.28	:12.597		-191.02
			-1.800					=193.61
		7.99						=201·82
.2			0.021		0 . 89			=215+84
2			1 • 188		=9.87			#237 #09
2		13.99	2.206		=16.73	:32 • 494		=255+52
2		16.03	4 - 044		-29.71			=288+24
2		17.99	5 • 637		=42.48			=315.83
v (⊅)	7 0.27	19.99	フェッフク	44.346	-57.FO	47.2nc	LQ.KR	-258.94

7.372

9.468

9.408

11.702

13,008

12.752

12.695 32.639

16.369

18.981

18 • 945

21 + 953

25.094

27

28

25

30

31

32

33

0.27 19.99

Q.27. 21.98

0.27 21.98

C:27: 28.00

24+00

25.99

29.99

Q:27 =0:01 =2:194

0.27

0.27

0.27

A-130

0.296

≈0.555

1:203

-7.87

1.78

=11.81

=10.36

=11.87

	•					,	19-0 E-7-	· *	
							A STATE OF THE PERSON NAMED OF THE PERSON NAME	erican de la calendario d	nitra nitrata ny maninta ara-
		, va	UGHT Le	W SPEED	WIND TU	NEL TES	630		a de la companya de l
			•						
				WIND.	AXES				
			i i i i Ali 🦫 Ali i Ali	* * * * * * * * * * * * * * * * * * *)·	,
	<u> </u>	RUN 35	·	4-50	11/20/8	0933		. RUN	35
			TEMP	68+			PO 14+6	464	
**************************************		GPSF 7	5.00	VFPS 25	53/194	RNFT 15	78041.	MACH O +2	2254
						and Sales and			
		 	101	0 :32			108 TO9		
	·		-		0 14 T14 T15	31 0 T16 T17	0 · 0 718 T19	0 T20	
	•		0	0 32		0 1	1.10 (1.13	0	
		- (A) (A)					<u> </u>	, , , , , , , , , , , , , , , , , , , 	
	SIN	SLE SUPP				AND INT	ERFERENCE FULL	EFFECTS	
	PNT	ALPHA	PSI	L/9	· #\ / #\	BH / 6		•	
	1.181	'WELLIA	1.01	<u>L</u> / 4	D/Q	PM/Q	.A\ñ	RM/Q	. JW/ō
	1	0.25	-0.01	-1.975	4.794	32.51	-0,555	.2.31	-10.99
기 기계	. 2			=8.437	4.934	51.91	-0.489		• •9•58
_ /	3	=3.78	-0.01	-14.863	5.366		=0.258	5.21	=11.78
(4	i=5∗78	=0.01	=21.245	6.123	98 • 67	=0:125	5 . 62	=11+49
	5	- 7•7 7	~0.01	=27.278	7.+207	113.10	=0:144	6 47	.=12.71
	6	=9.77	=0.01	=31.484	8.753	106.21	0 • 169	5+64	=15∙85
	7	-11+77	-0=01	-37.298	10.629	97 • 66	-0:092	7.61	-15.97
	3	-13.77			.12.637	104 . 68	-0.790	7.33	.=14+37
	9			-46.556	13.850	106.36	-0.980	7.06	=17.06
	10	0.24	=0.01	=2.008	4 827	32 • 44	=0:356	2 * 33	.=11+89
	11	. 2.26	=0.01	3.843	4.908	21.10	#Q+46U	1.37	=15.57
	12	4.26	-0.01	8.461	5 • 109	13.36	=0.506	0.11	-16.52
	13		=0.01	13.183	5.361	8+71	-0.295	-1.88	-18.72
	-14	8.25	-0.01	17.781	5.947	11.37	-0.057	=3.58	=18+79
	15	10.27	-0.01	:22.712	6.858	14.61	○ 0 • 175	-5.16	-18.18
	16	:12.25	=Q:01	27,566	.7 • 594	17 * 85	=0.032	=6 +35	-12.24
	17	14:28	#0.01	30.545	9.882	1.84	0:828	=10.78	-3.23
	18	16.26	-0.01	33.606	11.446	4.31	1.890	=14.60	-4.52
	19	18.30	-0.01	36.321	14.122	=26.72	0.875	=12.09	r =9×04
	20	20.26	-0.01	39.774	16+715	-54,19	-0.266	-6.90	-9.00
	21.	:22.27	-0.01	42.608	19 + 657	=79,26	-0.843	· =4.68	-11.82
	22	.24.25	-0.01	15 167	00 700	100	0.204	-7.47	-10.06

.22

24

-24 - 25

0.26

23 25 28

=0.01

=0.01

=0.01

45.667

=1.741

22.780 =100.65

· 4:827 32.54

49.105 25.125 =114.16

	بالانتباء تناسب	<u> </u>		<u> </u>	IN GPECO	ALNO IDA	INEL TEST	, <u>, , , , , , , , , , , , , , , , , , </u>	 	<u>,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>
					WIND (AXES				
			RUN 36			11/20/81	0933		: RUN	36
				TEM	68,		• .	PO 14-6	5464	
		1 2 4 5 20 40 20 40	QPSF 7	5.00	VFP8 2	53+94	RNFT 15	78041.	MACH 0+2	254
				rot	T02 T03	TO4 TO5	TOA TOT	708 TOS	T10	
<u></u>	فقتل تلطن الألبيراني		<u> </u>	0	0 32	0 15	31 0	0 . 0	0,	
				T11				718 T19	T20	
				0	0 32	.35 0	0 1	<u> </u>	<u>, Ò , , , , , , , , , , , , , , , , , ,</u>	
		SIN	LE SUPP			FOR TARE	AND INTI		E EFFECTS	
•		PNT	.ALPHA	,PSI	L/G	D/Q	PM/G	.A\d	RM/Q	. AWN8
WY W.	Allen	1	0.26	-0.01	-0.898	. 4.706	15,71	-0.988	=1+34	· =0*20
		2	-1.75	-0.01	-7.567		33,26	-0 ∗843	-1.16	0•33
وللمستحدث	<u> </u>	3	-3.76		-13.717	,	51 . 70	-0.421	0 • 1 4	3.14
		4	¥5 • 75	#0.01	×19.444	5 + 953	52,90	=0:424	0 • 50 1 • 05	· =3+34 · =4+29
.		5	'=7 • 7 · 7 · 7 · 7		=24 • 251	7.347	71 • 36	=0.383 =0.308	1 + 94	· = 7 • ⊆ 2 = 5 • 38
	No. 100 100 100 100 100 100 100 100 100 10	<u> </u>	=9.76 =11.77	=0.01 =0.01	=29.574 =35.871	8.609	74.44 80.67			-3.38 - 4.98
		8	■13.75	-0.01		11.942	89.55	-1.355	2.14	=6.27
		Š	-14.76		-45.909		95.91	-1.572	2 * 95	-6.83
		10	0.26	=0.01	-0.998	4 • 706	15.76	=0.888	=1+06	• =0.59
		11	: 2.27	-0.01	4.543	4.835	7+33	=0.977	- =0+94	-0.51
		12	. 4.29	=0.01	9.171	4.950	2.40	=1 . 122	=0+09	· =1 · 88
		13	6:25	=0.01	13,816	5,252	0.30	-0,991	=0+57	-3.35
		14	8 . 25	-0.01	18.220	5.748	4 + 84	-C.715	-2.44	-5-24
		15	10.25	-0:01	22.738		14.65	-0.356	-4-49	1 =5 . 66
			:12 * 25	=0.01	26.653	7.758	35 • 52	=0:353	=5.31	=2+86
			14.25	=0.01	28.242		43 • 01		=7 +59	6 • 82
			16.25	=0.01		11 • 195				4 • 0 4
			18.28		1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m 1 m			0.716	The second second second	=0.73
			20.24	-0.01		16.812			- 14	-0.73 -3.24
		21		-0.01		19.667			=3.46	-4.39
								[14[11]A	#J 640	
			24 24	=0:01 =0:01	46.291	22.940	≈99 €55			02.46

original page is of foor quality

A-132

VOUGHT LOW SPEED WIND TU	NNEL TEST 630
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			WIND	:AXES							
	RUN 37			11/2	20/81	093	á		, R	UN 3	17
		TEMP	80.				₽đ.	14-6	5464		
	QP6F 7	5.00 701	T02 T0				153373 07 708		MACH T10	0 422	5.4 tu 18
·		T11 0	T12 T1		T15 0		17 718	T19	T20 0	.,,,,,	was programmed and a second of the second of
SING	ILE SUPP						NTERFE				
PNT	.ALPHA	PSI	L/ (g į	۵/۵	PM/	, œ ,	YZQ	RM/	Q	YM/Q
1	0.24	-0.01	7.57	73 3	338	-112.	66 =0	.710	=0 €	51	2.38

SIN	GLE SUPP	OK L.UA	r <u>a</u>	DAIA	A. G.G.	PULL	SCALE U	IA
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	. Y/Q	RM/Q	YM/Q
	0.24	-0.01	7.573	3,338	=112.66	-0.710	=0.51	2.38
	-1.73	-0.01	3.481	: 3 • 1 4 9	m133.55	TO+492	m0.42	1.06
7 2 3 3 3 3 3	1-3.75	-0.01	-0.153	3.115	-152.38	-0.134	=0+64	1.66
4		=0.01	·=4 . 151	3.395	-171.30	=0,137	=0.28	. ≥0.82
5	-7+75	m0.01	≈8 ∘044	3 • 821	=189.46	-0:107	×0.45	-2.04
6	-9·74	≈0.01	=12.570	4 • 479	=204.50	=0.020	=1.07	=2.55
7	-11.76	-0.01	=17.745	5.262		=0.143	-1.63	-5.16
	-13.73	-0.01	×22.883		-223.79	-0:518	-2:73	-5.85
	-14.76		-25.138		-227.85	-1:052	-2.66	=7 - 15
10	0.24	=0.01	7.539	. 3.272	-112.10	=0.0604	=0 ●40	1.57
11		#0.01	11.209	3.588	×90+26	-0.775	0+04	0.61
12		· =0 :01	14.363	3 * 886	≈70.01	=0.875	=0:12	0.06
13		0.64.		4.406	-50.54	-C*787	=1.27	-0.43
		-0.01	20.845	5 * 0 4 6	-31.30	-0.442	-2.87	-2.33
		-0.01	24.323	5.914	=9.54	0,126	=6.28	-3.46
• 16		-0.01	27.975	7.108	11.89	0.317	=7.98	=1.96
17		#0 e 01	28.932	8.922	29.52	1:255	=15.07	8.00
. 18		m0.01	31.213	10+637	45.31	1.941	-16.07	7 • 17
1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		-0.01	30.789	12.692	60.62	0 : 5 + 5	-8.20	0.70
		-0.01	31.647	14.789	72.62	-C.7.83	-5.23	1.28
<u>21</u>			32.469	16.536	85.30	-0.721	-3.65	=1.02
22		=0.01	34.128	18.756	98.10	-0:025	=3,45	0 • 89
;23		0.01	36.109	20:120	103:10	0,925	=8:02	0 • 86
24		=0.01	7.539	3.338	-112-13	-0.717	=0.40	1.47
	W. T. W. T.			3.000	++			<u> </u>

VOUGHT LAW SPEED WIND TUNNEL TEST 630 WIND AXES RUN 11/20/81 0933 : RUN 38 TEMP 85. PO . 14.6464 GPSF 75.90 RNFT 1501650 # MACH 0 2254 VFPS 258:94 TO\$ 702 TO3 TO4 TO5 TO6 TO7 TO8 TUS TIO 0 32 0 17 31 0 0 0 Ø Tit Ti2 Ti3 Ti4 Ti5 Ti6 Ti7 Ti8 Ti9 T20 0 32 :32 ..0 0 CORRECTED FOR TARE AND INTERFERENCE EFFECTS SINGLE SUPPORT DATA DATA AT C.G. FULL SCALE DATA Y/4 PNT .ALPHA PSI 1/0 D/Q PM/Q KM/Q YM/Q 3.869 -107.97 . 5.438 . 21.18 -151.33 . 0.24 -0.01 7:181 -1.76 ***0.01** 3.686 =129.65 > 5.691 . 26.88 **-158.41** 3.234 3-3-74 -0.01 3.682 -146.90 6.399 33.23 -163.51 -0-337 W5 . 74 · =0.01 39+25 =167+38 6,596 =4.166 3.889 =167.64 3 =0.01 46.41 =171.86 ≒ファフフ **=7.962** 6:823 4 * 330 = 183 * 65 =9 : 74 =0.01 =12.539 54.09 =179.51 5.025 =196.60 7 . 379 -11.75 =0.01 =17.829 60 43 -179 43 5.761 =204.66 7:329 -0.01 -22.868 8 -13.78 . 6.853 =214.20 . 6.739 . 65.58 -171.19 -0.01 -25.112 9 -14,78 7.562 -218.90 6 . 400 . 68.37 =166.72 10 0.25 #0.01 7,348 3.909 =107.11 5:471 . 21:23 m151:56 11 2 . 25 **=0.01** 10.858 4.258 ***87.08** 4 # 504 15+83 =143+72 =0.01 12 . 4.24 13.709 4 + 480 11.03 =136.53 4 • 603 =68 · 78 £3 -47:49 . 4:060 6 . 26 **#0.01** 17,173 5.050 4.40 -133.09 , 4 =0.01 -26.90 . 4.401 8.26 20.670 5.595 -2472 WE26+41 15 10.25 a0.01 24.115 6.506 -9 83 -126 11 -6.50 4,893 27.617 16 :12:26 =0.01 7 + 647 5 130 #16.81 #127.12 15.02 17 =0.01 14.24 28 . 716 9.542 6:139 #28 #97 #120 +26 33 + 86 =0.01 18 16.24 31.213 50.36 6.788 =36.48 =119.14 11:189 64.47 19 -0.01 . 4.906 #34.59 #129.42 18 . 25 31.680 13.119 20: 20.26 -0.01 31.777 15 - 178 74+25 . 4.358 #34 .62 **#131 .78**

21

22

23

22.27

24.26

25 + 25

0.23

-0.01

=0.01

=0 * Q1

-0.01

32.798

33.781

35.563

7 . 114

17.176

19.248

20.661

87.38

95 + 17

98 + 10

34909 =109.02

4.533

5 + 481

5 . 271

. 6.252

-38 +94 -137 +15

#48+99 **#136** •86

=53.76 ×136.53

21.33 -151.73

(Vđ	UGHT LE	W SPEED	WIND TUN	INEL TEST	630	ىلىدىنىنىدى <u>د ئىسىيە سومات بىز چىستىد</u> ق	
			WIND :	AXES				
			*:					And the state of t
	RUN 39		j. c.	11/20/81	0933		RUN	
alayan ali da an in alika pangangan da an angangan da da an	RUN 33	<u></u>		11/20/01	<u> </u>		- <u>- </u>	
•		. TEMP	94.		,	PO. 14+6	6464	
	GPSF 7	5.00	VFPS 2	60.12	RNFT 148	14616.	MACH Des	2254
and the second s	<u> </u>	TOP		TO# TO5				
			0 39	0 18	31 0	0 0	0 T20	
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 32	T14 T15	116 117	0 0	120	
	40,		<u>, , , , , , , , , , , , , , , , , , , </u>	JE U	<u> </u>			
		CO	RECTED	FOR TARE	AND INTE	ERFERENCE	EFFECT	s i
SIN	GLE SUPP			DATA	T C.G.	FULL	SCALE D	ATA
(<u>(1.1.4), </u>							,	
PNT	ALPHA	PSI	L/Q	ĎΛŒ	PM/@	.A\ñ	. RM/Q	. AW50
	0.27	0.01	-0 400	. 2 • 686	-02.04	5 1 4 6 4	27-89	=156.16
	the state of the s		-0.888		=93,26 =110.81			-161+20
2		0.01	=3.078		=126 · 36	6.563	Control of the Contro	=175.56
4	=5.77	0:01	=4,210		=143.69	7:471		= 185.59
5		0/01	=5.325		=158.74	8,123		=195+54
6		0.01	=6.688		=171.02	8 • 434		=201 +60
	· · · · · · · · · · · · · · · · · · ·			0 4 0 1 0				=198.89
7	-11.74	0.01		4.192		8.090		
	=11.74 =13.75	0.01	-8,097		=181.96	8,090	70.35	=188+94
8	-13.75	-0.01	=8,097 =9,477	4.872	=181 +96 =193 +66	. 6,548		=188+94 =185×18
3 1	=13.75 =14.76	0.01	=8,097 =9,477 =10,283	4.872 5.255	=181.96 =193.66 =200.08	. 6,548 . 6,545	72.94	=185×18
8 9 10	=13.75 =14.76 Q+24	0.01 0.01 0.01	=8,097 =9,477 =10,283 =0,924	4.872 5.255 2.685	=181 • 96 =193 • 66 =200 • 08 =93 • 79	6,548 6,545 5,467	72 •94 24•07	=185×18 =154+04
	=13.75 =14.76 0.24 2.25	0.01 0.01 0.01 0.01	=8,097 =9,477 =10,283 =0,924 0,167	4.872 5.255 2.685 2.841	=181:96 =193:66 =200:08 =93:79 =78:00	. 6.548 . 6.545 . 5.467 5.009	72+94 24+07 17+00	=185×18 =154+04 =146+30
10 11 12	=13.75 =14.76 0.24 2.25 4.26	0.01 0.01 0.01 0.01 0.01	-8,097 -9,477 -10,283 -0,924 0,167 1,368	4.872 5.255 2.685 2.841 2.830	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62	6.548 6.545 5.467 5.009 4.394	72+94 24+07 17+00 10+60	=185×18 =154+04
10 11 12 13	=13.75 =14.76 0.24 2.25 -4.26	0.01 0.01 0.01 0.01 0.01 0.01	-8,097 -9,477 -10,283 -0,924 0,167 1,368	4.872 5.255 2.685 2.841 2.830 2.863	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62	6.548 6.545 5.467 5.009 4.394 4.347	72.94 24.07 17.00 10.60 10.12	#185 < 18 #154 + 04 #146 + 30 #134 + 95
10 11 12 13 14	#13,75 #14,76 0.24 2.25 4.26 4.26 4.27	0.01 0.01 0.01 0.01 0.01 0.01	-8,097 -9,477 -10,283 -0,924 0,167 1,368 1,334 2,380	4.872 5.255 2.685 2.841 2.830 2.863 2.980	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72	6.548 6.545 5.467 5.009 4.394 4.347 3.821	72.94 24.07 17.00 10.60 10.12 5.77	=185×18 =154+04 =146+30 =134+95 =136+88 =130+29
8 9 10 11 12 13 14 15	=13.75 =14.76 0.24 2.25 4.26 4.26 4.27 8.25	0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8,097 -9,477 -10,283 -0,924 0,167 1,368 1,334 2,380 3,240	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062	=181.96 =193.66 =200.08 =93.79 =78.00 =61.62 =61.71 =46.72 =28.66	6.548 6.545 5.467 5.009 4.394 4.347 3.821	72.94 24.07 17.00 10.60 10.12 5.77	=185×18 =154+04 =146+30 =134+95 =136+88 =130+29 =129+30
10 11 12 13 14 15	=13.75 =14.76 0.24 2.25 4.26 4.26 4.27 8.25	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8.097 -9.477 -10.283 -0.924 0.167 1.368 1.334 2.380 3.240 4.255	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062 3.324	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 #8.86	6.546 6.5467 5.009 4.394 4.347 3.720 3.720	72.94 24.07 17.00 10.60 10.12 5.77 0.39	=185 < 18 =154 + 04 =146 + 30 =134 + 95 =136 + 88 =130 + 29 =129 + 30 =131 + 81
10 11 12 13 14 15 16	-13.75 -14.76 0.24 2.25 4.26 -4.26 4.27 8.25 10.26 12.23	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8.097 -9.477 -10.283 -0.924 0.167 1.368 1.334 2.380 3.240 4.255 5.363	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062 3.324 3.618	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 8.63	6.548 6.545 5.467 5.009 4.394 4.347 3.821 3.720 3.994 4.372	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23	=185 x 18 =154 x 04 =146 x 30 =134 x 95 =136 x 88 =130 x 29 =129 x 30 =131 x 81
10 11 12 13 14 15 16 17	-13.75 -14.76 0.24 2.25 -4.26 -4.26 -4.26 -4.27 8.25 10.26 12.23 -14.28	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8.097 -9.477 -10.283 -0.924 0.167 1.368 1.334 2.380 3.240 4.255 5.363 6.476	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.962 3.962 3.962	#181 • 96 #193 • 66 #200 • 08 #93 • 79 #78 • 00 #61 • 62 #61 • 71 #46 • 72 #28 • 66 8 • 63 24 • 63	6.546 6.5467 5.009 4.394 4.347 3.821 3.720 3.974 4.372 4.759	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23 =18.09	=185 × 18 =154 + 04 =146 + 30 =134 + 95 =136 + 88 =129 + 30 =129 + 30 =131 + 81 =135 + 06 =141 + 89
10 11 12 13 14 15 16 17 18	13.75 14.76 0.24 2.25 4.26 4.26 4.27 8.25 10.26 12.23 14.28	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8.097 -9.477 -10.283 -0.924 0.167 1.368 1.334 2.380 3.240 4.255 5.363 6.476 7.631	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062 3.324 3.618 3.969 4.563	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 #8.86 8.63 24.63	6.545 5.467 5.009 4.394 4.347 3.720 3.720 3.720 4.759 4.759	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23 =18.09	#185 x 18 #154 x 04 #146 x 30 #134 x 95 #136 x 88 #130 x 29 #129 x 30 #131 x 81 #135 x 06
10 11 12 13 14 15 16 17 18 19	13.75 14.76 0.24 2.25 4.26 4.26 4.27 8.25 10.26 12.28 16.25 18.24	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8,097 -9,477 -10,283 -0,924 0,167 1,368 1,334 2,380 3,240 4,255 5,363 6,476 7,631 8,708	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062 3.324 3.618 3.969 4.563 5.323	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 #8.86 8.63 24.63 40.60 57.45	6.545 5.467 5.009 4.394 4.347 3.720 3.720 3.720 3.720 4.759 4.759 4.759	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23 =18.09 =22.25	=185×18 =154+04 =146+30 =136+88 =130+29 =129+30 =131+81 =135+06 =141+89 =346+03
10 11 12 13 14 15 16 17 18 19 20	13.75 14.76 0.24 2.25 4.26 4.26 4.26 4.27 8.25 10.26 12.23 14.28 16.25 18.24 20.27	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8,097 -9,483 -0,924 0,167 1,368 1,334 2,380 3,240 4,255 5,363 6,476 7,631 8,708 9,521	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062 3.324 3.563 5.323 5.997	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 8.63 24.63 40.60 57.45 73.96	6.545 5.467 5.009 4.394 4.372 3.720 3.94 4.372 4.3759 4.3759 4.382 3.246	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23 =18.09 =22.25 =25.48 =29.95	#185 x 18 #154 x 04 #146 x 30 #134 x 95 #136 x 88 #130 x 29 #129 x 30 #131 x 81 #135 x 06 #141 x 89 #141 x 89 #138 x 01
10 11 12 13 14 15 16 17 18 19 20 21	13.75 -14.76 0.24 2.25 4.26 4.26 4.26 4.26 10.26 12.23 14.28 16.26 18.24 20.27 22.26	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8.097 -9.477 -10.283 -0.924 -0.168 -1.334 -2.380 -3.240 -4.255 -5.363 -6.476 -7.631 -7.631 -7.631 -7.631 -7.631	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.062 3.324 3.618 3.965 4.563 5.323 5.997 6.690	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 8.63 24.63 24.63 57.45 90.26	6.548 6.545 5.467 5.009 4.394 4.347 3.720 3.5720 3.5720 4.759 4.759 4.759 4.982 3.246 2.986	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23 =18.09 =22.25 =25.48 =29.95	=185×18 =154*04 =146*30 =134*95 =136*88 =130*29 =129*30 =131*81 =141*89 =141*89 =141*89 =138*01 =132*43 =132*43
10 11 12 13 14 15 16 17 18 19 20	13.75 -14.76 0.24 2.25 4.26 4.26 4.26 12.25 10.26 12.23 14.28 16.27 20.27 22.26 24.26	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	-8,097 -9,483 -0,924 0,167 1,368 1,334 2,380 3,240 4,255 5,363 6,476 7,631 8,708 9,521	4.872 5.255 2.685 2.841 2.830 2.863 2.980 3.324 3.618 3.962 4.563 5.997 6.690 7.482	#181.96 #193.66 #200.08 #93.79 #78.00 #61.62 #61.71 #46.72 #28.66 8.63 24.63 40.60 57.45 73.96	6.548 6.545 5.467 5.409 4.394 4.394 3.720 3.7394 4.759 4.759 4.759 2.986 2.986 2.562	72.94 24.07 17.00 10.60 10.12 5.77 0.39 =6.27 =11.23 =18.09 =22.25 =25.48 =29.95 =34.36 =38.38	#185 x 18 #154 x 04 #146 x 30 #134 x 95 #136 x 88 #130 x 29 #129 x 30 #131 x 81 #135 x 06 #141 x 89 #141 x 89 #138 x 01 #132 x 43 #129 x 42

VOUGHT LOW SPEED WIND TUNNEL TEST 630 WIND AXES

RUN 43 11/20/81 0933 RUN 40 TEMP 94. PO 14.6464

QPSF 75.00 VFP8 260.12 RNFT 1484616. MACH 0.2254

TO: TO2 TO3 TO4 TO5 TO6 TO7 TOE TO5 T10

0 0 39 0 19 31 0 0 0 0

T1: T12 T13 T14 T15 T16 T17 T18 T19 T20

0 0 32 32 0 0 1 0 0

CORRECTED FOR TARE AND INTERFERENCE EFFECTS
SINGLE SUPPORT DATA DATA AT C.G. FULL SCALE DATA

PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	RM/Q	YM/Q
1.	0.23	0.01	=9,376	++117	37:18	. 6,002		-157.66
	-1.74	0.01	-13.216	4 + 587	64.56	. 6 . Q42		≈ 161 • 25
- H. B. W. W. B. B. B. B. B. B. S. B. B. S. B. B. S. B.	-3.78	0.01	-17.486	4.933	98 - 08	6.707		=170.56
• 4	=5.77	0.01	421.555	5.726	127 • 16	7, \$36		=182+24
5	'=フェフ 4	0.01	=23.671	6 • 843	133 + 17	. 8:485	54.55	
6	-9.77	0.01	=25.158	7 • 983	126.21	9 < 262		=200.65
7	-11·79	0.07	=27.891	9 • 295	134 • 07	9,496		=202+88
	-13.77	0.01	m30.447	10.584	144+12	3 5 573		≈202•60
	w13.74	0.01	-30.373	10.531	143.21	9.199		≈196.90
10	=14+77	0.01	#32,299	11.339	154+88	8 857	80+38	≒188∗55
1.1	0.23	0.01	=9.643	4.317	35 • 13	6 102	24+09	=161 • 15
12	2.27	0.01	≈5.914	3 • 829	12.41	5+694	16 +66	≈150•18
13	. 4.25	0.01	-2,195	3.684	-12.08	i 5.113	8.57	-142-14
	6.25	0.01	1.259	3.751	=32.91	. 4.784	2 42	=138+94
	. 8.27	0.01	4.519	3.863		4 . 695	-3+09	=141.97
16	10.24	0.01	8.519	4.014	=80+39	4 + 885	-8 .92	=144 . 28
, 17	12.26	0.01	12.400	4.608	=107+17	5,014	=14,69	=145.35
18	.14.27	0.01	15.194		=118 - 84	5.118	=20.27	=148.99
19	16.27	0.01	17.399	6+701		5.090	-26.81	-148+38
-	18.25	0.01	19.812		=125+14	3.542	-28 - 27	-137.34
21	20.25	0.01	21,366		=123.79	: 2:594		≈130 · 80
22	22+21	0.01	22.684			: 2:391	-35.40	
23	24.26	0.01	24.438	12.501		. 2 . 7.44	≈ 37 ≥ 95	
24	25 . 23	0.01	25.573	13.419	-122-15	2.790		=100+36
25		0.01	-9,509	4 - 117		5.921		=157.04

ORIGINAL PACE IS

X-136

=Q×Si4

2:47

4 • 14

=0.31

0.88

=0+14

=0.67

=0.87

		Ye	INGHT FE	W SPEED	WIND TU	NEL TEST	·.630	والمراجعة	
				WIND (A	XES				
**************************************			····			 			;;,,
			0						
eddyndd Gymri 4 - 1 i Madries y fryn 1 ar o'i		RUN 41	<u> </u>		11/20/8	0933	- Application to the state of t	RUN	41
			TEMP	94+			PO 14+6	6464	
	o i je povod dili sprava i se sprav sampa sig sa	QPSF 7	5.00	VFPS 26	0.12	RNFT 148	14616+	MACH 0+2	254
			" T01	T02 T03	TO4 TO5	Y06 T07	T08 T09	T10	
iki kangapan dan menjadi dan dipinasi di	روخ معمد از نظرت می می دادند. و را و او او او این این می این در این او او او او او این این این این این این این	(Q	0 39	0 20	31 0	0 0	O	
			711		T14 T15	T16 T17	718 T19	720	
,			. 0	0 35	:32 0	0 1	0 0	0	
deleta en estado de la estada en estado e	PNT	.ALPHA	PSI	'L/Q	D/Q	AT C.G. PM/Q	. Y/Q	SCALE DA	YM/Q
, 100, 100, 100, 100, 100, 100, 100, 10								, , , , , , , , , , , , , , , , , , , ,	1117 98
	1	0.26	0.01	-0.790	: 2.342		-C.104	-1.09	• =1 • 13
	2	-1.76	0.01	#1,804	2.442	=96+86 =113+38	-C.104	=1:09 =0:01	· =1 · 13 · =3 · 58
<u> </u>	2 3	=1.76 =3.75	0.01	=1,804 =2,902	2.442	#96 •86 #113 • 38 #131 • 80	-0.104 -0.378	=1.09 =0.01 0.64	· =1 • 13 · =3 • 58 · =3 • 77
	· 2 · 3	=1.76 :=3.75 =5.78	0.01	=1,804 =2,902 =3,926	2.442 2.622 2.816	=96.86 =113.38 =131.80 =148.28	-0:104 -0:378 : 0:084 0:775	=1.09 =0.01 0.64 0.82	· =1 · 13 · =3 · 58 · =3 · 77 · =9 · 34
	2 3 4 5	=1.76 :=3.75 =5.78 =7.74	0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 =4,935	2.622 2.622 2.816 3.125	=96.86 =143.38 =131.80 =148.28 =162.13	-0:104 -0:378 : 0:084 0:775 1:019	=1.09 =0.01 0.64 0.82 0.71	* =1 • 13 * =3 • 58 * =3 • 77 • =9 • 34 =12 • 88
	3 4 5 6	-1.76 -3.75 -5.78 -7.74 -9.74	0.01 0.01 0.01 0.01 0.01	#1,804 #2,902 #3,926 #4,935 #6,143	2.442 2.622 2.816 3.125 3.485	#96.86 #113.38 #131.80 #148.28 #162.13 #176.98	-0:104 -0:378 : 0:084 0:775 1:019	-1.09 -0.01 0.64 0.82 0.71 0.17	* #1 * 13 * #3 * 58 * #3 * 77 * #9 * 34 * #10 * 46
	3 4 5 6	=1.76 :=3.75 =5.78 =7.74 =9.74 =11.76	0.01 0.01 0.01 0.01 0.01	#1,804 #2,902 #3,926 #4,935 #6,143 #7,553	2.442 2.622 2.816 3.125 3.485 4.033	=96.86 =113.38 =131.80 =148.28 =162.13 =176.98 =189.96	-0:104 -0:378 : 0:084 0:775 1:019 1:235	-1.09 -0.01 0.64 0.82 0.71 0.17	* =1 • 13 * #3 • 58 * * 3 • 77 * #9 • 34 - 12 • 88 * 10 • 46 * * 4 • 97
	3 4 5 6	=1.76 :=3.75 =5.78 =7.74 =9.74 =11.76 =13.79	0.01 0.01 0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 =4,935 =6,143 =7,553 =9,066	2.442 2.622 2.816 3.125 3.485 4.033	#96.86 #113.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75	-0.104 -0.378 0.084 0.775 1.019 1.235 1.292	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79	* #3.58 * #3.58 * #3.77 * #9.34 * #10.46 * * #4.97 2.60
	2 3 4 5 6 7	=1.76 :=3.75 =5.78 =7.74 =9.74 =11.76	0.01 0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 =4,935 =6,143 =7,553 =9,066 =9,779	2.442 2.622 2.816 3.125 3.485 4.033	#96.86 #143.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75	-0.104 -0.378 0.084 0.775 1.019 1.235 1.292 1.213	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79	* #3.58 * #3.57 * #9.34 * #12.88 * #10.46
	2 3 4 5 6 7 8	=1.76 :=3.75 =5:78 =7:74 =9:74 =11:76 =13:79 =14:75	0.01 0.01 0.01 0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 =4,935 =6,143 =7,553 =9,066	2.442 2.622 2.816 3.125 3.485 4.033 4.605 4.982	#96.86 #143.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09	-0.104 -0.378 0.084 0.775 1.019 1.235 1.292	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96	* #3.58 * #3.58 * #3.77 * #9.34 * #10.46 * #4.97 2.60 5.36
	3 4 5 6 7 8 9	=1.76 :=3.75 =5:78 =7:74 =9:74 =11:76 =13:79 =14:75 Q:27 :2:24 -4:26	0.01 0.01 0.01 0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 *4,935 =6,143 =7,553 =9,779 =0,822 0,175 1,262	2.442 2.622 2.816 3.125 3.485 4.033 4.605 4.982 2.408 2.417 2.470	#96.86 #143.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09	-0.104 -0.378 0.084 0.775 1.019 1.235 1.292 1.219 1.396	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96	**1.13 **3.58 **3.77 **9.34 **10.46 **4.97 2.60 5.36 0.74
	3 4 5 6 7 8 9 10 11 12	-1.76 -3.75 -5.78 -7.74 -9.74 -11.76 -13.79 -14.75 0.27 .2.24 .4.26 6.27	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 =4,935 =6,143 =7,553 =9,779 =0,822 0,175 1,262	2.42 2.622 2.816 3.125 3.485 4.035 4.605 4.982 2.470 2.470 2.598	#96.86 #143.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09 #96.74 #81.63	-0.104 -0.378 -0.084 -0.775 1.019 1.235 1.292 1.219 -0.137 -0.120 -0.261	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96 =1.68 =1.64 =1.88	* #1 * 13 * #3 * 58 * #3 * 77 * #9 * 34 * 12 * 88 * 10 * 46 * * 4 * 97 2 * 60 5 * 36 0 * 74 * 0 * 38 1 * 61 1 * 89
	3 4 5 6 7 8 9 10 11 12 13	-1.76 :=3.75 =5.78 =7.74 =9.74 =11.76 -13.79 =14.75 Q.27 :2.24 -4.26 6.27 .8.27	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	=1,804 =2,902 =3,926 *4,935 =6,143 =7,553 =9,779 =0,825 1,262 1,262 3,274 3,292	2.42 2.62 2.816 3.125 3.485 4.605 4.605 4.988 2.470 2.470 2.598 2.766	#96.86 #113.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09 #96.74 #81.69 #64.32 #48.50 #29.81	-0:104 -0:378 -0:084 -0:775 1:019 1:235 1:235 1:213 1:396 -0:137 -0:120 -0:261	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96 =1.08 =1.64 =1.88	***3.58 **3.57 **9.34 **12.88 **10.46 **4.97 2.60 5.36 0.74 **0.38 1.61 1.89 1.47
	2 3 4 5 6 7 8 9 10 11 12 13 14	-1.76 -3.75 -5.78 -7.74 -9.74 -11.76 -13.79 -14.75 0.27 2.24 -4.26 6.27 8.27 10.26	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	#1,804 #2,902 #4,935 #6,143 #7,553 #9,779 #0,875 #0,162 *2,775 *2,776 *4,154	2.626 2.816 3.125 3.485 4.035 4.6082 2.477 2.4770 2.4770 2.7764	#96.86 #113.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09 #96.74 #81.63 #64.32 #48.50 #29.81	-0:104 -0:378 -0:084 -0:775 1:019 1:235 1:235 1:235 1:236 -0:137 -0:120 -0:261 -0:598 -0:702	-1.09 -0.01 -0.64 -0.82 -0.71 -1.23 -3.79 -4.96 -1.88 -1.66 -1.88	***3.58 **3.58 **3.77 **9.34 **12.88 **10.46 **4.97 2.60 5.36 0.74 **0.38 1.61 1.89 1.47 0.67
	2 3 4 5 6 7 8 9 10 11 12 13 14 15	-1.76 -3.75 -5.78 -7.74 -9.74 -11.76 -13.79 -14.75 0.27 2.24 -4.26 6.27 8.27 10.26 .12.23	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	1,804 2,926 1,926 1,935 1,553 1,	2.42 2.62 2.816 3.125 3.485 4.605 4.605 4.605 4.605 2.470 2.470 2.470 2.470 2.475 2.974 3.255	#96.86 #113.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09 #96.74 #81.63 #64.32 #48.50 #29.81 #10.99 6.39	-0.104 -0.378 -0.084 -0.775 1.019 1.235 1.292 1.219 -0.137 -0.120 -0.261 -0.261 -0.702 -0.641	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96 =1.64 =1.88 =1.66 =1.76 =1.85 =1.91	**1.13 **3.58 **3.77 **9.34 **12.88 **10.46 **4.97 2.60 5.36 0.74 **0.38 1.61 1.89 1.47 0.67 **1.28
	2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	-1.76 -3.75 -5.78 -7.74 -9.74 -11.76 -13.79 -14.75 0.27 .2.24 .4.26 .12.27 .12.23 .14.24	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	1,804 2,926 1,902 1,914 1,	2.42 2.62 2.815 3.185 3.485 4.033 4.605 4.935 4.935 2.470 2.470 2.2770 2.2775 3.775 3.775 3.775	#96 * 86 #143 * 38 #131 * 80 #148 * 28 #162 * 13 #176 * 98 #189 * 96 #201 * 75 #208 * 09 #96 * 74 #81 * 63 #64 * 32 #48 * 50 #29 * 81 #10 * 99 6 * 39 23 * 26	-0.104 -0.378 -0.084 -0.775 1.019 1.235 1.292 1.213 -0.137 -0.120 -0.261 -0.598 -0.598 -0.589 -0.589	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96 =1.64 =1.64 =1.85 =1.85 =1.91 =1.74	**1.13 **3.58 **3.77 **9.34 **12.88 **10.46 **4.97 2.60 5.36 0.74 **0.38 1.61 1.89 1.47 0.67 **1.28 **2.32
	2 3 4 5 6 7 8 9 10 11 12 13 14 15	-1.76 -3.75 -5.78 -7.74 -9.74 -11.76 -13.79 -14.27 -14.26 -12.27 -14.23 -14.27	0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	1,804 2,926 13,926 14,935 16,143 17,553 19,066 19,772 10,167	2.42 2.62 2.816 3.125 3.485 4.605 4.605 4.605 4.605 2.470 2.470 2.470 2.470 2.475 2.974 3.255	#96.86 #113.38 #131.80 #148.28 #162.13 #176.98 #189.96 #201.75 #208.09 #96.74 #81.63 #64.32 #48.50 #29.81 #10.99 6.39	-0.104 -0.378 -0.084 -0.775 1.019 1.235 1.292 1.219 -0.137 -0.120 -0.261 -0.261 -0.702 -0.641	=1.09 =0.01 0.64 0.82 0.71 0.17 =1.23 =3.79 =4.96 =1.64 =1.88 =1.66 =1.85 =1.91 =1.74 =1.38	**1.13 **3.58 **3.77 **9.34 **12.88 **10.46 **4.97 2.60 5.36 0.74 **0.38 1.61 1.89 1.47 0.67 **1.28

5 . 654

6.475

7.272

7 . 641

2+408

9.424

10.432

11.530

12.022

0.01 =0.890

73.53

88.99

104.92

111 + 89

=97.46

-1:514

≈1.+578

-1:237

=1:194

≈0 + 197

0.01

0.01

0.01

0.01

20 20,25

21.

22

23

24

22.26

-24 - 26

25.26

Q • 25

				WIND :	AYES				
				H TIVO	7/10	· · · · · · · · · · · · · · · · · · ·	·		
		RUN 42			11/20/81	0933		RUN	42
			TEMP	76.			PO . 14.0	6120	
		GPSF 7	5.00	VFPS 2	56 • 16	RNFT 15	6449,	MACH 0	2257
	Andria de Algo en la Angre		701	*02 *03	T04 T05	TOC TOS	TOE TOE	710	stoff for the state of the stat
<u>parties de la relación de la relaci</u>		<u></u>	0	0 39	0 20	31 0	0 0	0	
			711		T14 T15	Tie Tit	718 T19	-	
			. 0		32 0	0 1	Ο υ	0	
	SING	LE SUPP	COR BRT DAT	RECTED	FOR TARE		RFERENCI FULL	E EFFECT	S ATA
	PNT	.ALPHA	PSI	L/Q	.D\Ø	PM/Q	'Y/Q	RM/Q	· YM/Q
	1	. 0.24	0.01	+0.524	2.675	-97:01	=0.803	≠ 0,∗53	0.84
	2	1.75	.0.01	-1.570		-113.51	0.029		-2.60
	3	-3.73	0.01	-2.634		-129.49	0.250		· =6 • 19
	- 4	=5 + 75	0.01	=3.690		4146•41	0.613	0 +59	-8 • 47
	5	7-7+74	0.01	=4.802	3+338		0.7.72	0+88	-7×42
	<u>6</u> 7	=9.74 =11.77	0.01	=6.010		=178.16	263.0	0.11	<u>=6.27</u>
		=13.76	0.01	=7.487 =8.862		=191 •32 =203 •97	. 0.880 0.913	=1.24 =2.86	· =2.06 3.68
	, 9	-14.77	0.01	=9.616		-210.39	1.087		5 • 73
	10	0.26	0.01.	=0.323	2.608	=95.80	-0.190	=0.38	· ≡0∗43
	11	. 2 . 25	0 : 01	0.675	2 • 698	=78.68	-0.213	= 0.93	0.97
	12	. 4.27	0.01	1,796	2.717	=63.72	=0.461	-1.29	2 • 88
	.13	. 6.27	0.01	3.008	3 • 145	-47+72	-C.932	-1,59	1.86
	14	8.27	0.01	4.048	3+346	=30 x60	-1.135		
	.15		0.01	5.087	3.721	=13,64	-1:241	=1×73	
	16	.12 + 26	0.01	6.129	4 • 037	3,90	m1:449	=1.82	0 • 67
•	17	14.27	0.01	7 - 144		22 * 02	=1.739	=1.43	2.09
	18	16.26	0.01	8 . 1 67		39.31	*=2.401	≈0.68 ÷ =0.22	<u>#•13</u>
	50	18.27	0.01	9,792	5.525 6.002		-2.672 -3.167	and the second s	
	51	.22.25	0.01	10.931		74+21 89+23	=0 (545	the first of the second second	
- Andrews	22	-24-25	0.01	11.795		104+80	=0 · 897		2.25
	23	25.26	0.01	12,255	7.4854	112+62	=0:761	-0+04	5 • 1 4
	24	0.25	0.01	=0.257		=97 · 17	=0.203		0.08

Co	مستوجع وبخورون والمارون والمارون		/BUGHT L	dw Spee	D WIND TU	NNEL TEST	630	·	
				MIND	AXES				
								,	
and the second s		RUN 4	13		11/20/8	1 0933		RUN	4.3
	•	•	TEM	76.			P8 . 14 .	5120	
	,	GPSF '	75.00	YFPS 7	356 • 16	RNFT 15	6449+	MACH De	2257
		d d	T01	<u>ቸ</u> ወጀ ቸው፤	3 TO4 TO5	T06 T07	TOS TUS	T10	
<u> </u>		i de la capación de 	Ō	о э:	9 0 18	31 0	O : O	Ò	
			711 0		714 T15	T16 T17	T18 T19	T20	
			<u> </u>	о э	32 0			,,,	73
tr.			COF	RECTED	FOR TARE	AND INT	ERFERENC	E EFFECT	3
	SING	ale suf	PERT DAT	T	DATA.	AT C.G.	علما فالمخرجي	SCALE D	ATA
•	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q/	Y/Q	. RM/Q	YMZQ
at the same of the	1	0.2		-0.59		⇒94•59		: 23.31	
	2	=1.78	and the second second	-1.70		=112+28	5.276		=149.27
-(4	=3.76 =5.75		-2.91 -4.30		=128*41 =143.55	6.735		=157.88 =166.87
	. 5	=7 • 7 E		=5.25		=160+37	6,915		≈167.77
•	6	=9∗ 7°		-6. 6≥			6.602		=161.29
	7	-11.74	0.01	-7.96			5 . 757		=148.93
, , , , , , , , , , , , , , , , , , ,	8	-13.7		=9.47		-197.07	4 8 32		=141.73
		=14.7				-202-47	4 + 538		=141.08
	1.0 1.1	2 • 2		=0.55 0.43					143.54 133.98
	12	4 2		1.63					=127 • 5 0
11	13	6.2		2.78			3,335	6 47	≈125 · 93
	14	8 . 2		4.00					=129.77
	15	10.2		5,05	5 4.124	-13.16	. 3.128		=134.27
	16								■138 • 86
e e	17	14.2							#141.08
	18	16.2							=139 • 47 =135 • 18
	19						The second second second		=135·18
5 · · · · · · · · · · · · · · · · · · ·	20 21	20.2							P111.51
	52								#123.28
	23								#113.31
	14	بنكا تا المحاسدة	~ Y*Y*	一一名一年后为	- · !! * I J C				=143.56

-37 *45 ×113 •99

22.89 =140.39

				A waren		** ***	,	
		VBUGHT	Law spfED	WIND TUN	inel test	630		
			WIND					
	RUN			11/20/81	0933		RUN	.44
Managan general personner en inicial construction of the Construct		TE	MP 76.			P0 14.5	973	
	aps	75.00	VFPS 2	en Norsk samme Alleren		5668 ₁	San Haran da	258
And the state of t			0 0 39 1 712 713 0 0 32	0 18 T14 T15	31 0	0 0	0	
	SINGLE	C SUPPORT D	ORRECTED	FOR TARE		RFERENCE FULL		,
	PNT .AL	PHA PSI	L/Q	D/Q	PM/Q	Y/W	RMZ4	YMZQ
	. 2 .−1	1.26 0.0 (.76 0.0	1 =1.673	3.134	=95.76 =113.79 =129.21	5 9 473	29 * 56	⇒141¢93 ⇒147*94 ⇒158*76
	4 m5	0 • 77 0 • 0 7 • 76 0 • 0	1 =4.110 1 =5.359	3.243 3.510	×146∘00 ×159•68 ×171•31	6+808 7+003 6+768	40 ±55 46 •98	=167:53 =169:46 =160:61
	7 =1: 8 =1:	1.76 0.0 3.74 0.0	1 =8.100	4 • 493 5 • 211	#183.27 #195.60 #203.40	. 5,782 - 4,851	50 • 47 52 • 61	=148 + 89 =142 + 24 =141 • 39
	10 (11 . 2	1.24 0.0 2.24 0.0	1 =0.557 1 0.433	3 · 198 3 · 274	=97 + 18 =77 • 58	5 • 0 6 7 4 • 3 6 9 3 • 9 7 4	. 23+89 17+16	=143·47 =132·73 =124·07
	13 (14	6.25 0.0 6.24 0.0	1 2.879 1 3,906	3.553 3.856	=46.8? =32.31	3.307 3.106 3.135	4*66 =0*55	.=125·05
•	16 .1: 17 ·1	2.27 0.0 4.25 0.0	01 6+065 01 7+175	5 4 • 686 5 5 • 141	0 + 7 6 1 7 + 2 6	3 • 278 3 • 183	×11+06 ×16+14	*140.28 *140.58 *136.92
	19 1 20 2	\$ • 27 0 • 0 \$ • 25 0 • 0 0 • 27 0 • 6	1 8.808 1 9.75	6 • 024 6 • 630	50.71 69.18	. 2:569 . 1:859	=24.29 ==26.83	#133+03 #125+48
		2.27 0.0 4.24 0.0					=35+23	=113.04 =123.21

8 + 462

3.186

105.97

=95∙58

2.520

4.932

23 25.28

0.26

0.01

0.01

12.390

=0.622

			WI	ND .	AXES									
	RUN 45				11/2	20/8	ı os	933				RUN	45	***************************************
	•	TEMP	76	• •					FØ	14+	5973			
	gPSF 75∗		T02 0	T03 39 T13	T14		F.4	T07 T17	T08 0	709 0 T19	T10 0	0 • 2:	258	
SING	LE SUPPOR	COR	RECT	BD BD	FØR '						E EFF SCAU			

and with the state of the state	SIN	GLE SUPP	ORT DAT		DATA	T C.G.	FULL	SCALE D	VTA.
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/W	RM/Q	' YM/Q
····	1		0.01	=7.874	4.353	15.63	. 5.179	19.56	=135.62
	2	-1.76	0.01	=11.884	4.787	40.56	5.437	27.40	#140.54
V	3	-3.74	0.01	₩15.416	5.202	65.92	6.168	34+14	=152 • 79
	4	×5.79	0.01	=19.457	5.860	93 • 61	7:019	41.12	=164.68
	5	×7 ± 76	0.01	421.307	6 • 998	99 • 52	7.522	48 • 89	=170.67
	6	=9.81	0.01	≈23.464	8 • 163	97.56	7.703		=172•32
	7	#11 · 77	0.01	-26 454	9 402	110.56	7.1572	58.30	m167.07
	8	-13.78	0.01	=29.283	10.718	124 - 11		63.20	=155.59
	9	-14.75		-30.947	11 . 447	133.61	7.239		≈153·18
	10	0.25	0.01	=7.975	4 4 4 1 8	15+68	5:167	20+33	
	11	2 + 28	0.01	=4.380	4 • 197	= 5⋅81	4.727	13.81	=128.73
	1.5		0.01	=1,195	4.084	=21.74	. 4.347		=125 • 82
	13		0.01	1.960			: 3,817		=124.33
	14		0.01	5.051	4.395		3:461		-127.35
•	15		0.01	8.354			3,433		=133-14
	16		0.01	11.700	5 + 4 4 1	=90.43	3,314		=136:37
,	17		0.01	14.792	6.336	=104+26	3.064		=137*03
•	18		0 * 01	17.130	7 • 533		2.723		=135+82
	19		0.01	19.312	8 • 701		: 2.369		=130.77
	20		0.01	21.368		=125.09	1.558		-121 -52
	21	22.25	0.01	22.888		-123.50	0,931		=107 • 29
	22		0.01	24.673		=123+93	3.250		=111.73
	23		0.01	25.573		=124+84	2.987	=38 * 62	
	24		0.01	=7.942	4.285		5.108		*134.65

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A-141

	74.	,			****	•	-
					2 12 14	1949	
	YOUGHT L	MW SPEED	WIND TUN	NEL TEST	630		
		WIND A	XES				
	UN 46		11/20/81	0933		RUN	.46
•	TEM	· · · · · · · · · · · · · · · · · · ·			PØ. 14.5	973	
] be; [*]	F / 💵					
C I	PSF 75.00	VFPS 25	6,29	RNFT 154	5668	MACH 0 +2	258
	701	T02 T03	T04 T05	TO6 TO7	708 TUS	71 0	
The second secon	Q		0 19	31 0	0 0	0	
	T11	T12 T13					
	0	0 32	35 0	0 1	0 0	<u> </u>	
			46 7100	KIN WITE	apport of		
GTNAL	 E SUPPORT DA	RRECTED F		AND INTE	KFERENCE	SCALE DA	ት ፡
SENG!	E OUFFURI DA	I A	· PALA: A		F M La La		7.1.6
. PNT	ALPHA PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	. AW\d
	0.24 0.01	-9.042	4.551	32.37	: 5,508	: 21.81	-141-15
		412.88 3	4.837	59+05	5,509	. 28.70	-146.89
300	-3.79 0.01	-17.453	5.500	95+94	. 6.401		=159 - 42
		=21,254	6.126	123:11	7. • 234		=169.96
		. #23.796	7.0276	132•16	7:692		4177 - 29
	=9.71 0.01		8.463	122.05	8 • 096		=179.49
the state of the s		. =27 *699	9.728	129.68	7,503		-172 •02
		. =30,350	10.984	139 85	7,975		=168 +06
		. #32.042	11.653	147.79	7.880		=163.74
10	0.24 0.01	. —	4 • 651	33.21	5+468		=140+90
11 .	2.26 0.01		4.329	10.50	5 + 294		=135.08
	4 • 23 0 • 01		4.316	=13.46	4.194		=131 · 16 =134 · 36
13	6.28 0.01			±33.98	4.131	and a second of	
	8.25 0.01			≈55 • 10	3,581		#140*23 #144*99
	10.24 0.01 12.26 0.01		5 • 081	=80.89 =108.95	3.847		=145 • 85
4 **	14.24 0.01			=100·35 =123·35	3:537		=145 • 77
	16.25 0.01			=128 • 18	3.023		=141.53
	18.26 0.01			=132.22	2.569		=134 + 41
	20.26 0.01			=132 * 21	1.759		m124.94
	22.25 0.01			-123.03	0.298		=104.93
	22.24 0.01			=124+24	4.033		=131·02
	24.23 0.01		13.307		3 485		=113.89
	25.25 0.01			=123.00	3 . 237	=40 -23	=102.43
25	0.25 0.0		4.618	32.05	5.501		=140.28

ORIGINAL PAGE IS OF POOR QUALITY

A-1.42

C ***		OF POOR QUAL	MY A-:	142
Company of the Assessment of t	Venght L	HW SPEED WIND TU	NNEL TEST 630	
		WIND AXES		•
100	RUN #7	11/20/8	1 0933	: RUN 47
	TEN	1P 76 •	PO 14.	5973
eronezak) interesta para para la para para la para para la para La para la para	QPSF 75.00	VFPS 254.29	RNET 1545668.	MACH 0:2258
	Tii	0 92 0 11 T12 T13 T14 T15	31 0 0 0 T16 T17 T18 T19 0 1 0 0	0
	CC SINGLE SUPPORT DA	PRECTED FOR TARE		E EFFECTS SCALE DATA
	PNT .ALPHA PSI	L/Q D/Q	PM/Q Y/Q	RM/Q YM/Q
		2 =8.610 5.863 2 =13.476 6.312 2 =18.738 6.670	46+85 : 2+481	28.88 =135.00 33.48 =128.07
	4 =5.74 0.02 5 =7.78 0.02	=22.836 7.274 =26.669 8.535 =30.045 10.302	102.79 3.625 107.57 5.981	42+07 =139+10 48+30 =149+96
	7 =11.76 0.02	2 =33.972 .12.599 2 =36.004 15.480	106.81 4.578	

				H					* * * * * * * * * * * * * * * * * * * *	• • • • • • • • • • • • • • • • • • • •
No. of the Control of	1	0.23	0.02	=8.610	5.863	22.82	- 5	3,999	82.50	=139+99
	2	-1.76	0.02	-13.476	6.312	46+85	X.	2 . 481	8%489	=135.00
	3	3.75		-18.738	6.670	79.03		2.108	84.66	=128.07
	4	=5.74		#22.836	7.272	102.79	V-1	3 . 625	42.07	=139 • 10
\	5	-7.78	0.02	=26.669	8.535	107 + 57		5.081	48.30	-149+96
	6	=9.76	0.02	≈30.045	10.302			4 . 558		=147.12
	7	-11.76			.12.599	106.81		4,578		=149 · Q5
	8	-13.78	0.02	#36.004	15.480	114+94		4:268		=146+64
and the second second second second	9	=14.75	0.05	37.336	16.831	124.00	•	4.501	64.66	=148.56
	10	0.27	0.02	=8.508	5.985	22 • 62		4.034	21.76	=140:03
	11	2 • 25	0.02	=3.301	6 • 1,60	5.75		4.888	14.99	=141+97
	12		0.02	0.953	6.534	=7.61		5.340	7+26	=142.99
	43	6.23	0.02	4.690	7 • 254	-22.31	*:	4.619	0.98	≒139•51
	14	8 + 27	0.02	8 647	8 + 026	-35 97	a	4+025	-4-17	=137.09
	15	10.25	0.02	12.450	9 - 411	-43.32		3 6 5 9 9	-8.99	≈135×16
,	16	12:26	0.02	15.639	10.229	≒55 88		3:26%	=11.099	■134•44
•	17	14.26	0:02	18.673	11.809	=68+36		2.539	≈15 • 10	=131.59
	18	15.24	0.02	21.789	13.536	≈ 77 • 59		2.270	=19.42	=125.92
	19	18+24	0.02	25.199	15.533	-87 .89		1.967	-24.77	-122.98
	20	20.26	0 • 02	29.242	17.883	-95.58	fr	2:084	m30 c年生	=124 · 85
emining of the second of the second	21	.22.27	0.02	34.089	21.020			5 104	-42.26	=138.69
	22	24.23	0.02	40.881	24.660	=127.75		6 : 474	×53 +38	=144+35
	23	25 • 22	0.02	44,591	26.580	=139+55	•	7.102	M56+64	-146.80
	24	0.27	0.02	×8.475	5.965	23 • 64		3.967	21 +56	=141 · 77
		· · · · · · · · · · · · · · · · · · ·						£		the first of the last of the l

	٧٥	UGHT Le	W SPEED	WIND TUN	INEL TEST	630		
			WIND .	AXES				
	RUN 48			11/20/81	0933		: RUN	48
		TEMF	76,			PØ. 14•5	5973	
	GPSF 7	5.00	VFPS 2	56+29	RNFT 154	5668:	MACH O	2258
		TQ1		T04 T05		TOS TOS	T10	
		711 0	0 48 T12 T13 0 32	0 12 T14 T15 32 0	31 0 T16 T17 0 1	0 0 718 T15 0 0	0 T20 1	
sin	GLE SUPP			FOR TARE	AND INTE		EFFECT: SCALE D	
PNT	ALPHA	PSI	L/Q	פעם	PM/Q	.Υ\ō	RM/Q	YMZQ
1	0.27 0.27 0.27	0.01 =2.02 =3.98	=8.751 =9.135 =9.493	9.515	38 • 84 40 • 02 44 • 21	2.409	20-16	=143.05 =141.70 =137.32
(4 5 6	Q+27 Q+27 Q+27	=6:01 =8:00 =10:02	=10:006 =9:561 =8:766	9 • 754 10 • 168	47+60 43+99		22 • 45	
, , , , , , , , , , , , , , , , , , ,	0.27	=12.00 =14.00 =16.01		11.978	26 • 67 18 • 79	*15.343 *19.973		
10 11 12	0.26	=18.00 =20.02 =22.00	=2.459 =0.305 1.127	16.585 18.884 21.551	=2 • 58 =12 • 72	#29:075 #33:629 #38:677	11+89 9+38 7+69	30 • 81 62 • 18 80 • 32
13 . 14 15	0.25	=24.00 =26.00 =28.01	3.039 3.986 4.420	24.454 27.301	≠29 • 25 =28 • 68	#43 • 548 #47 • 853 #51 • 555	7+18 8+04	105.03
. 16 17 18	Q • 25 Q • 25	=30.01 =0.01 2.01	3.423 =8.284	33.947 9.527	=1.42 36.40	≠55±360 5•018	24 • 18 18 • 91	147 • 68 =143 • 33
19 20	0.25	4.02 8.02	=7.848 =7.479 =6.515	11.340	35·21 31·83 21·70	6+787 9:154 -15:580	15+40 20+43	=127+70 =124+85 =154+20
21 22 23	0 + 25 0 + 25	12.00 14.01	=5.824 =5.011 =3.748	13.232 .14.660	12•79 3•80 =5•68	19:050 23:228 27:876	24+80 25±50	=169.76 =193.31 =217.23
24 25 26	0.25	16.01 18.00 20.01	=2:343 =0:337 1:627	16:327 18:429 20:758	=16 · 81 =28 · 05 =37 · 75	32.827 37.202 43.306	28.25	=244+69 =276+70 =290+37

27

29

30

31

32

0.25 22.00

24001

26.01

28.00

30+00

-0.01

0.25

0.25

0.25

0.25

0.25

2.659

4.750

5.784

5 * 653

3.425

-8.218

23:285

26.313

29.524

32.798

35 + 856

9 . 527

=41.99 47.771

52:786

57:252

61:242

63.325

=48.56

=45 €63

<u> =33.13</u>

-8.72

37+24

20.66 =286.22

20.30 =314.86

16 462 4337 + 70

#6+18 Ø367+72

4.738 . 20.37 -144.08

9.07 =361:18

VOUGHT LOW SPEED WIND TUNNEL TEST 630

CENTER THE PROPERTY OF THE PRO	· · · · · · · · · · · · · · · · · · ·	V S	UGHT L	W SPEED	WIND TUN	INEL TES	F 630		
				WIND	AXES				
And the state of t			, , , , , , , , , , , , , , , , , , , 	**************************************					a <u>Parisanian di sana dan aratan di sana dan aratan di</u> sana dan aratan di sana dan aratan di sana dan aratan dan aratan di sana dan aratan dan
means of Community (2) (1)	:	RUN 49	···		11/20/81	0933		, RUN	49
			TEM	9 55.			PØ 14+6	5562	
		QPSF 7	5.00	VFPS 2	50.71	RNFT 16	29067+	MACH O .	2254
	, W		Tör	T02 T03	T04 T05	TOS TO7	TOS TOS	Tio	
Che Santania and Anna		land of the control of the con-	0	0 39	0 18	31 0	0 0	0	in the second
			T11		T14 T15	T16 T17	718 T19		
ATTACA CONTRACTOR CONT		;	0		.32 O	0 1	0 0	0	
	SIN	GLE SUPP	CO ORT DA	RREGTED	FOR TARE	AND INTI	ERFERENCE FULL	E EFFECTS	3
	PNT	.ALPHA	PSI	۲\ō	D/Q	PM/Q	YZQ	RM/Q	YM/Q
				-r -	<i>5</i> , 4	1 117 04	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	11117	s are se
	1	0.26	0.01	=0.589	2.919	=97.37	5 • 652	24.96	#163949
*	. 2	一定主了在一	0.01	-1.571	2.934		6.130	31 + 93	-170 • 59
and I manage the second	3	=3.75	0.01	=2.645		=132.76			=176.75
* .	4	≠5.76	0.01	≈3.776		=147.80	7 • 523		=189 • 25
	5	=7.76	0.01	=5.125		=160.82	8 • 257		=199+96
	6	= 9∗35	0.01	=6.435		=173.43	8.373		=199 • 06
		=11.77	0.01	-7.901		=183.37		66 • 66	
•	8	-13.77	0.01	=9.346		*195.08	7 • 191		=191 .82
CONTRACTOR OF THE PROPERTY OF	9	-14.73	0.01		5.518				=188+14
	10	0.25	0.01	=0.556		≈96 • 26	5,633		=162+40
	11	. 2.26	0.01	0.568		=80 • 81	5 . 128		4152 68
	12	4 • 25	0.01	1.767		=66∙20	4 • 607		=141 • 17
	13	6.26	0.01	2.679		H49,84			=139.31
	14	8 • 25	0.01	3.673		-32.28	3.540	0.31	=137.68
emploration that the control of the	15	10.26	0.01	4.588		m14+34	+ 4 • 161		=139.85
	16	12.26	0.01	5,631		3.68	4 * 4 6 3		=147 + 17
•	17	14.24	0 • 01	6.808		19 # 82	4 * 8 4 1		=150+33
	18	16.27	0.01	8.065		35.18	4.935		=153:79
	19	18.27	0.01	9.376		51.41	3 4 4 0 8		=146.18
	20	20.28	0.01	10.355		67.53	3.371		-142.81
n de la companya de l	21	.22 • 26	0.01	11.445		83.21	3.266		=137.92
	'2''	C3 21 C3 57	17 . D.4	40 101	~ ~ ~ ~	ستندر ويور	- E		

.24 . 27

25.27

0.25

23

24

0.01

0.01

0:01

12.434

13.022

=0.556

7.916

8 + 394

2 * 918

96.58

104 * 42

=97 . 94

2.510

1.880

5 • 553

#34 • 55 **=**125 • 42

=36+99 =116+23

24 * 85 = 162 * 92

ORIGINIAL PLACE IS OF POOR QUALITY

A-145

			_			ŧ	AA MAA	•	
	· · · · · · · · · · · · · · · · · · ·		in akan kan kan kan ja ja ja La	•	**************************************	Paragraphing marks	िंग के प्रश्निक के स्थाप के स्थाप कर कर के प्रश्निक के प्रश्निक के स्थाप के प्रश्निक के प्रश्निक के प्रश्निक क 	k gefälltigis i errykthise vargestätigere	The state of the s
	<u> مشخوره در می جانب </u>	V.	UGHT LE	w SPEED	WIND TUN	INEL TES	630	ن ماندان الماندان ال	
				WIND /	AXES				
							· · · · · · · · · · · · · · · · · · ·		
	10 (4.1 a) 134	RUN 50	نها الأراب أي الأربي بعارل		11/20/81	1 0933		. RUN	50
te, anamerica (meri i de propoles pireliga) di il dan artan ia							44 - 1 30 - 144 - 144 - 144 - 144 - 144 - 144 - 1		
			TEMP	61.			PO 14.6	759	
The state of the s		GPSF 7	5.00	VFPS 2	52.00	RNFT 16	04504.	MACH De	2252
							المسيد شها السائد المسادد		
the same to the same of the sa			101	702 T03	704 T05 0 18		TOS TUS	710 0	in the second of
			-				718 T19	ਜ	
			0	0 35	32 0	0 1	0 0	, _0	
					FOR TARE	AND INT	ERFERENCE	EFFECT	S ilan (September
Ng tangan makatika di Pangan Manada adalah sa dari	SIN	GLE SUPP	BRT DAY	A	DATA	AT C.G.	FULL	SCALE D	ATA
	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	RM/Q	· YM/Q
	1	(:0.25	0.01	= 0.656	. 2.852	=100.69	5.800	24.88	=166+11
1 (1) 1 (1) 1 (1) (1) (1) (1)	Ž	3.1	0.01	-1.672	4.4	=117.29			-176.71
	3	2 2/12	0.01		2 • 895				≒188•09
	4		0.01	=4:108		=146 + 14	8 + 262		#203.64
`	5	°=7∗75	0.01	45:391		=157+24	8 • 855	58,30	-212-16
	6		0.01	≖6,788		=169.58	8 • 967		≈212.97
w()	7	-11.76	0.01	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-181.01			=209.17
v [*]		=13.73	0.01	=9,708		=191 + 89			=199.03
· Production of the latest and experience of the latest and the la	9		0.01	-10.383		-197-26	. 6.945		=194.61
	10 11		0:01 0:01	=0.555	2.819	=99.09			=166+43 =157:57
	12		0.01	0.435 1.534	2 • 875 2 • 963		5•341 4•814		=148 * 26
Andready of the second	A		0001	2,614			· 4:255		=142.42
	14		9.01	3,607					#141 · 61
	15		10.0	4.521					=142.94
-	16		0.01	5,498	3,785	0.29	Marie Division of the Control of the		=147 + 25
,	17		0.01	6.808	4 * 1 4 1	16 * 18	40889	=17.78	=153+00
19	18		0.01	8.030		31.13	mentioned to be a constitution of the		9160.52
	19		0.01						0856 035
	20		0.01	10.423		62 • 49			=155 098
Marine William Committee C	21		0.01	11.410			3 825		*149+34
	22		0.01	12,502					=138*24 =129*33
	24		0.01	12.985 =0.624		96 ± 84 = 101 • 49			=166+84
	<u></u>	<u> </u>			<u> </u>	<u> </u>	<u> </u>	LTFLO	-10010#

				ORIGINAL OF POOR	PAGE IS		Д.—.	L46	
		γı	SUGHT L	SPEED	WIND TU	NNEL TES!	630	econol 20 - 1400/2004 pares - symmethy programme	
				WIND	AXES				
		N. Sala						-V	
		RUN 5	(11/20/3	1 0933	m of many	RUN	51
			TEM	64.			PO 14+6	808	
		GPSF I	3.00	VFPS 2	65 • 81	RNFT 16	78079:	MACH O.	2369
			701	TO2 TO3	T04 T05	TOS TOT	TOR TOS	T10	
and the transfer of the first harring of the second state of first	<u> </u>	<u> </u>	0	0 51		31 0	0 0	0	
			T11		T14 T15		77 75		
			ď		32 0	0 1	0 0	1	
	· · · · · · · · · · · · · · · · · · ·		PORT DA	*		AT C.G.	.FULL	SCALE D	ATA
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	RM/Q	· YM/Q
	1	0+26	0.00	-0,151	. 2.620	=102.42	. 5.273	23.89	-159.52
	2	0.26		-0.100		-104+39			=149.36
	3		-4.00			-106.08			=140.74
×.	4	0.26	= 5.99	0.167		=107.25	≈2 • 8 4 8		=150 • 11
	5	0.27	≈8 ∗00	0.618		=114,16	=6.326		4132.06
	6	0.27	=9.99	1.059		=118+11			=109 • 13
	7		-12.00			=113+34			-95.87
18. July 18.	8		=14.01	0.686		-102+32			
ne to me distribute de la company de la c	9 10		<u>*15.99</u>	0.046		<u>=89.14</u>			. -59 • 88
	11		=17.99 =19.99	=0.083					
	12		×21 +99	≈0.280			≈27 €07	=10.80 =7.80	=17.54 =1.83
	13		-23.99	=0.432 =0.548		<u>≠51⋅87</u>	≈35: 066	-4+29	
	14		.=25.99	=0.5TA		=25.70		=0.39	
	15		-28.07	=0.644		=9.61		4.00	
and the standard of the standa	16		=30.03	=0.737			#45 671	10+44	
•	17	0.27	=0.01	=Q.242		=103.46	5 • 365		=159+96
•	18	0 + 27	2.01	-0.180		±104+86	7.610		=161.36
	19	0.27		0.024		*107 · 77			=161+99
	20	0.27	The Art of the Control of the Contro	0.157		-112+24			-148.91
en de la companya de La companya de la co	21	0.27		0.550		×118+55			=150.30
<u>, and the Mary and the second and t</u>	22	0.27	9,99	1.015		-126:58	17.0348		=158+65
	22	0.00		4 44 4		عديد يعونهمون		24.24	

5.729 -129.93

7.479 =125.20

8 931 #113 24

2.650 -103.33

≈97*58

m82.82

=64.50

=43.36

38 · +5m

22:04

39,28

10.528

12.412

14.668

16.920

19.602

22.788

25.974

20:720

24 . 873

28,532

32.669

36.667

41:117

44 + 823

49.504

49 * 110

53:323

5.303

61.63 ×185.08

66+16 =195+20

66.71 -207.68

65.73 =224.40

65.93 -249.78

65.52 =280.61

62.63 =303.91

52.83 =320.54

9,08 -229,44

1.61 -249.73

24.23 =161.18

23

24

25

26

27

28

29

30

31.

37

30

Q + 28

0.28

0 + 28

0.25

0 . 75

11.98

14+00

15.99

21.99

26.00

0.20 0.00 -0.272

0.29 18.00

10.01 45.0

0.25.23.98

5088 28+00

0.48. 29.99

1.368

1.483

1.081

0.577

0 1 41

₩Q.286

-0.976

m1 -145

-2+527

*2 534

7:012

5.391

86060

4.009 -114.37

=60.41 =151.03

21.93 -158.88

VOUGHT LAW SPEED WIND TUNNEL TEST 630

			WIND A	XES				
	RUN 52			11/20/81	0933		RUN	.52
		TEMP	66.			P0 14 s	808 "	
	QPSF 75	5.00	VFPS 25	53.16	RNFT 15	37495.	MACH OF	252
		و ماکد د				والمستقدية		
				T04 T05				
		0	0 32	0 17	31 0	0 . 0	0	
		T1#		T14 T15				
**************************************		<u>U</u>	0 35	35 U	01	<u> </u>	<u> </u>	
		COR	RECTED F	FOR TARE	AND INT	ERFERENCI	EFFECT	
SIN	GLE SUPP	TRT DAT	*Δ	DATA A	T C.G.	FULL	SCALE D	ATA
ראק	ALPHA	PSI	٢١٥	D/Q	PM/Q	PYY.	RM/Q	YM/Q
	0.28	0.02	6,816	3.976	-113.49	5,571	21+74	=161+29
		0.02	2.867		=134 :00	5 . 825	. 28 - 10	=166+54
		0.02	⇒0.738		=153.14	6 • 146	34.55	=171.17
0 (0.02	=4.533		=170+04	6.329	42+15	=174.97
		0.02	=8.562		=184+24	6.930	49+90	#181+34
	=9.77	0.02	=12.974		=196.01	7.560		≈189.96
	-11.75	0.02	=18.496	6.020	-204+18	7,462	63.67	=188.28
	-13.77		-23.711		-213.71	6.7.92		-179.05
	=14.74	0.02	-25.962	7.830	-216.83			=174 • 13
10	0.24	0 €02	6.781	4:009	=113+34			≈161•17
11	2 • 25	0.02	10° 25	4.324	=93.50	5•437		-156.96
12	2 4 27	0.02	13.513	4.578	=73.08	5 • 121		=148.52
	6 • 26	0.02	16.640	5.083	-54+77	. 4,554		=140.83
		0.02	19.831	5.792	-34.81	. 4 806		=139.30
1.		0.02	23.752		=12.53			=136+34
. 10		0.02	27.624	7.914	7 • 83			=133.08
. 17		0.02	30.650	9 • 609	27+68			-129 • 15
18		0.02	31.933	11.190	42.66	6 • 8 6 8		≖ 126.99
1:		0.02	28.941	13.859	52+16			■139 • 82
2 ()		0.02	30.245		63.26		. * . *	-144.90
2:		0.05	32.262		75.16			=151+73
22		0.02	34,550	19.969	84 + 05			-154 • 27
~	· ~ ~ /	~ ~~	~~ ~~ ~	~ 4 4 ~ ~		7 640	-60-111	- A - A - A - A - A - A - A - A - A - A

0.02 35.918 21.195

0.02 6.615

23 25.26

0.25

ORIGINAL PAGE IS OF POOR QUALITY

A-148

						era seria		
	Ves	GHT LA	w SPPED	WIND TUN	INFL TFS	F:630	Tiganitis of Yellings on the Company and	***************************************
			WIND A	and the second second	<u> </u>		(1	
				 	 			
	RUN 53			11/20/81	0933		RUN	53
		TEMP	68.		*	PO. 14+6	857	
	opsf 75	•00	VFPS 25	53,60	RNFT 15	80156+	MACH O+	2251
		T01	EOT SOT	T04 T05	T06 T07	EUT BOT	T10	
		O	0 32	0 17	31 0	0 0	Ö	11
		T11	712 713 0 32	T14 T15	T16 T17	718 T19	T20	
SIN PNT	GLE SUPPE	COR RT DAT PSI	RECTED :F		AND INTI T C.G. PM/Q	ERFERENCE FULL: Y/Q	EFFECT: SCALE D RM/Q	S ATA Ym/Q
	요 시간 이번 이번 그리고 있다.	0.02	6,881		*109.39		. 22•15	#159.73
. ,	=1 • 75 =3 • 74	0.02	2.934 =0.737		=130.44 =153.96	5,591		=161 • 68 =162 • 77
4	=5.74	0.02	=4.366	4 • 255				=165.83
5	=7.75	0.02	=8.394		=185.30			=172.71
6	-9.82		=12.879		=196.71	7. 369		=181 • 63
	-11.77		m18.267		-204.95			≓179+88
	-13.76	0.02	=23.408		=214.84	6.811		=175.16
9 10	-14.76 Q.25		₩25.970		-218.45			=168+10
11	2 • 25	0.02	6.715	4 • 142		5 538		=159 • 21
12	4.26	0.02	10.158 13.411	4 • 378 • 4 • 704	=89.69 =69.96	5.337		=154 • 52 =145 • 81
13		0.02	16,605	5.149				w138•19
	8.25	0.02	50,005	5 827				=134+49
	10.25	0.02	23.681	6.706		5.093		=133 - 27
16	.12 • 24	0 .02	27.646	7 • 978	12:11	5,375	=16 +23	≈131 • 1 4
17	14.24	0.02	30.436	9 • 409	30.43	5,919		=131•79
18	16.26	20.02	31.916	11.352	48.62	6 • 7 0 9		=126•30
19	18.25	0.02	29.140	13,878	56+47	. 4.573	-31.99	=136.54

30.671 15.929

117.769

19:829

21.026

32.065

340443

35.527

6.748

70.14 4.590

81.65 - 4.906

5,802

6.564

5:391

91.32

93.12

4 • 082 = 109 • 33

-34+05 -140-28

=39.22 =144.85

=48 :92 =147 · 12

=55.58 =143.67

22 - 27 4159 - 71

20.24

22.27

24.27

23.23

0.25

22

23

0.02

0.02

0.02

0.02

0.02

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0.02

0.02

8.500

13.486

17.755

22.305

26.353

29 - 179

31.973

34+108

38.430

42.415

46.554

49.839

=1.331

5 • 114

5,387

6.015

5.939

8 . 125

9 • 608

11:438

14 . 817

17.526

20.385

4 . 873

23 + 504 = 106 + 78

25 + 648 = 119 + 94

6 . 28

. 4 + 25

8.26

10.25

.12 . 25

.14.27

16 . 28

18.27

20.25

22.26

24.26

25 . 28

0.27

13

14

15

16

17

18

19

21

22

23

24

20

-0:72

-1.08

-2.00

-3.56

=4+64

-6 •30

-8.90

=4+67

m2.67

-0.55

≈3,59

-5.65

-0.99

-3.55

-2.55

-1.26

1.53

6.36

2.40

=0.08

=3.36

-5.53

-3.67

2.39

-0.836

-0.837

-0.595

=Q.202

0.080

0.577

1 . 661

-0.438

-0.868

=0,651

. 1 . 186

0,396

= 1 * 08

=2:41

10.23

31 + 18

57.02

52 . 23

-13.99

-49.37

-77+65

13.38

physical Activity of the second of the secon	·	and the second s	····		·····				·
, i	•	yeu	GHT La	W SPEED	WIND TUN	NEL TEST	630	,	<u> </u>
				MIND A	XES				
		RUN 54			11/20/81	0933		: RUN	54
			TEMÉ	68+			PO 14.6	857	
		GPSF 75	1.00	VFPS 25	53,60	RNFT 158	0156.	MACH 0.2	251
			701	*02 T03	T04 T05	T06 T07	TOS TOS	T10	
Marian Ma	التعزيب والأرادة المتاريخ	and the second second second second second	0	0 Э2	0 15 T14 T15	31 0	Ο υ	0	•
	SING	LE SUPPO	COR DRT .DAT	NECTED F	OR TARE	AND INTE	RFERENCE FULL	EFFECTS SCALE DA	TA
	PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	RM/Q	· YM/Q
	1 2 3	0.25 -1.74 -3.77		=1.098 =7.233 =13.751	4 • 839 5 • 059	11.96 28.06 49.09	=0,969 =1,162 =1,028	=1.01 =0.90 =0.44	1.40 2.91 1.86
	4 5	=5.76 =7.75	0.02	=19.578 =24.588	6 • 286 7 • 601	68+96 72+39	=1 • 105 .=0 • 894	=0+75 =0+02	4 * 55 1 • 36
	6 7 8	=9.76 =11.77 =13.77	0.02	=29.707 +36.471 =43.026	8 · 9 6 3 10 · 3 5 4 12 · 28 1	72 • 35 84 • 54 95 • 33	=0.521 =0.771 =1.281	2+04 1+02 2+77	=0.40 =0.09 =1.99
		-14.76 0.28 2.26		=45.842 =1.297 4.043	.13.332 .4.940 .4.967	98.56 12.03 4.26	=1.519 =0.540 =0.858	A SECTION AND ADDRESS OF THE PARTY OF THE PA	1.74 -0.38
		. H.4 E.3	4 1.4	TRUTE	7 4 2 4 7	7760	-01000	-0.270	-4.40

VOUGHT LAW SPEED WIND TUNNEL TEST 630

			WI	ND.	AXES								
	RUN 55				11/2	20/8	ı o	933		1. 3.	. F	UN 5	55
•		TEMP	70	•					PO.	14+6	857		
	QPSF 75	•00 TO1	y de	 1 m 1.7 	54+08 T04	i garan Tabuh		T 157	- 14 g	Tos	MACH Tio	0 .225	11
		0 T11 0	0 †12 0	32 T13 32		15 T15 0	31 716 0	0 T17 1	0 718 0	o T1ğ Ç	0		
SING	LE SUPPO	COR RT DAY	RECT	ΈD	FOR 1	TARE	AND AT C	INT:			E EFFE SCALE		
PNT	.ALPHA	PSI,	L	./@	ſ	D/Q	P	M/Q	,	1/19	RM/	'Q	YM/Q
	0 • 27	0.02	-1.	531	8	639	2	0.79	=0	634	=0	-23	0+64

PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	YMZQ
	0.27	0.02	-1.531	8 • 639	20.79	-0:634	=0+23	0+64
2	-1-74	0.02	⇒7.900	8 • 785	35.04	-0.669	· =0.36	1.51
	-3.78	0.02	=14.118	9 • 180	52.30	-0.736	-0.39	1.93
4	=5 • 78	0.02	-20.018	9 • 7.52	68 • 59	-0:939	=0.66	5.07
5	≍ 7∙79	0.02	=25.351	10 + 847	73.80	=0 •863	0.99	4 • 28
6	=9 = 75	0 .02	±30.006	12 • 196	71:37	=0.554	2 • 19	1 • 1 1
7.	-11.78	0.05	-37.266	.13.713	79.07	-0.864	1.16	· -0·17
	-13.75	0.02	#42,266	15.082	78 - 42	-1,295	1.91	- =0.46
	-14.77	0.02	-45.359	16 - 245		=1.518	2.76	=1.50
10	0.25	0.02	=1.665	8 • 605	20.49	=0:635	-1.20	0+29
11	2:27	0.02	3.777	8+701	14+11	□0 • 524	=0.00	: =1 +94
. 12	4 . 28	0.02	8.737	8 * 882	9.94	=0+469	0 • 47	#4 • O1
13	6.24	0.02	13.215	9 • 184	10.01	=0.405	0,38	-4.36
14	8.26	0.02		9.782	14.08	=0.028	-0.74	=5.40
	10.24	0 . 02		10.638		0.364	=2.93	=5. 02
16	12.25	0.02	26.420	11.758	43,92	0.420	=3.50	=2+64
. 17	.14 . 24	0.02	29.721	13.051	71 • 43	0.530	-4.11	1.20
18	16 . 28	0.02	32.293	14.691	72 • 63	1:161	=6 +56	7 * 03
19	18.26	0.02	34.380	18 • 123	+3,40		-2+85	0.27
20	20.24	0.02	38.243	20.531	-30.05	=0.069	-1.75	-0.92
21	.22 . 25	0.02	42.476	23.417	≈56·89	-0.186	0+24	• =5 • 85
22	-24 - 25	0.02	46.402	26.535	=85,28	0.421	=1+46	=7×56
23	25 . 25	0.02	48,653	28.309	=101.01	1:480	=3.39	=6.51
24	Q+24	0.02	=1.532	8.605	20.72	=0.643	=0.23	0.92

-1.78

=1.49

1.80

-10.80

.=12.53

=10+16

#5+35 · **=9**+92

0.490

1:022

1:847

0.011

				MIND	AXES				
	-	RUN 56			11/20/8	1 0933		. RUN	,56
			TEMP	70•			PØ 14.6	857	
		GPSF 7	5.00	VFPS	254:08	RNFT 15	72614.	MACH O 42	2251
			₩	-AA	A -A -A		**************	*AA	y was a
			101	0 3	3 TO4 TO5		0 0	0	<u> </u>
			· T14		3 T14 T15		- +	7	
			1 + 1	0 3			0 0	0	
F	тич	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
	1	0.26	0.02	=2.87	4 8.673	41.65		1.28	* -9:10
	. 2	-1.76	0.02				-0:049		1 =6:04
	3,			=15.76					· =5·81
منسنداد مناسدة فيسيد ويستنداد مناسيد ويوا	Jı.	≈ 5 • 79	0.02	=21.94	E 0.0E4	0/ /0		3 ,58	=2 ,56
1	. 4						=0:292		
	5	=7.76	0.02	=27.47	8 10.806	107+34	= 0.297	4.38	=1.46
		=7•76 =9•75	0.02	=27.47 =32.36	8 10.806 8 12.319	107+34 102+86	-0.297 0.029	4 • 38 3 • 66	=1.46 =3.91
	5 6 7	=7 • 76 =9 • 75 =11 • 74	0.05 0.05 0.05	#27.47 #32.36 #38.05	8 10.806 8 12.319 8 13.934	107+34 102+86 90+79	-0.297 0.029 -0.084	4 • 38 3 • 66 5 • 23	=1.46 =3.91
	5 6 7 8	=7.76 =9.75 =11.74 =13.74	0.02 0.02 0.02	=27.47 =32.36 =38.05 =43.65	8 10.806 8 12.319 8 13.934 3 15.722	107+34 102+86 90+79	-0.297 0.029 -0.084 -0.690	4.38 3.66 5.23 5.07	=1.46 =3.91 =6.65
	5 6 7 8 9	=7.76 =9.75 =11.74 =13.74 =14.76	20.0 20.0 20.0 20.0	=27.47 =32.36 =38.05 =43.65 =45.73	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770	107+34 102-86 90+79 90+93 86+02	=0.297 0.029 =0.084 =0.690 =0.813	4.38 3.66 5.23 5.07 5.45	=1.46 =3.91 =6.65 =4.30
	5 6 7 8 9	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25	0.02	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560	107.34 102.86 90.79 90.93 86.02 41.19	=0.297 0.029 =0.084 =0.690 =0.813	4.38 3.66 5.23 5.07	=1.46 =3.91 =6.65 =4.30 =9.33
	5 6 7 8 9 10 11	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26	0.05 0.05 0.05 0.05 0.05 0.05	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90 2.61	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774	107+34 102+86 90+79 90+93 86+02 41+19 32+47	=0.297 0.029 =0.084 =0.690 =0.813 0.045 0.306	4.38 3.66 5.23 5.07 5.45 1.45	=1.46 =3.91 =6.65 =4.30 =9.33 =10.63 =12.98
	5 6 7 8 9	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27	0.02	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90 2.61 7.39	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08	=0.297 0.029 =0.084 =0.690 =0.813 0.045 0.306 0.427	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84	=1.46 =3.91 =6.65 =4.30 =10.63 =12.98 =16.09
	5 6 7 8 9 10 11 12	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27	0.02 0.02 0.03 0.03 0.03 0.03	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90 2.61 7.39	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942 9 9.330	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35	-0.297 0.029 -0.084 -0.690 -0.813 0.045 0.427 0.427	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06	=1.46 =3.91 =6.65 =4.30 =10.63 =12.93 =16.05 =17.30 =15.91
	5 6 7 8 9 10 11 12 13	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27 8.24	0.05 0.05 0.05 0.05 0.05 0.05	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90 2.61 7.39	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942 9 9.330 3 9.833	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35 25.88	-0.297 0.029 -0.084 -0.690 -0.813 0.045 0.306 0.427 0.373 0.676 0.875	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06 =2.06	=1.46 =3.91 =6.65 =4.30 =10.63 =12.98 =16.09 =17.30 =15.91 =13.53
	5 6 7 8 9 10 11 12 13 14	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27 8.24	0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90 2.61 7.39 12.41 16.81 21.91	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942 9 9.330 3 9.833 4 10.825	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35 25.88 28.67 30.24	-0.297 0.029 -0.084 -0.690 -0.813 0.045 0.306 0.427 0.373 0.676 0.875	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06 =2.06 =3.80	=1.46 =3.91 =6.65 , =4.30 =10.63 =12.98 =16.09 =17.30 =15.53 =9.55
	5 6 7 8 9 10 11 2 13 14 15	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27 6.27 8.24 10.28 12.28 14.27	0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05	=27.47 =32.36 =38.05 =43.65 =45.73 =2.90 2.61 7.39 12.41 16.81 21.91 27.09 31.61	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942 9 9.330 3 9.833 4 10.825 6 11.963	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35 25.88 28.67 30.24 26.21	-0.297 0.029 -0.084 -0.813 0.045 0.306 0.427 0.373 0.676 0.875 0.869 1.148	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06 =2.06 =3.80 =4.44 =6.24	=1.46 =3.91 =6.65 , =4.30 =10.63 =12.98 =16.09 =17.30 =15.53 =9.55 =6.88
	5 6 7 8 9 10 11 2 13 14 15 6 17 18	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27 6.27 8.28 12.28 14.27 16.26	0.02 0.02 0.03 0.03 0.03 0.03 0.03 0.03	27.47 32.36 38.05 43.65 45.73 2.61 7.39 12.41 16.81 21.91 27.09 31.61 34.05	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 8.942 9 9 9 330 3 9.833 4 10.825 6 11.963 0 13.282 9 14.993	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35 25.88 28.67 30.24 26.21 25.59	-0.297 0.029 -0.084 -0.813 0.045 0.306 0.427 0.373 0.676 0.875 0.875 0.869 1.148 1.736	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06 2.06 2.06 2.06 2.44 2.6.24	=1.46 =3.91 =6.65 =4.33 =10.63 =12.93 =16.09 =17.30 =15.53 =9.55 =6.82
	5 6 7 8 9 11 12 13 14 15 17 8 19	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27 6.27 8.24 10.28 14.27 16.26	0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.03	27.47 32.365 43.65 45.73 2.61 7.39 12.41 16.81 21.91 27.09 31.61 34.05 35.62	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942 9 9.330 3 9.833 4 10.825 6 11.963 13.282 9 14.993	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35 25.88 28.67 30.24 26.21 25.59	-0.297 0.029 -0.084 -0.813 0.045 0.306 0.427 0.373 0.676 0.875 0.869 1.148 1.736	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06 2.06 2.80 4.44 =6.24 =10.47	=1.46 =3.91 =6.65 =4.30 =10.63 =10.63 =16.09 =17.30 =15.55 =6.82 =4.24 =8.54
	5 6 7 8 9 10 11 2 13 14 15 6 17 18	=7.76 =9.75 =11.74 =13.74 =14.76 Q.25 2.26 4.27 6.27 6.27 8.24 10.28 14.27 16.26	0.02 0.02 0.03 0.03 0.03 0.03 0.03 0.03	27.47 32.365 43.65 45.73 2.61 7.39 12.41 16.81 21.91 27.09 31.61 34.05 35.62	8 10.806 8 12.319 8 13.934 3 15.722 2 16.770 8 8.560 0 8.774 5 8.942 9 9.330 3 9.833 4 10.825 6 11.963 13.282 9 14.993	107.34 102.86 90.79 90.93 86.02 41.19 32.47 26.08 23.35 25.88 28.67 30.24 26.21 25.59	-0.297 0.029 -0.084 -0.813 0.045 0.306 0.427 0.373 0.676 0.875 0.869 1.148 1.736	4.38 3.66 5.23 5.07 5.45 1.45 1.14 0.84 0.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.06 2.07 2.06 2.06 2.07 2.06 2.07 2.06 2.07 2.06 2.06 2.07	#1.44 #3.95 #4.36 #10.66 #12.93 #16.00 #17.3 #15.55 #13.55 #4.2 #8.5

22.27

24.25

25 . 25

0 . 24

21

22

23

0.02

0.02

0.02

0.02

41.881

45,573

48,072

-2.875

23:284

26.327

8 • 659

28 + 321 = 101 + 45

≈69·43

=88.31

VOUGHT LOW SPEED WIND TUNNEL TEST 630

WIND AXES

RUN 57 11/20/81 0933 : RUN '57

TEMP 70.

PS 14.6759

QPSF 75.00 VFPS 254.16 RNFT 1572087. MACH 0.2252

T01 702 T03 T04 T05 T06 T07 T08 T09 T10

0 0 32 0 14 32 0 0 0 0

T11 T12 T13 T14 T13 (6 727 T28 T19 T20

0 0 32 32 0 0 0

CORRECTED FOR THE AND INCREEN MAD EFFECTS
SINGLE SUPPORT DATA DATA OF BUILD SCALE DATA

PNT	.ALPHA	PSI	L/Q	D/®	B. 48	A 3 M	RM/Q	YM/Q
1	0.24	0.02	=2.242	4.928	250	FU#0.22	1.43	. =8.68
2	-1.75	0.02	*8.703	5 • 135	boe33	#2+7:08	2.80	· =6 • 72
- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	=3.76	0.02	=15.496	5 • 699	80.5%	·90.643	3.42	
4	=5.77	0.02	m21 + 144	6.423	99.76	□C • 737	3.37	=4+34
5	-7.77	0.02	=26.218	7.697	105.35	₩0.584	3 • 08	-5+37
4	≠9•75	0.02	=31.261	9•199	100.89	#0,064	4 + 19	· =9.05
7	-11.77	0.02	×37.744	10.956	105.07	-0.292	4+94	-5.80
	=13.76	0.02	-44.047	.12.903	114.92	-0.644	5.07	8-76
<u> </u>	-14.76		-46.999	14.103	116.88	-1.093	5.03	. =9.21
10	0.24	0:02	-2.375	4.900	33,15	-0:489	1.51	=8+54
11	2.27	0.02	2.910	4 + 541	23.93	=0 :320	1.19	=12+70
12		0.02	7.793	5 . 175	15.04	=0.240	0 +65	=14.56
13		0.02	12,684	5.562	10.61	-0.228	-1.35	=15·79
		0.02	17+248	6.134	13.30	0.044	=3.33	.=15+84
15		0.02	21.977	6.989	15.61	0.375	=4.31	-12.67
16		0+,02	27.228	8 • 196	17+04	. 0:449	=5.67	±8.29
- 17		0.02	31,581	9.713	12.02	1:060	- 7 •89	: =6.95
18		0.02	34.391	11.544	9.63	2.049	=12 - 15	· =5 • 04
19		0.02	34.964	.14.661	-39.21	0.313	∞6.38	· #7.73
20		0.02	38.901	17 + 444	=64+49	m0 .132	-3.77	-7.99
2		0.02	41.995	20.110	₩87.74	-0.290	-1:32	
22		0.02	46.235	23.233	=107∙95	0:761	=3.0.0	-10.07
23		0.02	48.928	25.200	=120.53	1.279	=5+94	=11.25
24		0.02	=2.608	4.993	33 45	=0.662	1.67	=8 • 14
And 1	~ ~ ~ ~ ~	- 1 V A						

YOUGHT LOW SPEED WIND TUNNEL TEST 630

			•		W	IND	AXES									
		₹UN_	58			A A A A A A A A A A A A A A A A A A A	11/	20/8	1 ΩS)33		·	: 1	RUN 5	8	
				TEM	₽ 7	۵.					PØ	14.6	660		•	
The second secon		PSF	75.	00 T01			54.2 T04		Ar Degr					0 • 225	3	
egyang hetsesspiralised		<u>. 2000 - 2, 11 (12)</u>		0	0	32 713	0 T14	11	31 T16	0	0	719 0	0			
	aING	E SI	JPPOF	CO AT DA	RREC	TED	FOR.	TARE ATA	AND	INTI	ERFE	RENC! Full	EFF1 SCALI	ECTS E DATA		
distribution of the state of th	DNT	AI PI		PST		: ZÖ		D / O	D 1	4.Zn		Y / 13	RM.	/ D ·	YM/G	1

	NGLE SUPP	OK I DK		DAIA	T C+G+	<u> </u>	SCALE DI	VIA.
PN	T ALPHA	PSI	L/Q	D/Q	PM/Q	Y/4	RM/Q	· YM/Q
	1 0.25	0.00	=3.009	5,567	38 • 13	5,473		=164+86
	2 -1.75	0.00	-9.509	5.780	57.21	5.068	33,22	=164.35
	3 =3.75	0.00	-15.731	6 • 118	82.95	5 . 448		¤166•35
1	4 =5.76	0.00	×22 · 171	6.905	104+98	5 • 691	46 + 44	=170+67
*	5 =7.77	0 + 0 0	m27.048	8.035	106.01	6.254	53 432	#176 • 77
	6 =9.76	0.00	=31.578	9 • 341	99.76	7.111	64 4 31	4188•39
	7 -11:75	0.00		10.997	105 * 73	7:131	69.37	■189+94
	8 =13.76	0.00		12.936	114,12		76+74	=190.05
	9 -14.76	0.00	-46.317	14.067	116.29	6.910	81 47	-195.34
1	0 0.25	0.00	=3.109	5.560	38.52	5.433	26 + 49	=165 • 11
1		0.00	2.767	5.630	27 - 04	. 5.315	19.21	=162.12
1	2 - 4 - 26	0.00	7.715		18 * 29	5.067	12:22	=159+29
	3 6.25	0.00	12.191	6.126	12.10	. 4.826	5.23	=155+74
	4 8 . 24	0.00	16.664	6+628	15.09	The second secon		-150-19
	5 10.26	0.00	21.484	7			· ×9.50	=149.10
	6 12.26	0.00	26.405	8 • 688	17=74	5:168		=144.09
	7 .14 . 25	0.00	30,752	10.267	11.21	5 • 499		=139+62
	8 16 - 23	0.00	33.108	12.027	8 • 73	6 + 4 4 3	-32.00	=134.46
	9 18 24	0.00	34.305					-142.43
	0 20.25	0.00			=71 -17			=145.90
	1 .22 . 26	0.00	42,215					=157.50
	2 .24 . 26	0.00				6.006		=158+44
	3 25 25	0.00	49.520	26 • 155	=129.27	7:015		=160 +44
	4 0 - 25	0.00	=3.276	5.600	37 • 18	5,240		=164+06

=22.21 =140.81

=31#19 =136.97

=32.08 =142.03

=36.07 =147.59

-42.55 -1% 6.10

=53.28 =167×12

#60×59 #168*%

4.779 21.65 -143.03

			WTND	AXES					
		····· /********************************	7439	.4750					
	RUN 59			11/20/81	0933		RUN	59	
		TEMF	70.		•	PØ · 14c	6660		
	QPSF 7	5.00	VFPS	254,25	RNFT 15	71561.	MACH O*	2253	
		TOT	*02 TO	3 TO4 TO5	TO6 ቸርታ	POT ROT	T10		#1
<u> </u>	<u>منفود شوه این استام چوه این سب</u>	0	0 5		31 0	0 0	0	<u> </u>	
		T11	T12 T1	3 714 715	T16 T17	718 T19	720		
		. 0	O 3	2 32 0	0 1	0 0	Q		
TNP	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/4	RM/Q	YM/Q	
	ALL A STATE OF THE SECTION AND ADDRESS OF THE SECTION ADDRESS OF TH	0,00	-3.14		46.03	- 4.939		-143+04	
			-9.30		61.46	5.001		=144.79	
			#16.30			5.161		=146.92	
4		0.00	=22.27		100.68	5.231		=151.26	
5		0.00	=28 (24)		110 • 48	5 4 6 0 7		=156 • 44	
6		Ø • O O	=32.31	3 12.534	103446	6.599	20.17	=170 • 09	- सम्बद्धाः
	44.70	0.00		AND REAL PROPERTY OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED	103.65			-667-04	
	=11.79 =13.78	0.00	-38.00	8 14.036	95.31	. 6,381	63,02	=167e31	
8	-13.78	0.00	#38.00 #42.24	8 14.036 4 15.730	95•31 87•09	. 6,381 6,261	63.02 69.16	=179.91	
8	=13:78 =15:03	0.00	#38.00 #42.24 #45.22	8 14:036 4 15:730 6 17:039	95.31 87.09 86.49	6,381 6,261 6,295	63.02 69.16 73.30	= 179.91 = 178.97	
8	=13.78 =15.03	0.00	=38.00 =42.24 =45.22 =2.94	8 14.036 4 15.730 6 17.039 2 9.201	95•31 87•09 86•49 44•53	6,381 6,261 6,295 4,807	63.02 69.16 73.30 21.33	=179.91 =178.97 =144.14	
3 9 10	=13.78 =15.03 0.27 : 2.42	0.00 0.00 0.00	#38.00 #42.24 #45.22	8 14.036 4 15.730 6 17.039 2 9.201 9 9.372	95.31 87.09 86.49 44.53 36.25	6,381 6,261 6,295	63.02 69.16 73.30 21.33 15.25	= 179.91 = 178.97	
10 11 11 12	-13:78 -15:03 0:27 : 2:42 : 4:28 6:32	0+00 0+00 0+00 0+00 0+00	=38.00 =42.24 =45.22 =2.94 2.80	8 14.036 4 15.730 6 17.039 2 9.201 9 9.372 6 9.506	95 • 31 87 • 09 86 • 49 44 • 53 36 • 25 29 • 63 25 • 35	. 6,381 6,261 6,295 . 4,807 . 4,733 4,647	63.02 69.16 73.30 21.33 15.25 10.58	=179.91 =178.97 =144.14 =140.94 =141.06 =140.20	
3 9 10 11 12 13 14	-13:78 -15:03 0:27 : 2:42 : 4:28 6:32 8:26	0.00 0.00 0.00 0.00 0.00	38.00 42.24 45.22 =2.94 2.80 7.35 12.06 16.41	8 14.036 4 15.730 6 17.039 2 9.201 9 9.372 6 9.506 3 9.864 3 10.396	95.31 87.09 86.49 44.53 36.25 29.63 25.35 27.36	6,381 6,261 6,295 4,807 4,733 4,647 4,760 5,011	63.02 69.16 73.30 21.33 15.25 10.58 4.42	=179.91 =178.97 =144.14 =140.94 =141.06 =140.20 =142.58	
10 11 11 12	-13:78 -15:03 0:27 : 2:42 : 4:28 6:32 8:26 10:22	0+00 0+00 0+00 0+00 0+00	=38.00 =42.24 =45.22 =2.94 2.80 7.35	8 14.036 4 15.730 6 17.039 2 9.201 9 9.372 6 9.506 3 9.864 3 10.396 7 11.213	95 • 31 87 • 09 86 • 49 44 • 53 36 • 25 29 • 63 25 • 35	6,381 6,261 6,295 4,807 4,733 4,647	63.02 69.16 73.30 21.33 15.25 10.58 4.42 41.85	=179.91 =178.97 =144.14 =140.94 =141.06 =140.20	

17

18

19

20

21.

22

23

-14-26

1.6 + 23

18.25

20.24

22.26

24.28

25.25

0.24

0.00

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0.00

0.00

0.00

0.00

0.00

30.947

33.708

34.560

37.934

41.315

46.365

48.947

=3.676

13 • 681

15.421

18 + 439

20.864

23.515

27 * 105

28 • 854 = 108 • 58

9.333 46.77

24+91

24.12

***19.03**

=53.78

=75.06

≖96 ∗38

5 • 6 4 6

6,609

5.575

5.576

6:290

8 9 9 8 2

7.751

=58.87 **=**162.66

21:42 =139:65

VOUGHT LAW SPEED WIND TUNNEL TEST 630 WIND AXES 11/20/81 0933 RUN 60 RUN 60 TEMP 70. PS 14.6660 * 4PSF 75.00 VFPS 254 . 25 RNFT 1571561. MACH 0.2253 TO1 TO2 TO3 TO4 TO5 TO6 TO7 TO8 TU9 T10 0 Q **5**9 0 11 31 0 0 0 T11 T12 T13 T14 T15 T16 T17 T18 T19 T20 0 0 32 32 Ö Ω. CORRECTED FOR TARE AND INTERFERENCE EFFECTS SINGLE SUPPORT DATA DATA AT C.G. FULL SCALE DATA PNT .ALPHA PSI L/Q DIQ PM/Q Y/Q RM/Q YMZQ 0.23 0.00 9.466 - 43.17 - 4.739 : 21.36 -139.64 1 #45.E= 0.00 =9.543 2 -1.76 . 27.80 -141.43 9.513 60.38 4.528 3 -3.77 5.048 . 33.28 =144.86 0.00 -16.072 9.904 83.16 10 - 411 -5 . 77 0.00 #22,238 5.065 40.38 =146.98 98 18 108.33 5.587 **≈**7∗76 49+04 =155+04 0.00 =27.881 11.348 55.81 =166.68 =9.73 0.00 -32.182 12.635 103.36 6.403 14.150 91.32 6.565 7 -11-76 63.08 #173.25 0.00 #37.725 8 -13.77 88.32 - 6:160 0.00 -42.643 15.763 69+44 -172-92 73.27 -172.96 9 -14.76 0.00 -45.130 16.947 84.84 6.176 10 0.00 4.773 0 + 25 **=3.509** 9 466 43.37 21.78 =140.70 2 • 24 11 0 + 00 2.265 9.563 . 35.24 4,668 15+43 =137+04 . 4.25 7.421 4.613 12 0 + 00 9.671 27.16 10.09 =136.15 9.959 13 . 6 . 24 0.00 11.790 23.29 . 4.659 5,63 =137.73 14 8 . 25 0.00 25.55 4,998 · =1.85 =140.06 16.445 10.542 10.24 0.00 =8.52 =141.60 15 21.016 11.314 27 . 81 5.312 16 0.00 =14.57 =139.90 12.27 26.573 12.522 . 28 • 51 5 • 268 17 5 1579 =21.97 =138.69 .14 . 26 0.00 30.967 13.908 22.86 18 16.25 0.00 33.857 15.763 -29.32 -133.73 21.53 6+363 -30.85 -137.73 19 18 . 25 0.00 34.166 18.765 =28.03 5,261 20 20.26 0.00 37.949 21.081 5 5 C91 -32.83 -141.37 =51+17 21 28.26 0.00 42.595 24:122 -80.95 5 476 =40.38 =150.56 22 .24.27 0.00 -50+58 -159+25 46.331 27.403 -103.62 6 . 755

23

25.26

0.23

0.00

48.901

0.00 43.344

29 • 136 = 116 • 32

9 4 4 9 9 4 2 4 7 4 4 4 6 3 9

*				BUGHT Le	N SPEED	WIND TU	NNEL TES	r 630	and the second of the second o	2333 200 \$1,\$444 4244 424
					WIND:	AXES				
			RUN 6	1		11/20/8	1 0933		RUN	61
•		•	•	TEMP	70.			P6 14*	5660	
			QPSF	75.00	VFPS 2	54.25	RNFT 15	71561.	MACH O	2253
				TOT	702 TO3	T04 T05	T06 T07	T08 T09	T10	
				0	0 59	0 11	31 0	0 0	0	
				T11		T14 T15	T16 T17	T18 T19	T20	
		SIN	LE SUP	COR PORT DAT		FOR TARE	AND INT		E EFFECT SCALE D	
		PHT	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/@	RM/Q	, AW\Ø
		1	0.24					5.173		-151 - 81
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2 3	=1.76 =3.76							*152*99
، نشد		4	=5 · 75		-16.272 -21.870			5.574 5.665		<pre>=156.90 =159.28</pre>
٠.		5	-7.77		=27.815		107 • 93	6.054		-165.20
		6	=9.76		-32.411			6.598		=178 • 14
4.41		7	-11.76		-37.65 2	.14+297	91.00	7.052	69+69	-184.29
an post il		8			-42,741			× 6.770		m180.71
<u> </u>		9	-14.76		+45,297			6 • 6 4 3		m183.84
		10	0 • 25		=3,209			5,206		=150+97
		11 12	2 • 27		2.667 7.521		34 • 81 27 • 11	5:129 · 4:980		#149*45 #146*01
		ែរ			11.992					=147.82
		ī+	8.26		16.775					=149+06
-4		15	10.25		21.350	السديد في الأراب		المسالسات		=150.76
	,	16	12.27		26.640			5,668		=147+56
	•	1.7	14.26		31.240	13.975	23.33	5 . 8 4 6		-144+28
		18	. 16.28		33,727			6.545		=139.44
		19	18 - 24		34.532					-144+73
and the		20			38.783					=151.77
		21 22	.22 • 27 ·24 • 26		42.536 46.510			5.524 6.933		=159 • 63 =169 • 77
		23	25.26		49,261			8,211		=169+23
		24			=3.143					-151 - 41

A-157

VOUGHT	LOW SPEEL	WIND	TUNNEL	TEST.	<u>630</u>
			,		
		•	•		
	WIND	.AXES			

RUN 62 11/20/81 0933 : RUN 62

TEMP 74.

1

PØ. 14.6660

QPSF 83.00 VFPS 268.47 RNFT 1637583. MACH 0.2370

TOI TO2 TO3 TO4 TO5 TO6 TO7 TO8 TU9 TIO

O 0 48 0 13 31 0 0 0 0

T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

O 0 32 32 0 0 1 0 0 1

CORRECTED FOR TARE AND INTERFERENCE EFFECTS
SINGLE SUPPORT DATA DATA AT C.G. FULL SCALE DATA

PNT	ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	. RM/Q	YM/Q
		0.02	-2,861	9•365	48.60	517.22		=151+21
		-2.01	2.991	9.232	50.19	1.918		=140+08
		=4.00	#3.126	√ 2•305	50.81	=1.976		-126.45
4		=6.01	=2.726	9.701	43.36	=6.700	24.41	=107.36
5.		=8+03	=2:426	10.208	37•73	=11:050	21 +85	80.68
			=1.472	10.911	30.59		16 66	= 55∙04
7		-12.02	-0.114	.12.046		= 20,550	11044	:=27.46
			1.230	13.638		=25:181	8•93	
			2.575	15.527	7.17			. 36•23
1.0			3.488	17 • 645	1 • 10	=33∙801	7.82	67.50
11			4.389	20.080		= 37.999	6+79	94.51
12		:=22.03	6.369	23,008	<u> =22.98</u>		4 • 87	121 • 04
13		.=23.99	8 • 187	25.879		=46.734		
		.=26.00	9.600	28.927		■50•649		
4		.#28+00	11.055			*53+943	5.01	
1.6		≈30.00	11.140	34•393	=27 • 85	m56,936	9+70	170 • 84
17		0.00	-2.922	9•396	47+94	5 • 8 4 6	24+85	
18		2.01	=2.981	9 • 494	45•03	8 • 7 2 4	23.18	
		4.01	-2.927	9.830	41 • 15	.11:878		
<u>3</u> 0			-5.555	10.341	30.75	16.284		=194.96
21			-1.347	10.946	16.88	19:999		-209 . 42
22		10.02	=0.249	11.787	4.27	24:030		-227 • 15
23		12.00	0.826	12.776	≈7 • B1	28:006		=244.09
24		14.00	2.146	14.075	=20.16	30.927		=271.50
2:			3.791	15.707	-33.51	37.251		-291.08
26	0.26		4.793	17.638	-41.75	41.898		-312.36
27			6.014	20.058	-47.48	47.0311		=352.30
28		22.01	7.537	22.759	=58 • 18	52,771	54+73	
29			9 • 142	25.596	=67.16	57 • 261	54.73	413.94
30		26.00	9.301	29 • 698	=44.94	58,534		Annual Control of the Party of
31			9.993	33 • 157	=39.80	62.547		
		30.01	9.616	36.354	-25.36	65,316		
33	0.26	0.00	=2.862	9,335	48.08	5.243	26.99	=150.76

1	٧e	U	GН	T.	1.6	١W	S	0	F	Ξ[)	W	Ï	N	D	. 1	٢L	١ħ	Jŀ	V	ΞΙ	. K	TF	9	٦	 53	30)
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n		N	u	٠, ۴	١X	_	O

	709	14+6	PO					75.	TEMP	•
(O #2370	MACH	9 a	3397	163	RNFT	3	68.6	FPS	•00	QPSF
	TIO	TUS	7.08	T07	T06	T05	T04)2 TO	TOT TO	
7.55-7410)3G1/	Q	· U	0	0	31	13		0 4	Q	
	T20	T19	T18	T17	T16	T15	T14	.2 Ti	T11 T	
	1	(1	0	4	0	O	.32	0 3	O	

CORRECTED FOR TARE AND INTERFERENCE EFFECTS SINGLE SUPPORT DATA DATA O.G. FULL SCALE DATA

	PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	. RM/Q	. AW\d
	1	Q • 25	0.01	-2.711	9 • 486	49+76	5 4 4 0 4		-147 • 89
	2	0.25		-2.841	9.383	52.29	1.648		=138 +90
<i>(</i>	3	0 • 25	=4.02	-2.826	9 • 3 9 5	50 • 05			-122.18
(4	0.26	= 5⋅99	■2.725	9 * 6 4 1	45•77	=6 € 372		=109.82
	5	0 + 26	= 7∙97	=2.332	10.226	38 • 81	■11 • 09 0	19#47	=82+33
	6		-10.01	=1.262	11.122		=15.812		=52.96
	7		-12.03	0.187	12.317		-20.909		
	8		13.99	1.320	13.879	12.31	#25,332	7 • 95	
	9		-15.99	2.637	15 • 798	7.71	-29.810		37.69
	10		≈18 ∗00	3 + 470	17.934	2.77			70.14
	11		.×20+04	4 • 1 47	20:430	=5+20	438 •492	6.23	97 • 96
	12		-22.03	6.037	23.248		≈42•797	2.68	124 • 98
	13		24.02	7 • 874	26.235	=31.56	m47 .647		
보스 4 시간 10년 전 10년 1 1887 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888 - 1888	14		~25 98	9.334	29 • 1,43	-36 86	+51 : 114		-166 • 85
	15		-28-02	10.845	32.040	-38.27	⇒54.43 0		
	. 16	0 + 26	.=29.99	11.414	34.897	≈28 • 28	■57.151	8 • 83	177 • 83
,	17	Q • 26	=0.01	=2.941	9 • 577	49 + 15	5.787	24.11	=149.60
	18	0 . 26	2.01	=2.891	9 • 675	46 • 75	8 + 8 4 6	22.51	#144 • 60
	19	0.26	4.03	*2.535	9.950	39.57	:12.068	25.76	=155 • 92
	50	0.26	5.99	-2.101	10@299	31.00	16 4 152	35.07	=151.38
	21	0 . 26	8.02	=1.196	11 + 114	17.01	20.076	39.33	-209 - 57
	.22	0.26	10+00	0.082	11.788	2 • 98	23.702		=218.36
	23	0.26	. 12:00	1.278	12.855	=9∙91	27:795	43.62	=240 +48
	24	Q • 26	14.00	2.778	14.256	=21 • 52	32 . 349	44.97	=264·88
	25	0.26	16.01	4.213	15,827	=34.99	37.180	46 • 52	=288.71
	26	0.27	17.99	5.324	17.519	-42.44			≈309·17
	27	0 # 27		6.558	20.098	=48.48	47 . 092		=348+26
<u> </u>	28	0.27		7.719	22.713	=57.34	52,381		=386+19
(29	0.27		9.264	25 • 447	=68.78	56.991		=407+43
· 📏	30	0 • 27	26.01	9.426	29 • 666	=43.28	57 . 996		≈354 • 8 0
	31	0.27		10.157	33.074	-39.10	· · · · · · · · · · · · · · · · · · ·		×377.71
	32	0 • 27			36 • 236	×24·13			₩378 • 81
医环状腺素抗原腺	33			-3,343	9.516	51.02			=148+43

			of poo	r quality		₽	<u>~159</u>	
		SUGHT L	W SPEED	WIND TUN	NEL TEST	r 630		
			MIND.	AXES				
	RUN 6			11/20/8	0933		RUN	64
		TEM	50.			P0 14.6		7 Table 1 Tabl
	@PSF '	75 • 00	YFPS 2	49•16	RNFT 16	51425,	MACH 0+2	251
		701	T02 T03	T04 T05	T06 T07	TO8 TU9	T10	
and the second s		0	0 48	0 12	31 0	0 0	0	
		T11		T14 T15	T16 T17	718 T19	T20	
		(1.00)						
	OLE CHE	CO; PORT DA-	RECTED	FOR TARE				
<u> </u>	GLE SUP	TORI DA	<u> </u>	DATA	AT C.G.	PULLS	SCALE D	MA.
PNT	.ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RMZQ	YM/Q
	0 • 25	0.01	⇒3.317			; 5.901		
	0.25		-3.388			2.047		
	0.25		-3.395			=1.896		<u>=127•18</u>
5	Q • 25 Q • 25	=5.99 =7.98	=3.005 =2.627		46+09	#6.230 #10.306	20+69	=110+69 =84+55
6	0.25	=9.99	-1.685			±14.930	15 +84	=57 · 79
7		-11.98	-0.391			≈19.748		
8		-13.99	0.852		The state of the s	-24,422		4 • 07
9	0 • 25	-15.99	2.156			#28.531		36+47
10		=17.99	3.409	17.316	4 • 90	433:144		68+91
11		=20.03	3.960			≅37∗70 7		100.08
12		.=21.99	5.815			≈42:179	3.17	122.78
13		.=23+99	7.408	25 • 851		546 € 623	=0 ≥59	148 • 55
		=26.00	9.026	28:857		The second secon	0.55	167 • 14
15	0.23	-28.01 -30.01	11.053			■54 • 7.55	1.86	174.06
_′ 17	0.23	0.01	11.003 =3.451	35 • 044	=28:17	■58 • 093	7+74 23+17	178+}/ =154+30
18	0 • 23	2.03	=3•401 =3•448	9•563 9•628	51•52 48•97	9.217		=148 + 18
19	0.23	4.00	-3.146			:12:690		=163+65
Žo			-2.412		30.80	16.658		=197.5 4
21	0.23	8.00	=1.615		17.03			-210.29
22	0+23	10.00	-0.357		2,17	24 • 111		=222.46
23	0.23	11.98	0.956		m10.43	28:197	42+34	
54	0.23	13.98	2.345	14.131	=23.43	32.606		=265∙51
25		and the second s	3,757			37.727		=291.92
26		18.01	4.963		1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A 1 A	.42.334		=312.62
27			6.094		-49.21	47. 806		⊯350.92
. 28		21.99	7.306		=58.57	53 • 039		=387+74
29	0.23	24.00	9.451		≠68 • 87	57.620		≖406.48
30	0.23	26.01	10.651	28 • 493	≖ 76∗73	62.545	5/+14	=434 • 15

31 32 33
 Q.23
 27.99
 10.062
 33.163
 =38.06
 63.024
 17.84
 =374.33

 Q.23
 29.99
 9.215
 36.122
 =21.37
 65.500
 9.93
 =376.25

 Q.26
 0.00
 =2.751
 9.450
 51.02
 5.790
 24.38
 =152.59

Name of the state		<u> </u>	IUGHT LI	W SPEEC	WIND TUN	NEL TES	r 630		· · · · · · · · · · · · · · · · · · ·
	**************************************		a benedik (7)	WIND	AXES	•			
(b.				224					
navanasi kanada kanada kata kata an salah kata ka		RUN 65	<u> </u>		11/20/81	L0933	-	RUN	65
			Temi	62.			PØ. 14+6	3955	
**************************************		QPSF 7	5.00	VFPS 2	252.07	RNFT 16	03691,	MACH 0 2	251
				خريدان يتريدين	المستعددات المتعارب المتعارب	ساعفة بمنسو			
Complete mark College and Control of the states					TO4 TO5				10. · · · · · · · · · · · · · · · · · · ·
			0 . Tak	0 55		31 0	0 0	0 720	
			177	712 T13	714 T15	T16 [17	718 119	1 60	
			-	<u> </u>	<u> </u>	<u>V1</u> .	<u>V</u>	<u> </u>	
# 1			CO	RECTED	FOR TARE	AND TRITI	FREERENCE	E EEFECTS	i :
1	SINC	LE SUPP	ORT DA	74		AT C.G.		SCALE DA	
the and built of the second developing and the second seco				*					
	PNT	ALPHA	buī	Γ\Ø	D/Q	PM/Q	.A\m	RM/Q	. AW\o
4) 76	1	0.26	0.00	=3.309	9 • 634	44.49	5,027	24.21	=147.38
4 1 1 1 1	2		0.00	=9.742					=148 ×98
1	3	=3.74	0.00	-16.171		84.64	5.335		=153∙93
(4	=5.77	0.00	×22.438		100:12			=156+59
	5	≠7 • 77	0.00	=27.648		108 • 28	5 674		-162.52
	6	=9.77	0.00	-32.212		102 • 12	6.498		=177 • 21
	7	-11.77	0.00	-37.720		94+01	6.573	68.78	=179.48
and the second s	8	m13 . 76	0.00			83 • 61	6,358		=178.79
and the second s	9	-14.77	0+00			89:81	6.265		=183.16
	10	0.25	0.00	=3.37 6		43+98	. 4.960		=147+29
	11	2+27	0.00	2.334		35.92	4.715	17+08	-145+30
Processor in the contract of t	12	· 4.27	0.00	7.223	9.772	27.78			m144.47
	13	2 - 2 - 2 - 2	0.00	11.727	10.061	23.22	4.786		-147 - 41
÷	14	8.26	0.00	16.213		24.49	5.125	=1.39	-147 . 05
Charles and the state of the st	15	10.26	0.00		11.449	27.76			×151 • 79
,	16	12.24	0.00	26.370		28 • 83	5 4 4 3 4		=146.39
7	17	14:26	0.00	31.213		22 * 62			=145.61
·	18	16.26	0 * 00	33,631		19.86	6.650	<u>=32 •76</u>	=140.23
	19	18,26	0.00	35.041		-26.32			-144.01
**************************************	50	50.58	0.00	38.325		=57+62		=35.93	×149 • 45
	21	22.24	0.00					-42.54	=158 · 11
	22	24.26	0.00			=106.04			#165.79
	23	25.26	0 * 00	49.25			7.837		=168.61
	24	0 • 25	0 + 0 0	3.40 9	9 603	45 • 46	44926	24 * 26	=148.69

ORIGINAL PAGE IS OF POOR QUALITY

A-161

in cho rthaellans a	Manager Comments and State of the Comments of		BUGHT L	W SPEED	WIND TUN	NEL TES	<u>0</u> 26	tion of the Company	, pod i kazalik taloniyy pod od to s
		KAN TANAN TANA		WIND.	AXES	Nigotalani, asi isi katalani daga nigo basinya	and the second second second second second	a villainetti (Mg F Nita 200 ka pilli ili ili ili ili ili ili ili ili i	a quarante la materia de
CELLE NO. OF THE PARTY OF THE P	- Name of the state of the stat	RUN 6	6	water a best of the said state of the	11/20/8	10933		RUN	66
			TEMP	64.			PO 14.6	985	
		QPSF	75.00	VFPS 2	52 • 55	RNFT 15	95961.	MACH 0.2	251
			ት የአቀ	መስማ ማሽን	T04 T05	907 MAH	ቁለው ምክይ	ተ ላለ	
ALL SHARE BACKET AND A SERVICE	See 3rs. Add with the section of the	. dal manda, di syralmani si	Ď,	0 59		31 0	<u> </u>	0	wa an order
					T14 T15	715 717			
	AND THE RESERVE OF THE PROPERTY OF THE PROPERT	Manager of the Author State of the			32 0	0 1	0 0	. 0	<u> </u>
12° 244	SIN	GLE SUP		RECTED				EFFECTS SCALE DA	
	PNT	ALPHA	PSI	L/Q	0/0	PM/Q	YZQ	RM/Q	· YM/Q
AD THE PROPERTY OF THE PARTY OF	1	0.25	0.00	=3.343	9.666	45.48	4.620	21.47	=138.65
	2	-1.75		-10.009			41734		-140 - 11
	3	-3.76		=16.538			4.994		-143.21
(4			=22.371		100.90	4.991	41,413	
	5	≈7.76		-27.814		108,49	5.333		-150.05
	<u> </u>	<u> #9.75</u>		-32.417			Careful Conference (1965-1180) Fredericker - Illian		=164.35
		-11.76		■37.872		and the same form	6.098		=167.85
	8 9	H13+75		442.534		85.66			m169 • 65
a upotani di distributi di ancioni	. 10	-14.77 0.24		-44.925 013.E=			5.792 4.586		<u>-170 •57</u> -138 • 65
	11	2.24		2.065		44+69 36+61	4.368		=136.94
	12	4.26	0.00	7.188			4.360		=130 €5 =134 • 99
ra)). It is seen in the sandamic of the	13			11.758		24+13	4.472		=138+73
	14		0.00	16.414		25.96	4 8 4 5		=139 · 0
and the same of th	15	10-25		20.983		28.03		=9.76	-143-89
	16	12.26	0 • 0 0	26.305		28.92	5.348	=15.49.	=141.8
-	. 17			31.098	14:113	22.79	5.539	=22.52	=138.92
all successions and and and all all all all all all all all all al	18	16.25		33.583		21.08	6.390	=32.52	
	19	18 - 24		35.079			5 474	#32+24	
	20			37.986			5.201	≖ 35•33	
despendent software and	21	22.25		42.241		-80.91	5.521	-41.05	
	55			45.968		=102 • 18	6.296	= 50 . 53	
	29 24	25 24		49 266			7.526	=59 +04 04 • 35	
	<u> </u>	0.26	0.00	=3.409	9 • 6 6 7	45.52	4.520	C1030	=139.17

A-162.

•			Or Lega.	10 7-1			<u>.</u> †† <u>@</u> 5% •	
1	VAL	icur la	w Spefn	WTAD TIE	INEL TEST	1 630	THE PARTY AND THE PARTY	*
and the state of t			WIND A		MEL WIES	<u></u>		
								,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	100 ALCONOMICS			n kind ja de Aria. Ngjara	1			
	RUN 67			11/20/8	0933		RUN	'67
<u> </u>	RVII		<u></u>	-LIVENIA	نىڭ كەلچىك ئىلىسىنىسى			
		TEMP	65•			PØ 14+6	955	
44					de a production de la constitución	56440	MACH OLO	os d
	gPSF 75	i•00	VFPS 25	2.79	RNFT 15	921184	MACH OFE	251
		TO 1	EDT SOT	TO4 TO5	TO6 TO7	T08 T09	T10	
and the second s		0	0 67	0 19	31 0	0 0	0	
		T 1 1				T18 T19	T20	
(A)		0	0 32		0 1	0 0	<u> </u>	
	[15] [16] (16] [16] [16] 함께 (16] [16] [17] [16] [16]					adalah d		
		COR	RECTED F	OR TARE	AND INT	ERFERENCE	EFFEUIS	
SIN	GLE SUPPO	IRT DAT	A	DATA	AT CLG	PULL	SCALE DA	VI A
ran?	ALBUA	PSI	1.70	D (0	PM/Q	YZQ	RM/Q	YMZQ
PNT	ALPHA	LOT	Γ\Q	D/Q	יט קויו דו	1 / 54	Mar a	1 + 1 / Og
1	0.25	0.01	-9.742	8.218	43.45	5.721	20.13	-141.99
		and the second of the second of the second of	#13.752	8 • 552	67.81	. 6.152		-147.71
	海绵 化二甲基酚 化二甲基二酚二酰甲基			9.026		or and the second second	35.41	=155,046
4		0.01		9•693	122,25	7 4 4 4 6		4168 • 10
5	=7•77		-24.675	10.429	135.80	8 • 050		=176 +93
6			-25.566	11.676	122.37	8 • 6 2 4		<u>=185.31</u>
	-11.77		27,387		122.56			41.86 + 61
			-29.311	13.985	The section of the se			=184.90
	=1 <u>*•75</u>		-30.420	14,547				=181.90 =140.87
10		0.01	=9.776	8 • 184 7 • 929				=136+84
11	2.27	0.01	=5.947 =2.393	7.719				=134 • 5S
<u> </u>		0.01		7.685		, 5 · C84		#135·30
	8.25	0.01	4.618	7.795		the second secon		-140+66
15			8.720		=73.61	A company of the comp		=144.43
16		0.01	12.466	8.574				=147 .62
17		0.01	15.593		=113.00	5 818	=20.41	=149.51
18		0.01	17.698	10.701	=115.48	5 • 856		=153.05
19		0.01	19.780	12.028		5 • 948		m155.61
		0.01	21.368			. 4.931	40.00	-145.21
<u> </u>		0.01	22.753		-111.21			=135.50
22		0.01	24.139		≈108∗91			=115.71
23		0.01	25.342		=112.21			=108+65 =140+73
	نسخاس نسان	U 4 () ¹ 1	一 田 4 。 サバメ	× 1	44 W 4 7 1L		Z U #350	ニーサレチノご

0.01 =9.708 8.251 43.14 5.601 20.36 =140.73

24 0.25

			WIND :	AYES				
The second secon			NIND A	4VE2	· · · · · · · · · · · · · · · · · · ·			
		84		w B				
<u>an ita a angarang sa anga a sa at angara</u>	RUN 6	8		11/20/8	1 0933		. RUN	68
		TEM	P 74.			PO 14.6	5 9 55	
the state of the s	QPSF 1	6 0 - 00	· · · · · · · · · · · · · · · · · · ·	24.00	She's and	06297	HACH O.	2500
	Wror 1	00.00	VFPS a	74633	KNF (17)	7520/1	MACH O.	2077
			T02 T03	TO4 TO5	T06 T07	TO8 TO9	T10	
		0	0 67	0 19	31 0	Q V	O	
		T11		T14 T15	T16 T17	T18 T19	T20	
		Ca	RREGTED	FOR TARE	AND INT	ERFERENCI	E EFFECTS	and in 1995. Since the
SI	VOLE SUP	PORT DA	7A		AT C.G.	FULL	SCALE D	ATA
PN"	Γ .ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	. AW\đ
			-					
	L 0.24				A CALL OF THE REAL PROPERTY AND A SECOND CO.	5.485		#140+74
	2 =1,76 3 =3,78		=13.525			5.954		=147 +75
	3		=18:136 =21:728					=156.93 =166.66
	±7.76			10.338		7.809		=177 ⋅ 86
	5 =9.75		-25.335					=182.99
	7 =11.77			12.713	the state of the s	8.338		=184+45
	3 0.24			8 4 1 7 5	44.18	5 400		-141+44
	3 5.5					5 • 168		=137.71
1.0				7 • 642		5,005		≈133 •63
1:				7.567		4 8 8 5 9		≡136 • 05
1:	2 8 • 22 3 1 Q • 25			7.702		5.137		=140.56 =144.70
	4 12.24		8.570 12.432	7 • 923	=97.06	5.259		=147 • 95
	5 0.24	0.02	-0.444	9.091	-3/•UG		- 12,45 - 12,45	=141.73
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		1990 - Paris #110		off of North Control	the page of the second	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1. A. C.	

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23 25 25

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49.060 29.555 =116.64

=51.81 =158.29

-58.03 -163.07

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RUN 69	· · · · · · · · · · · · · · · · · · ·	-()		······································					The second second second	nyan masa masa ya sa ya sa
### RUN 65	(·	g, Se		OUT Im	i: carea	LOVEN TILL	niet west	F 4970		
TEMP 75. P6 14.6955 GPSF 75.00 VFPS 255.19 RNFT 1554537. HACH 0.2251 TGT T02 T03 T04 T05 T06 T07 T08 T04 T10 0 0 59 0 11 31 0 0 0 0 T11 T12 T13 T14 T15 T16 T17 T18 T19 T20 0 0 32 32 C 0 1 0 0 0 CGRRECTED FOR TARE AND INTERFERENCE EFFECTS SINGLE SUPPORT DATA DATA T C.G. FULL SCALE DATA PNT ALPHA PSI L/Q D/Q PM/Q Y/Q RM/Q YM/Q 1 0.24 0.00 =3.310 9.633 46.66 4.286 21.38 *135.40 2 -1.77 0.00 =3.376 7.46 63.84 4.501 28.59 =137.09 3 -3.77 0.00 =15.872 10.004 85.73 *1548 33.72 *140.62 4 =5.76 0.00 =21.771 10.572 99.66 4.554 40.86 *143.81 5 =7.76 0.00 =21.771 10.572 99.66 4.545 40.86 *143.81 5 =7.76 0.00 =21.471 11.381 107.80 4.813 47.11 *145.38 6 =9.78 0.00 *31.879 12.714 10.10 5.392 55.36 *160.49 7 =11.77 0.00 =37.140 14.424 86.79 5.386 61.02 *162.43 8 =13.75 0.00 *41.761 15.857 \$55.74 *1590 67.79 *163.56 9 =13.78 0.00 *41.761 15.857 \$55.74 *1590 67.79 *163.56 9 =13.78 0.00 *41.761 15.857 \$55.74 *1590 67.79 *163.56 10 0.23 0.00 *32.244 9.559 \$46.30 *13 *1501 76.99 *171.57 10 0.23 0.00 *32.245 9.664 38.02 *155 15.73 *135.25 12 4.26 0.00 7.421 9.772 31.27 4.127 10.98 *134.76 13 6.26 0.00 12.225 10.027 26.69 *1.25 5.77 *136.76 14 8.27 0.00 21.857 10.564 27.83 *176 1.828 *3.75 1.038 *137.16 15 10.26 0.00 21.848 11.381 30.775 5.099 *7.79 *136.76 16 12.27 0.00 26.606 12.422 31.76 *188 *13.16 *139.37 17 14.26 0.00 29.393 14.440 10.88 5.755 92.264 *131.46 18 16.25 0.00 32.670 16.129 11.57 6.422 -30.26 *131.46 19 18.26 0.00 35.214 18.707 -23.75 5.535 -31.03 *1.384.99 20 20.26 0.00 38.596 21.188 -56.34 *5.071 -34.956 -134.46	Control programme to the state of the state		YOU	uni Lo	M SPEED	MINT	INEL LES	<u> </u>	, , , , , , , , , , , , , , , , , , , 	
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QPSF 75.00 VFPS 256.19 RNFT 1554537. MACH 0.2251	and the second s	B	UN 69	· · · · · · · · · · · · · · · · · · ·		11/20/81	0533	<u> </u>	RUN	P
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2 -1:77		PNT .	ALPHA	PSI	L/Q	D/Q	PM/Q	Y/Q	RM/Q	· YM/Q
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Chipmentheses, - a reprinciple of the second	<u> </u>	ADOQUE F	W SMEED	··W.T. N.C.	NACL IES	030	· · · · · · · · · · · · · · · · · · ·	
			WIND	AXES				
				i de la		Transfer in the second		
				11/20/8	0000		RUN	70
	RUN	70		11/24/6	<u> </u>	<u> </u>		
		TEM	78•			PF 14.0	8857	
	GPSF	75.00	VFPs 2	55.99	RNFT 19	+3036+	MACH . O o	251
								arka a ser a sér
		<u>τυι</u> ο	702 T03	TO4 TO5	106 T07 31 0	0 0	T10	<u></u>
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S	ingle su	CO IPPORT DA		FOR TARE	and the same of th	ERFERENC FULL	E ERFECTS	S ATA
PI	NT .ALPH	HA PSI	Γ\σ	D/Q	PM/Q	Y/Q	RM/Q	YM/Q
	1 0 . 2	5 0.00	-3.276	9.233	49.00	. 4.206	20.66	#131.72
기가 있는 것 같아 하는 것 같아. 기가 나타가 하는 것 같아 얼마를 했다.	2 -1.7	4 0.00	-9,408	9.374	477	. 4:321		=133. 02
	3 *3.7		-16.439		88:66			=136.29
· · · · · ·	4 ≒5 • 7		=21.903		101+24	4.531		=141 • 07 =145 • 04
	5 =7.7 6 =9.7		≈27.647		109 • 69	4 • 686 5 • 312		=158.49
	6 =9.7 7 =11.7		=31.692 =37.406		97 • 54 92 • 17			=159 • 33
	8 -13.7	and the second section is the second			86.40			-163.74
	9 =140							=164+65
چاند آده آداد آی اور بازی بازی داده کوی در بازی داده کوی خود بازی بازی بازی بازی بازی بازی بازی و بازی و بازی ا	10 Q+2		=3.376		48.23	4 106		=132 • 17
	11 2.2		2.599		40.37			=130.61
	12 . 4 . 2	0.00	7.087		33.69	4.013		=130.57
	13 6.2		12.090	9.759	28 • 19	4:079	4.20	=131.77
	14 8 . 2	7 0.00			30 • 18	4,598		=133.52
	15 10 . 2						=9.09	=137.99
	16 .12 • 2					4 1735	=13.26	-136.32
	17 -14 + 2	26 0.00			14.23	5 . 846		=129 • 11
	18 16 • 2							=128∙91
	19 18 1			18.508	=23.32	5,329		=138+20
	20 ,20 0			20.828	-52.68			=140.67
	21 22 1				-77 • 70			=145 • 85
	22 -24 - 2							-158 · 15
	23 25 • 2	23 0.00	48.692	28 + 884	=112.35	7 + 378	=55.87	=159.89

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VOUGHT LOW SPEED WIND TUNNEL TEST 630
. WIND AXES
 RUN 71 11/20/81 0933 : RUN 71
TEMP 81. PO 14.6857
 GPSF 75.00 VFPS 256.70 RNFT 1532185. MACH 0.2251
0 0 59 0 11 31 0 0 0 0 T11 T12 T13 T14 T15 T16 T17 T18 T19 T20

CORRECTED FOR TARE AND INTERFERENCE EFFECTS SINGLE SUPPORT DATA DATA AT C.G. FULL SCALE DATA PNT .ALPHA PSI L/Q D/Q PM/Q 'Y/W RM/Q 'Y

PNT	.ALPHA	PSI		D/Q	PM/Q	.A\A	RM/Q	YMZQ	:
	0.24	0.00	-3.243	10.366	51+86	4.606		≒1 35•96	
		0.00	-9.343	10.646	68.42	4.661	28.49	=135.95	t i
			=14.704	11.239	91.29	4.301		=134.06	المسا
4	≈5 • 7 4	0.00	=19.903	12,306	105.81	4.265		=135.02	
5		0+00	m24.562	13.482	113.12	· 4 : 134		=134.31	,
6			=27.785	15.310	97.07	4 • 072		=140.21	
	=11+77		-31.840	16.933	95.52	63,953		=146.97	
	-13.78		=36.071	18.660	92.27	. 4 : 134	63.08	=153.62	
	=14+77		#38.132	19.691	91.55	. 4.345	66.91	=158+05	
10		0.00	=3.176	10.333	50.46	4 • 573	20 • 82		
11		0.00	2,669	10.166	41 • 99	4 • 629	13.96	=136.28	
12		0.00	7 • 688	10.305	33.54	- 4 • 680	8 • 5 6	≈137•03	
13	6.26	0.00	13.159	10.594	28.24	. 4 . 759	3 * 25	=138+80	
Language Company	48.84	0.00	17.879	11.164	28.70	4.931	-1-99	=138.53	
15		0.00	22.982	12.015	32.87	5+266	-9-17	-143 -44	
1.6	12.24	0.00	28.003	13.054	35,13	· 4 • 888	-12.77	=140.90	_
. 17	.14.23	0.00	30.610	14.811	16.87	5 4 6 7 8	=22:42	M132.96	
18	16 • 25	0.00	33.570	16+663	15.58	6 4 4 6 3	=31.67	=130.22	
19	18.26	0.00	36.501	19+241		5,609	=34.71	=138.97	
20	50.56	0.00	39.269	21.575	=49.27	5.091	=35.06	=143.34	
. 21	22.24	0.00	42.233	24.466	*=78 · 80	5.813	-42.03	=146,36	
22		0.00	45.751	27.669	-102.83	6.522	=48.17		
23	25 • 27	0.00	48.922	29 825	≈117.34	7:086	-54+60	=163.15	
24	0 . 25	0.00	=3.576	10.333	51.39	4.573		=135 • 27	
			**************************************			·····	· · · · · · · · · · · · · · · · · · ·		

-35.33 -142.13 =41.98 =<u>150.67</u>

=49.21 =160.50

=56 • 13 = 162 • 01

20.39 =134.19

5 . 644

6:175

6.966

•							•	
		HGUT I	u secen	WTMD TIIN	NEL TES	F.,630		
	<u>Y9</u>	udni L			VINEL 150		and the second s	<u></u>
			WIND A	XES				and the second s
	RUN :72			11/20/8	0933		RUN	·72
	. NON ./E	TEMP	84.			PØ 14.	6562	
	QPSF 7	5+00	VFPS 25	57•67	RNFT 15	19934•	MACH OR	2254
		T01			TO6 TO7			
		0	0 59	0 11	31 0	0 0	0	
•		Tii			T16 T17	0 0	0	
			0 32	<u>32 0</u>				
	NGLE SUPF	ORT DA	<u> </u>	DATA	AND INT	FULL	SCALE D	ATA
PÑ	IT ALPHA	PSI	L/Q	D/Q	PM/Q	YZQ	RM/Q	YM/Q
	1 0.25	0.00	-3.309	10.400	51+39	. 4,613		≈134.02
	2 -1.74	0.00	-9.175	10.781	68+49	4 * 641		4136+34
	3 =3.75		=14.504	11.372				•135·19
_ (4 =5.79	0.00	=19.872	12.438		4 • C51		4133.46
٠.	5 =7.77		=24.582	13.576	113.38	3 • 8 4 0		≈131 •20
	6 =9.72	0.00	=27.255	15.351	96.80			<u> </u>
	7 -11.77		-31.846	17.093				=140.73 =148.58
	8 -13.76		=36.409	.18.746	92.61	3:471	and the same decreases of	=156*02
	9 *14 * 76	0.00	=38.097 =3.076	19.631 10.320				-134+34
	0 2 2 5	0.00	2.433	10.320				-135.11
	2 4 25	0.00	7.754	10.305				-136.27
	3 6.24	0.00	12.824	10.559				-136.59
그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그 그	4 8.25					7 7		3 ≈135 •91
	10.25	0.00	and the first of the second	10.00		5 • 186		=141.07
<u> </u>	6 12 24	0.00						3 =140.57
	17 .14 .27	0.00	30.694	15.049				3 =129.91
	18 16 24	0.00	33.682					5 =129 ⋅86
	18.26	0.00						5 ≈ 137 •63
	20.27		20.017					3 =142.13

0.00 39.917 21.716 -47.58 5.112

10.399

24 . 624 = 75 . 00

27 . 770 -102 . 40

29 • 652 = 118 • 49

50 - 04

20

21

22

23

20.27

22:27

.24.27

25 . 24

0.24

0.00

0.00

0.00

0.00

43.523

46.251

48.326

-3.076

			ing the second		some active met had	NICL SECT	r .400	र ४४ मा अवस्थितसम्बद्धाः व्यक्तिस्या	
· .	The state of the s	Λαυι	וחו בחו	N SPEED	WIND TUN	MEL LESI			رېږىيى ئىگەرىتى ئىسىدىن ئېرىدىلەپ كەكىلەپ د
				MIND A	XES				
		RUN 73			11/20/81	0933		RUN	.73
•		•	TEMP	85•			P8 14+6	562	
		GPSF 75	•00	VFPs 25	7.91	RNFT 151	.6390•	MACH O	2254
			TOI	TO2 TO3			TOS TOS	T10	
			0	0 32	0 11	31 0	0 0	0	
			T11		T14 T15	T16 T17	T18 T19	T20	
	SIN	IGLE SUPPO	COR RT DAI	RECTED F	ER TARE	AND INTE	RFERENCE	EFFECT SCALE D	S ATA
	PNT	T ALPHA	PŞI	L/13	פֿעמ	PM/7	Ϋ́Ϋ́	RM/Q	PMYQ
		0.25 -1.74 -3.75		-8.642	6,633 7,048 7,745	61 . 86	5 140 • 4 588 • 4 815	31 • 64	=156 • 15 =155 • 53 =153 • 91
μώ ε ∳ '23	4	+ =5.76 =7.75	0.00	₩19.611 ₩23.234	8.886 10.550	110·18 109·30	· 4 • 465 · 4 • 386	42 • 24 48 • 37	=151:09 =148:62
		5 =9.76 7 =11.74 3 =13.76	0.00	=27.085 =31.924 =37.209	12.237 13.947 15.873	99.01 107.75 118.06	4.131 4.070 4.065	61.46	=157 • 21 =163 • 09 =165 • 70
-		3 14 - 77	0700	-39.512		116.79	. 4.378		=178+90
	1(- 1; 12	2:26	© + 00 O + 00 O + 00	×2,776	6 • 600 6 • 464	41.70 29.77	· 4*\$95	16.94	=155+59. =154+81 =152+61
		6 • 26	0.0.0	8.521 13.459 18.645		21 • 15 15 • 34 17 • 11	· 4 • 819	2.56	=149*42 =145*15
	15	12.24		23.583 27.770	8•416 9•554	21.29 19.71	4.866 4.901	=9*55 =15*54	=145.02 =139.58
41.62	17 18	16.26	0 + 0 0 0 + 0 0	32.040 34.251	11 · 182 13 · 325	11 • 26 7 • 06	5•450	=31:65	4135+95 4132+48
	19 20 21	20.28	0.00 0.00	37.100 40.138	16 • 113	=28 · 83 =62 · 65	3 • 826	×33+38	# 4138+71 3 #142+38 3 #146+57
	22 23	24 • 25 25 • 24	0.00	43.653 47.042 49.053	21 • 486 25 • 060 26 • 679		5.151	=46+84 =50+2;	+ =151 · 90 L =151 · 65
	24	Q.25	0 100	=2.776	6 • 673	43.26		23.5	=155.57

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YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 75

(RUN 75-RUN 10)/ 1.00

COMPANY TO THE PARTY OF THE PAR	MIM	FULL S	CALE DATA	SUP	ED	D				
	PNT	ALPHA	PSI	L/G	D/@	PM/G	SF/0	. RM/G	YM/Q	
i	4	=12.00	=0.75	=34+182	13.914	124 • 73	0.767	6+09	=7.51	
	ž	-10.00	=0.75	=28 + 773		122 85	0.753	U • 15	=10.09	
	<u>ā</u>		=Q+75	-26.010	10.529	145 • 61	0.725	=3.91	=5+37	
	4	-6.QO	-0.75	-21.066	9.406	134 . 84	1 . 135	≈8.51	=9 • 16	, ha
	5	-4.00	-0.75	-15.282	8 • 436	114.61	1.693	=11.71	-10.76	
Communication Communication	6	=2.00	≈ 0+75	-8.918	7.960	90.02	1.699	=12.43	=12.56	
	7	0.00	×0 ∗75	=2.523	7 • 628	69.72	1.729	-11:04	=13+75	
	8	2 + 00	=0 +75	2:424	7:466	59:23	1.802	=12.54	=16.96	
	9	4.00	-0.75	7:056	117.400	54+94	2.117	=14.00		
	10	6.00	-0.75	11.291		49.70	2.379	=14.12	.=23.91	edijis.
	12	8.00	-0.75	15.359	7.735	50.82	2.897	=15.63	=25 • 73	
- 7	12	10.00	-0.75	19+573		51 • 67	2.890	=16.93	=24 * 76	
· \	13	12.00	=0.75	23.343	9.330	45 * 31	2 • 1 4 4	=12 +60	=10 • 97	

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 76

(RUN 76=RUN 10)/ 1.00

WIND	AXES DATA	FULL SC	ALE DATA	SUPPORT TARES REMOVED			E D
PNT	ALPHA PSI	L/Q	D/G	PM/Q	SF/Q	RM/Q	YMZQ
1	=12+00 =0+75	#32∙8#6	13.546	103.66	0.737	2.72	=4.75
ž	-10:00 -0:75	=27.359	12 • 102	95.57	0.718	≡3.75	#4 • 98
8	-8.00 -0.75	=23.757	10.566	106 • 15	0.557	¥4.97	2.20
i es fise. 🐺 i	#6+00 - #0+75	119.234	9.250	104.19	C • 775	.=10.17	0.03
	-4+00 -0+75	-13.548	8.527	85.30	1.261	=14.97	- 4 + 79
6	=2.00 =0.75	-7.542	7 * 861	66.92	1.364	≈14.33	#4.02
7	0.00 =0.75	1.390	7.561	50.23	1.295	=12∗77	= 4 • 49.
8	2 . 00 =0 . 75	3 . 436	7.269	42 • 49	1.214	=12:17	≈5 •78
9	4 • DO =0 • 7 5		7.234	40.30	1.461	*12.54	≈9•38°
10	6.50 =0.75		7.338	37.32	1.651	-11.47	=9.51
11	8.00 -0.75		7.766	38 • 65	2 • 127	=11.87	=10.53
12	10.00 =0.75		8.272	45+96	2.289	=14.60	=11+64
13	12.00 -0.75		5 • 436	55.90	1.548	=9.86	=6.19

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 77

(RUN 77=RUN 10)/ 1+00

					FULL SC		SUPPORT TARES HEMOVED			
-		PNT	ALPHA	PSI	, L/G	0/0	PM/G	SF/Q	Rm/Q	YM/Q
			#12+Q0	0+04	=16:021	8 • 4 9 0	-105.00	4 = 20	U • 59	12.80
		2	=10.00	0+04	=11.025	7 • 439	=485 • 89 =179 • 62	=1.532 =1.206	±5.94	8.94
· · · · · · · · · · · · · · · · · · ·		3	-8·00	0.04	-7.424		-163.72	-0.910	#3.30	9.7%
	4 3	4	=6 • C0	0.04	-3.829	6.291	=146 . 69	-0.097	-7.21	2+84
		5	₩4.00	0.04	-0.555	5 . 966	-129 + 45	0.627	-10.98	=1.44
	1978	6	=5.00	0.04	3 • 456	5.767	-1G7.50	0.764	=9.75	■0+76
		7	0.00	0+04	7.240	5.862	-87.70	0.662	= 9 , 1 5	0 • 88
		8	5.00	Q + Q 4	10.548	5 • 834	=66 ∗71	0.568	≖7.69	2.47
1.1		9	4.00	0.04	13.406	5 • 995	=45.57	0.792	=10.28	-0+89
. A "	**,	10	6.00	0.04	16.214	6.208	-23.51	0.974	#8.78	-0.65
		11	8 • 00	0.04	19.094	6 . 702	-3.18	1.404	-9.98	-0.58
~ ~		12	10.00	0.04	22.256	7,383	18.99	1.824	=13.28	-0.68
		13	12.00	0+04	24 + 842	8 • 320	40.17	1.503	=9 +41	4 • 08

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AQUELL TEST SEED MINGLIFFE TEST SESO

DELTA DATA

ID.NO. 78

(RUN 78=RUN 10)/ 1+00

CHI E CHINNA	WIN	WIND AXES DATA		FULL SCALE DATA		SUF	D		
· · · · · · · · · · · · · · · · · · ·	PNT	ALPHA	PSI	L/Q	D/Q	PM/G	SF/Q	RM/G	YM/Q
	1	=12.00	0.06	=33.049	13 • 228	113.08	=1.133	U • 56	7 • 81
	2	=10 + CO	0.06	-27.774	11.609	99.89	-1.056	≠ 5+08	8 • 55
	3	#8 • 00	0.06	-23.813	10.003	106.86	=0.418	-3.58	7 + 03
		~6.00	0.06	-19.195	8 • 8 4 7	102.20	0 . 404	#8+15	1.91
	5	=4+00	0+06	-13:283	7 • 985	82.08	1.007	=9.72	=3 *13
#3 *******************	6	=2.00	0.06	-7.478	7 • 424	65.82	1.061	=10.03	=1.05
	7	0 + 0 0	0+04	=1.556	7 • 095	50.58	0.895	-9.52	1.58
	8	2.00	0.06	3.563	6 • 800	44.27	0.800	≠9•11	0.59
**************	9	4 . 00	0.06	8.065	6.833	40.52	0.866	=1U.82	0.56
	10	6.00	0.06	12.311	6 • 871	38.95	1.103	≠9. 56	0.31
,	11	and the same of th		16.426	7.235	40.29	1.431	≈9.64	1+94
(12		0.06	20.291	7.910	46.38	1.823	=12.42	0.49
	13	12.00		23.051	8 • 863	57.91	1.430	=7.11	5 • 1 4

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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 79

(RUN 79=RUN 10)/ 1.00

11/20/81 1438

	WIND AXES	FULL S	CALE DATA	SUP	ED	ED			
d Himburatan	PNY ALPI	A PSI	١/٩ ,	D/Q	PM/Q	SF/Q	RM/Q	YM/Q	en A
	1 =12.0	,		13.395	170 - 85	-0.400	3.32	*1 ·53	
1	2 =10 × (=29·379 =26·127	11.766 10.114	163.64	-0.598 0.134	#2.42 #1.90	=1,43 =1,05	
	4 =6•(5 =4•(0.01	-21.097 -15.249	8 • 575	133.63 112.61	0.714	*4.34 *7.24	-7·41 -12·62	
A	6 =2•	00 0.03	=8.942	7 • 561	89.27	1.568	*6.29	=11.21	
	7 0+0 8 2+0			7 + 265 <i>6</i> + 966	68+32 61+60	1.299 1.248	≈6.61 ≈6.82,	=10 • 17 =12 • 11	
In the second se	9 4.4 10 6.4	00 : =0 = 01 00 : =0 • 01		6•900 7•071	55 • 66 50 • 95	1.466	=10.60 =9.75	=13.75 =13.16	
1	11 8•0	00 -0.01	15.768	7 • 433	50.96	2.027	-10.04	-11:22	
1	12 10 · 6 13 12 · 6			8 • 038 9 • 058	51.50 47.89	2.122	=12.01 =3.89	=7.45 =1.82	, ,

YOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630

DELTA DATA

ID.NO. 80

IRUN 80 HUN 101/ 1-00

	WINC	AXES	ATA	FULL SC	ALE DATA	SUP	PORT TAR	ES .KEMO	/ED	5
in a malar to the first	PNT	ALPHA	PSI	L/G	D/G	PM/G	8F/Q	. RH/B	YM/Q	
	1	m12.00	0.01	=33 +967	13+684	130.03	5.447	63.51	=153.01	
	2	#10.00	0 . 01	=29.204	12.265	127 . 84	5.035	51.89	m151 • 66	
	3	-8.00	- 0.01	-26.216	10.555	147.90	5.724	45.39	#159+35	-
	4	#6+00	0.01	m21 - 198	9.422	137 - 81	6.377	36.13	-162+26	
	5	-4-00	0.01	-15.382	8.529	117.26	6.853	27.62	-163.01	. 1
	6	≈2.00	0.01	≈8.938	7.995	92.25	6.892	. 21.40	=161 943	-
	7	₩0+00	0.01	#2 •556	7.730	71.79	6 . 4 6 4	15.85	-157 ·92	
	8	2.00	0 . 0 1,	2.596	7 . 567	61.99	6.307		=154 ×22	
	9	4+00	0.01	7:190	7.401	55.84	6.234		-148+29	error (Wingsoff
	10	6.00	0.01	114470	7.573	50.65	6.240		-1-2-38	
	11	8.00	0.01	15.693	7 • 968	52.00	6.631		-139-92	
باعيبسيتن	12	10.00	0.01	19.832	8 + 497	53+04	6.868		=138+90	, , , , , , , , , , , , , , , , , , ,
	13	12.00	0.01	23.580	9 • 459	48.20	5.695	=15.41		
						•				

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ID.NO. 81)	630	TEST	JNNEL	יד כ	WINE	SPEE	LOW	OUGHT	٧			(
RUN 81=RUN 10 1:00 11/20/81 1498 1498 1498 1498 1498 1498		MANAGE SPANS		······································	71-00-104-127-1-12-12-12-12-12-12-12-12-12-12-12-12-1	1. 24. 24. Av.		1	DATA	DELTA	the state of the s	aran kepada di akel ik ke lebira				
### ### ##############################	No. of Control of Cont	Jespinsery	er, a mark de des services	erikaniana de Manerika de K	-	Para destructiva programa de la composición del composición de la composición de la composición del composición de la co			. 81	ID, NO	Sign	-		g n(m		TO PARTITION
WIND AXES DAYA FULL SCALE DAYA SUPPORT YARES NEMBVEL PNT ALPHA PSX L/9 D/9 PM/9 SE/9 RM/9 1 #12.00 0.01 #16.007 8.708 #182.22 5.170 59.61 # 2 #10.00 0.01 #11.189 7.884 #174.82 5.260 46.68 # 3 #8.00 0.01 7.442 7.128 #174.82 5.260 46.68 # 4 #6.00 0.01 -3.888 6.575 -138.05 6.199 31.41 # 5 -4.00 0.01 -0.542 6.334 #121.24 6.589 24.16 # 6 #2.00 0.01 9.10 6.199 #103.00 6.592 18.51 # 7 0.00 0.01 6.840 6.229 #85.60 6.281 13.20 # 8 2.00 0.01 10.031 6.267 #64.79 5.887 7.82 # 9 4.00 0.01 10.031 6.267 #64.79 5.887 7.82 # 10 6.00 0.01 15.798 6.672 #21.44 5.637 #3.27 # 11 8.00 0.01 18.743 7.133 =0.32 6.094 #10.61 # 12 10.00 0.01 24.118 8.725 43.64 5.521 #16.10 #	and the second of the second	X		**************************************	index or the	00	1/_1	10	RUN	N 81	(RU		e de la composition della com	Value (100) la comb e	and the second s	*11719
PNT ALPHA PSI L/9 D/9 PH/9 SE/9 RM/9 1 *12*00 0*01 *16*007 8*708 *182*22 5*170 59*61 * 2 *10*00 0*01 *11*189 7*884 *174*82 5*1260 46*68 * 3 *8*00 0*01 *7*482 7*128 *157*16 5*558 40*77 * 4 *6*00 0*01 *3*88 6*575 *138*06 6*199 31**1 * 5 **00 0*01 *0*582 6*334 *121*24 6*592 18*51 * 7 0*00 0*01 3*110 6*199 *103*00 6*592 18*51 * 7 0*00 0*01 5*840 6*229 *85*60 6*281 13*20 * 8 2*00 0*01 10*091 6*267 *64*79 5*887 7*82 * 9 4*00 0*01 12*940 6*365 **43*01 5*702 0**5* 10 6*00 0*01 15*798 6*365 **43*01 5*702 0**5* 11 8*00 0*01 18*743 7*133 **0*32 6*0.924 **10*61 12 10*00 0*01 21*774 7*809 21*44 6*488 **18*07 ** 13 12*00 0*01 24*118 8*725 43*64 5*521 **16*10 ** ***10 **10 **10 **10 **10 **10 *								8	1,43	/20/81	11			•		
1 = 12.00)	JVE	.KEMO	TARE	ORT	SUPP	4	TAC	ALE	ULL S	F	AYA	AXES (WIND		<u>Carrisons (an</u>
2 =10.00	YM/Q	M. Sangaran Spilan	RM/Q	<u> </u>	_SEZ)	PH/0	<u> </u>	0/0	L/0		PSI	ALPHA	PNT	n kun ana ana ana ana ana ana ana ana ana a	And parties and pro-
3 =8.00																
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5 -4.00 0.01 -0.542 6.334 -121.24 6.533 2+.16 = 6 -2.00 0.01 3.110 6.1393 -103.00 6.592 18.51 = 7 0.00 0.01 6.840 6.223 -85.60 6.281 13.20 = 8 2.00 0.01 10.031 6.267 -64.79 5.887 7.82 = 9 4.00 0.01 12.940 6.365 -43.01 5.702 0.45 = 10 6.00 0.01 15.793 6.672 -21.44 5.637 +3.27 = 11 8.00 0.01 15.743 7.133 -0.32 6.094 -10.61 = 12 10.00 0.01 21.774 7.805 21.49 6.438 -18.07 = 13 12.00 0.01 24.118 8.725 43.64 5.521 -16.10 =													***	J.		
6 #2+00 0+01 3+10 6+199 #103+00 6+592 18+51 #7 0+00 0+01 6+840 6+229 #85+60 6+281 13+20 #82+00 0+01 10+091 6+267 #64+79 5+887 7+82 #9 4+00 0+01 12+940 6+365 -+39+01 5+702 0+49 #10 6+00 0+01 15+798 6+672 -21+44 5+637 #3+27 #11 8+00 0+01 18+743 7+133 -0+32 6+694 #10+61 #12 10+00 0+01 24+118 8+725 43+64 5+521 #16+10 #13 12+00 0+01 24+118 8+725 43+64 5+521 #16+10 #16+														5		
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D AXES DATA	FULL SCALE	DATA SUPP	ORT TARES HEMOV	ED
ALPHA PSI	. L/8 p)/G PM/G	SF/Q RM/Q	YM/G
				=181+90
				=189.50 =178.48
#6+00 0+01	-44.183 S			=169.00
				*165*49
			·	=150 •69
			* * * * * * * * * * * * * * * * * * *	=144*02
4.00 0.01	-0.207 4		5.536 0.01	=136+45
		.434 =28.25	5.265 -4.01	
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VOUGHT !	LOW	SPEED	WIND	TUNNEL	TEST	630
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DELTA DATA

ID.NO. 83

IRUN 83-RUN 10)/ 1+00

	HIND	AXES D	ATA	FULL SC	ALE DATA	SUPI	PORT TAR	ES REMO	/ED	
	PNT	ALPHA	PSI	LV0	D/G	PM/Q	SF/Q	RM/Q	YMZQ	· · · · · · · · · · · · · · · · · · ·
	1	#12.00	003	= 26∗593	11.509	161 • 81	6,468	79+40	#185+04	
	2	-10:00	: 0 • 0 3	#24 • 536	10.269	154.90	6.586	62.20	=179×33	
	3	-8+00	0.01	-23.474	9 • 117	158.94	6.531	52.50	-171+29	
	4	-6.00	0.01	-21-645	7.931	152-15	6.698	40.40	-167.85	7
	. 5	-4+00	0.01	=17,855	7.232	122.70	6.773	28.26	-166.76	
٠	6	=2.00	0.01	=13.949	6 • 691	88.28	6.594	. 22.35	=160+14	
	7	0.00	0.02	=10.526	6 • 1.94	60 • 18	6.328	. 15.50	=155.79	
	8	2.00	0.03	#6+969	5 • 7.34	33.47	6.200	8.29	=151.75	
	. 5	4+00	0.03	#3.683	5.503	11.70	6.003	1,06	-145.79	***************************************
	10	6.00	0+03	-0.468	5.299	-10.34	5.965	-5.30	-144+86	
	11	8.00	0.03	2.576	5 • 157	-32 *05	5.864	*9.33	-142 -55	
47,100,000	12	10.00	0.03	6 • 1.78	5.202	=55.64	6.332	-17.12	=146.37	
	13	12.00	0.02	9.763	5 • 5 6 4	=80.20	6.316	=19.14	-149.95	

VOUGHT	IPW	SPECD	MIND	THNNFI	TEST	630
YOUGH!	W + 15	71 EEU	M TIAM	TOMMER	(C 3)	030

DELTA DATA

10.NO. 84

.(RUN 84=RUN 10)/ 1+00

	WIN	D AXES I	DATA	FULL SCALE DATA SUPPORT TARES HEMOVED						
	PNT	ALPHA	PSI	. L/Q	p/G	PM/Q	SF/Q	RM/Q	YM/Q	÷.
	Ĺ	#12+00	.0.02	=6.33 <u>1</u>	6 • 232	=164.57	=1.664	5 • 53	3.21	
	ج	4 - 4 -	0.02	=5.515	5 . 7.22	=153 ∗33	=1.098	0.61	-3.18_	
	3			-4-671	5.317	=140+34	-0.522	0.37	-3-22	
	I I	-6+00	-0.02	·=3.950	4+895	H124-92	0.013	#3.61	-7.34	
	5		0.02	:-3.261	4 + 665	-107.91	0.434	-6.92	.=11*09	
	6	=2.00	0 • 02	-2.619	4 • 495	-92.20	0.529	7.29	-7+94	
	7	0.00	0.02	=1.903	4.329	#75·49	0.396	-6 ±85	# 5 ∗73	
	ģ	2.00	0 • 02	#0.948	4 + 167	=59+09	0.366	×7.25	· =4 • 15	
***	9			-0-173	4.067	#43.30	0.235		-3.35	
	10			0.688	3.999	-26.76	0.099	1.6	#1.00	
	11		200	1.595	3.969	-12.76	-0.002	1. 75 (4) 27 (2) 27 (4) 5 (2.5) 49	1.03	
	12			2 • 424	. 4 . 067	2 + 54	0.155		-0.18	
N	13	1.9 1.5		3 • 335	4.265	20.66	0.023		#D#04	
									**	· ,

VOUGHT	LOW	SPEED	WYND	TUNNEL	TEST	630
4000111	— — D.	E E U	M T I I	I WITH L	I E O I	930

DELTA DATA

.10.No. 85

MRUN 85-RUN 101/ 1+00

	WIND AXES DATA			FULL SC	/ED				
ا	PNT	ALPHA	PSI	. L/O	0/0	PM/Q	SF/Q	RM/Q	YM/Q
	1:	=12.00	.0.02	#6 • 742	6 + 9 4 6	≒155 +09	6.264	73.89	=184+49
	2	=10.00	0+02	-5.778	6.350	=143.62	7.087	61.39	=192+10
	3	-8.00	0 402	4.879	5.920	=136+30	7.052	. 52.37	-182×53
	4	-6+00	0.02	-4.045	5 . 627	-122.88	6.954	40.02	-173.76
t t	5	-4.00	0.02	-3.29g	5.399	-106@15	6.926	. 28.49	
	6	-2.00	0.02	-2.590	5 • 165		6.756	. 20.29	=163+13
	7	=0.00	0.02	=1.902	5 • 129	= 75 ⋅ 23	6.131	15.73	=153×33
	8	2.00	0.02	=0 a 945	4.916	=60+01	5.817	7.71	=146.96
TO THE PERSON NAMED IN	9	4.00	0.02	-0.145	4 + 834	=44.16	5.525	1.01	-140.38
	10	6.00	0.02	0.703	4 . 668	-29-14	5.298	#3.54	=137+92
	11	8.00	0.02	4.457	4.735	-13.25	5.297	-7.51	-137 +99
	12	10.00	9.02	. 2.340	4 • 835	4+26	5.627	=15.32	=143*13
	13	12.00	.0.02	3.168	4.992	19.51	5 • 649	-16.35	
								•	¥ . •

DELTA DATA

ID.NO. 86

(RUN 86=RUN 10)/ 1+00

WIND	AXES	DATA	FULL S	CALE DAT	A SUPI	PORT TAR	ES .HEMO	VED
PNT	ALPHA	PSI	. L/O.	p/g	PM/G	SF/Q	RM/Q	Ym/Q
1	-12.00	0 402	-15.252	9 • 0 6 4	=183+84	4.668	58+94	=148+24
2	=10:00	20.0	-10.821	8 • 274	=176.92	4.957	48.85	=149*92
	₩8.00	0.02	-6.979	7 * 380	-161.29	5.084	41.42	=148 ×03
	-4.00	0.02	-3.547	7.026	-142.87	5.735	33.22	-154-64
	-4+00	0.02	0 - 144	5.700	-124.21	6.260	23.50	-157.69
6	=2.00	0.02	3.700			6.258	. 18+04	=157•26
7	0.00	0.02	7.507			6.028	13,25	=152 .52
8	2 + 00		10:779			5.702	8.38	=146:30
	4.00	0.02	13.607			5.435	2.12	-140.00
	6.00		16.150		-23.72	5.587	×3.58	#134 · 80
	8.00		77 Y			6.027		-132.51
12	10.00		.22 • 351		19+49	6.433		=132.01
13	12:00		24.359		40,99	5.651	=15.76	

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				DELTA	DATA	, , , , , , , , , , , , , , , , , , , ,			
				ID.NO	• 87	······································	···· ·································	aga ga malagaga ya masa ka ka	
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				11/20/81	1438				
en garage	WINI	D AXES DA	TA	FULL SC	ALE DATA	SUP	PORT TAP	RES .REMOVE	D .
en e	PNT	ALPHA	PSI	. L/G	0/0	PM/Q	SF/Q	: Rm/Q	YM/Q
	: 1 2	#12+00 #10+00	0 .00		13+558 11+854	106+46 98+36	=1.619 =1.190	6 • 26 #1 • 56	7+04 2+79
77 77 	3	-8.00	0.00	=23.534	10.340	102.73	=0.802	-U.O2	3.67
- 1 - 10 - 1		#6+00 #4+00	0.00		9.055	100.92 81.57	0.113	*4.73 ·	=0+73 =6+57
- 18 1-181 - 184	5	#2·00	0.00	=7.075	8 • 236 7 • 712	63.05	0.540	=8+24	-3.41
	7	0.00	0.00	=1.022	7 • 430	47 • 92	0.543	≅8.€39 •	* 4 • 87
	<u> </u>	2 • 0 0 4 • 0 0	0 • 0 0	3.902 8.201	7 • 135	41.49	0.302	=7.01	=3+12 =4+90
	10	6.00	0.00	12.412	7.204	98+97 : 36+08	0.510	•7•64 •7•97	=4.64
uncer) e	11	8 • 00	0.00	16.668	7.567	37+75	1.274	9.71	-4.13
(12 13	10.00	0 + 0 0	20•594 23•640	8 • 275 9 • 125	44•73 57•19	1.565	#12.16 #6.13	#2•67 1#39
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	gaster til skiper det i det skiper som			المراجع والمراجع والم	i a kanagaan				
ng pangkabilang spanson ng mangkabilan	······································	·						······································	
							•		
	<u> </u>			iliteration and a second and a s		·			nanaki ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '
	•								

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A-182

BUGHT LOW SPEED WIND TUNKEL TEST 630

DELTA DATA

ID.NO. 88

IRUN 88-RUN 10)/ 1-00

······································	NIN	D AXES D	ATA	FULL S	CALE DATA	SUP	PORT TAR	ES HEMOV	ΕD
In the second	PNT	ALPHA	PSI	L/Q	D/Q	PM/G	SF/Q	Rm/Q	YM/G
	1	#12.00	- #0 + 01	=33.882	16.701	98+84	=1.432	2.43	9.01
	2	=10.00	#0 + 01	=28.525	15.105	98 + 86	=1.115	· #0+90	8:01
THE PARTY OF THE P	3	-8-00	0.00	-23.870	13.739	99.91	-0.568	-0.29	6 + 03
1	→	-6+00	0.01	=19.064	12.549	100.38	0.404	5.82	-2.65
	5	-4.00	0.01	-13:250	11.772	83.08	0.994	-10-08	-8.28
	6	-2.00	0.01	*=ブ・4フフ	11.395	69.17	1.096	■9.32	=6 .22
	7	0 + 0 0	=0.01	■1.456	11+195	55.31	0.921	≈8.31	=4.45
	8	2.00	-0.01	3.468	10.902	50 • 78	0.768	=7.27	* #4 #OB
	9	4+00	-U.01	7.965	10 834	48 • 65	0.997	-7.81	=6.48
	40	6+00	-0.01	the state of the s	10.934	44.06	1.330	=7.09	=4.70
P	11	3 - 3. than 12 3 3 4	4.4	16.334	11+399	47.06	1.893	#9.06	. =4+17
	12		· =0.01	20.409	12+071	54.32	2.156	=11.62	- =4.62
••	13		1. 1	23,397	13.030	66.70	1.584	-6.03	0 +22
									*

ORIGINAL PAGE IS OF POOR QUALITY.

A-183

VOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630
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DELTA DATA

ID.NO. 89

(RUN 89=RUN 10)/ 1.00

WIND AXES DATA			FULL SC	CALE DATA	SUPPORT TARES REMOVED			/ED	1: 1:	
adagan ni in atau na aga na na atau na ana ana ana ana ana ana ana ana an	PNT	ALPHA	PSI	. L/Q	0/0	PM/G	SF/0	RM/Q	YM/Q	
	1:	=12.00		=34.212	16+777	111.88	-0.852	5.73	3,17	
	2	=10 • 00	-0.01		15+384	148.38	=0.637	1.03	0.434	
	3	-8.00			13.867	135.87	-0.115	0 - 44	-0.75	
	4.	-6.00	* #0.01	#21 · 101	12,774	127.43	0.644	#1.61	-7.39	
	5	-4+00	. #0.01	m15.349	12.036	114.77	1.324	-6.77	-14.36	1 .
(<u>Crishpostica) </u>	6	₩2.00	- WU.01	#8 • 875	11.562	91 . 65	1.628	=6.46	=14 487	
	7	0.00	0.01	= 2.769	11:357	75.10	1.365	#5 •68	.×14+39	
	8	2 . 00	· =0.01	2 • 473	11.124	67 • 18	1.531	=6.62	.=18.06	
N	9	4.00	=0.01	7.050	11.033	63.69	1,766	-7.91	-19.15	****
	10	6.00	-0.01	11.421		59.28	2.233	-8.16	-18.50	
	11	8.00	-0.01	15.734	11.533	59.90	2.627	+9.99	-17+14	## .
	12	10.00	-0.01	20.181	12 • 171	59 + 88	2.755	-12.76	=13.94	
`	13	12.00	- =0.01	24.497	13 • 131	56.77	1.821	≈5.31	-6.09	

ORIGINAL PAGE 13 OF POOR QUALITY

A-184

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 90

(RUN 90-RUN 10)/ 1+00

	WIND	WIND AXES DATA			CALE DATA	SUF	PORT TAR	ES : KEMOV	ED
	PNT	ALPHA	PSI	. L/G	D/G	PM/Q	SF/Q	ŔM/Q	YMZQ
	1	-12.00	#0 . O.1	=33∙9 06	13.613	126+03	=0+7.62	5 • 41	=3.36
	2	=10.90	· =0.01	=29.211	12+089	121.96	=0.853	0.02	-0.45
	3	#8+00	-0.01	-25.846	10.637	136.20	-0.322	0.31	· -2×13
	•	-6+00	0.01	-20.763	9.342	130.20	0.312	-1.25	=6.52
	5	-4.00	-0.01	-14-875	8 • 491	109.77	1.127	-6.63	×13.25
anaman kapadata - Kanada Kanada an k ababah	6	=2·00		-8·509	7,927	85+22	1,203	#5.90	=14+34
	7	0.00	=0.01	.=2.422	7 • 628	64.88	1.062	=6.78	-12.21
	8	2.00	-0.01	2.730	7.334	56.79	1.133	₹6÷55	=15.63
	9	*•00	-0.01	7.337	7.300	52.70	1.200	* =7.14	-17:15
	10	6.00	-0.01	11.521	7.303	48.22	1.633	#7.88	16.30
	11	8.00	-0.01	15.900		48:67	1.961	-1U.06	-15.98
المنطق المنطق المنطق المنطقة ا	12	10.00	and the second second second	20.312	8 * 417	· 47 • 20	2.057	-12.09	=11+98
	13	12+00		24.063	5.297	42.39	1.550	=7.36	=4.16
•				* *			7		•

(Particular)		•	/ GUGHT	LOW SPEED	WIND TU	NNEL TES	T 630		
		2 - 1887 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	<u> </u>	DELTA	DATA		angan and a jump dangan 3 7 yakin asinda n		ti i, ma_{ni y}a adan iya iyangan
				IQ.Ne	91	and the second s	······································	——————————————————————————————————————	
				RUN 91	RUN 101	/ 1.00			
		·		C0/20/81	1438				
√	WIN	D AXES	ATA	FULL SC	ALE DATA	SUP	PORT TAR	RES REMO	VED
in de la company <u>Jamain de la company de la</u>	PNT	ALPHA	PSI	L/G	0/0	PM/G	SF/Q	RM/Q	YMZ
	1.	#12:00	=0.01	#33 • 9 4 4	13+945	:126 •82	5.504		=158.51
	3		-0.01	#26 · 037	10.885	124.75	5.498	48,20	=158.96 =158.77
	4	-6+00		-20.859 -14.812	9 • 777 8 • 763	135.03	6.501	38.23	=166 ×89 =167 +81
<u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>	5		-0.01 -0.01		8.325	91.12	6.929		=164:42
	7		- mo.01	#2.289	8 • 023	70.30	6.803	16.19	=161 •22
	8		- #0 · D1			61 + 45	6.532		=157.09
	9 10		-0.01 -0.01		7•734 7•613	53+99 48+79	6.403		=151.07 =144.71
	11	8.00	#O.01		8 • 199	50.39	6.761		-142.63
(12	10:00	· MO . 01	19+847	8 • 738	50,54	7.243	≈18 • 78	=146.21
,	13	12+00	· #0*01	23.929	9.763	46+5F	6 + 584	■18.78	≈137 •78
		AND THE				3			
en de la companya de La companya de la co			Januari and a state and a state of the sta						
. Year									
	i ka ji samada sika sa ka ji			·		· · · · · · · · · · · · · · · · · · ·			
4	\$ \$2.	.*					44 (4) (4) (4)		•
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					·	* • .			
						in the second second	yr Tagailte	e de la companya de l	
<u> </u>			 		 	ana di kalendara di	<u></u>	y anaktaranya ya<u>in</u>ayi ana kata	- Carana - Lind Corana - Lind Corana - Lind Corana

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A-186

WOUGHT LO	W SPEED	WYND	TUNNEL	TEST	630
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DELTA DATA

10,NO. 92

(RUN 92=RUN 10)/ 1+00

WIN	D AXES DATA	FULL SC	FULL SCALE DATA SUPPORT TARES REMOVED						
PNT	ALPHA PSI	. L/G	D/G	PM/G	SF/G	RH/Q	YM/Q		
. 1	#12 00 O40	1 =33.952	16+951	117:00	4.722	. 60,57	≈138 €62		
	#10.00 0.0	1 =29.347	15.730	118 • 16	4.905	48.13	=138.35		
3	-8.00 040	1 -26.169	13+957	138+28	5.450	49.40	-143653		
julia filozofi (1904) 🛊	-6.00 0.0	11 -21.098	13 - 155	131.48	5.979	32.66	-148.39		
5	-4.00 0.0	1 -15.316	12.436	118+24	5.426	: 21.53	-159+00		
6	=2.00 O.C	14 =8.840	11.955	95.87	6,292	. 17.66	=145 · 00		
7	0.00 0.0	1 =2.822	11.683	78.56	6.149	12.35	=141+24		
	2400 040	1 . 2.330	11.567	70.01	5.880	6 + 47	≒135 +96		
9	4.00 040	7.110	11:499	65.23	5.568	0.04	=132.47		
10	6.00 0.0	1 11.419	11:602	62.20	6.347	· =5.13	#133.90		
11	8 • 00 D • 0	15 449	11.901	61.73	6.840	-11.13	=133×38		
(12	10.00 0.0	19.955	12.666	62.39	7:389	-20-04	4139.82		
13		23.719	13.455	58+44	6.655	=17.23			

DELTA DATA

10.NO. 93

(RUN 93-RUN 10)/ 1+00

WIND AXES DATA			FULL S	ALE DATA	SUPPORT TARES .KEMOVED					
·.		PNT	ALPHA	PSI	. L/Q	D/Q	PM/Q	SF/Q	RH/Q	YM/Q
		1	=12.00	0.01	433,831	17.397	113.62	4.668	59.79	=137+16
		2	=10.00	0.01	=29.552	15.876	131.56	4.828	47.48	=139 •35
		3	-8.00	0.01	-25.925	14/301	137.37	5.251	40.62	-141+67
	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-6.00	0.01	-20-768	13.301	130 - 17	5.794	31.68	m146+16
		5	-4+00	.0 .01	-15.082	12 • 636	114.36	6.193		-143 - 87
		6	-2.00	0.01	.=8.509	12 • 193	93.56	6.094		≈139 e69
		7	0 + 00	0.01	:=2.522	12.008	76+84	5.968	. 11 . 47	
		8	2.00	0.01	2 • 623	11.786	69,20	5.700	5.98	
		9	4.00		7.131	11.616	64.59	5.799	0.39	≈ \$33+39
		10	6.00	0.01	11.468	11.805	60-12	6.150	-5.39	-129.76
. ÷		11	8.00		15.593	12 - 135	60.25	6.731		=131.45
		12	10.00	سيها أنسان فسيراح أبير برود فلسنتين التد	20.022	12.833	60.50	7.323		≈136÷3 0
		13	12.00		23 • 829	13+770	56 + 57	6.451	=16.89	
		- 		· * *		4-11-	" • /		man and a state	

DELTA DATA

10.NO. 94

IRUN 94-RUN 10)/ 1.00

Control of Picting and Property	eriore de la composition della	HIND	AXES DATA		FULL SC	FULL SCALE DATA SUPPORT TARES KEMOVED				
	ارد المراجعة المحمودة الم	PNT	ALPHA	PSI	, L/Q	p/q	PM/Q	SF/G	RH/Q	YM/Q
		1	m12#00	0.01	#33.812	17.+270	114:07	4,935	. 64.47	=145.07
		·	#10.00	0.01	#29·215	15.945	115.43	5.152	: 52.77	=148+74
		3	48.00	0.01	-26.024	14.345	1,33 • 83	5.621	· 46.01	-151:07
<i>31</i> (4)	5 B	4	m6 . 00	0.01	-20.899	13.387	127 • 28	6.130	35.86	
		5	-4.00	0.01	=15.177	12.596	114.44	6.460		-154.08
		6	#2.00	0.01	=8.740	12,229	92.08	6.518		=150 • 40
		7	0 + 00	0.១1	=2.624	12:097	74+72	6.199	13.98	=147.78
		8	5.00	0.01	2 * 651	11.802	69:27	6.042	7 • 86	=143 - 40
**************************************		9	4.00	0.01	7 - 191	11.668	63.47	6.067	0.81	
		10	6.00	0.01	11.387	11.836	60.12	6.408	#4.25	-137+94
		11	8 00	0.01	15.668	12.134	60.95	7.059	=10.08	=139+92
		12	10.00	0.01	20.048	12,909	59.90	7,538	=18.90	-143.46
•		13	12:00	0 . 01	23.947	13:792	55,90	6.588	. ≒16 • 95	=140+25

DELTA DATA

ID. NO. 95

(RUN 95=RUN 6)/ 1.00

WIND	AXES DATA	FULL SCALE	DATA SU	SUPPORT TARES REMOVED				
PNT	ALPHA PSI	L/0 p	/0 PM/0	SF/Q .	RH/Q YM/G			
1	#0+07:=24+00		1.201 0.71		24+99 -265+61			
2	=0+07:=22+00	· 6 • 830 28			24.46 .124.43			
3	₩0.07 . ₩20.00		.001 . 28.13	-41.256 :	27.08 102.06			
4	-0.07 -18.00	3 * 576 22	+205 40 - 16	-36.315	24.61 70.91			
5	#0+07 .#16#00				19.72 . 40.00			
. 6	=0+07 =14+00	1.897 17	. 262 69 . 15	=24.807 .	15.71 10.20			
7	-0.07 -12.00	1.295 15	1.753 63.80	H22.241 .	14:37 =19:00			
8	#G • 07 =10 • 00	0.955 14	1941 70 42	-18.40S	15.71 -41.71			
9	WO.07 -8.00		1.800 72.68		14+26 =68+05			
10	-0+07 -6+00	-1.079 13	+518 82 07		17.36 =97.27			
(° 1	-0.07 -4.00	-1.775 13	1.222 88.53	-2.969	19.79 =115.75			
12	#0.07 · #2.00		0061 91.73		22.32 =130.28			
13	=0.07 0.00	#1.536 13	1+193 89+56		31.49 =140.64			
1.4	=0.07 2.00	=1+656 13	8 468 88 42		26.68 =138.39			
15	-0.07 4.00		1.515 81.70		28.73 4152.96			
16	#0.07 6.00		· 058 72 · 05		31 .48 =195 .78			
17	-0.07 8.00	0.066 14	. 602 58 606		38.99 #211.46			
18	=0.07 10.00		·693 39 ·83		38.55 =225.29			
1,9	=0.07 12.00	2 + 410 16	·807 28 · 02		40.78 =248.23			
20	m0+07. 14+00		14336 16451	35.973	41+78 =275+08			
21	-0.07 16.00		1.910 10.54		38.96 =302.56			
22	-0+07 18+00		-1.04		39,47 =328+13			
23	-0.07 20.00		·743 =6.45		37.90 =359.77			
24	#0.07 . 22.00		7.591 =16.98		38.39 =391.69			
25	m0+07: 24+00		0•572 ⇒32•07		37.73 =415.27			

DELTA DATA

ID.NO. 96

(RUN 96-RUN 6)/ 1.00

	MIND	AXES DATA	FULL SC	ALE PATA	sur	PPORT TAR	RES .KEMO	/ED
	PNT	ALPHA PSI	L/G	D/Q	PM/Q	SF/Q	. RM/Q	YM/Q
**				· .				
	1.	-0.08 -24.00	3.878	31.567		≒50.381	. 21.34	
-	2	-0.08 -55.00	7.•223.	28 • 110	16.27	≈45.803	23.13	117.40
	3	=0.08 :=20.00		26.007	26+71	m44 . 048	29.69	109.77
	4	=0.08 =18.00	4 . 870	23 • 871	37.87	-39.410	. 28.32	82.43
21 · · · · · · · · · · · · · · · · · · ·	5	≈0.08 =16.00	4.001	21.080	49.37	-34 . 68C	. 26.70	50.37
	6	#0+08 #14+00	3.042	18:371	68.29	=29.621	. 20:41	: 21 • 10
	7	=0+08 =12+00	2:379	17:199	62+68	≈25 • 211	17:74	· =3 ×23
	8	#0+08 #10+00	1.590	15.994	71 • 47	=20.572	16.63	=29.02
	9	#0.08 #8.00	0.873	15.060	77 + 41	-15.284	17 - 08	-52.20
	10	-0.08 -6.00	=0 -179	14.427	84 - 70		15.75	·=80+35
- Ti	11	-0.08 -4.00	-0.964	14.247	94 480	-4.843	18.44	-102-43
7	12	=0.08 =2.00	-1.386	14 - 037	10:1.87	=0.338	20.79	
Ne s	13	-0.08 0.00	-1.416	14.337	/97.52	3.584	31.67	=134+9A
	14	-0.08 R.00	=1.687	14 + 458	99.53	8.072	26.60	#138 •13
**************************************	15	-0.08 4.00		14+774	92.46	12.577	. 26.58	-151.25
e distribution	16	-0.08 6.00	-6 Z23	15-121	81.64	17.956		=191+10
	/17	-0.08 8.00	0.180	15.633	68 • 26			-214+39
	18	#0.08 10.00	1.386	1846,86	49 • 44	27. 09	35.54	H228+34
•	19	-0.08 12.00	2.734	17,7526	34 + 54			=249+44
	20·	=0.08 14.00	3 • 6 8 4	18/ 1634	•	31.333	37.59	
	21	-0.08 16.00	4.711	2/0.656	22.84	35.331	38 • 27	=271 •78
		-0.08 18.00	7./11		6.78	39.616	38.86	-296 - 69
*.	22	-0.08 50.00	5.969	22.372	3.93	44.822		-322.46
	53		6.984	25 • 045	-2.02	50.213	. 42+49	
	24			28.012	=14.51	55.572	43.30	=388∗33
	25	#0.08 24.0Q	9.633 }	31 • 121	=26+31	60.434	42+38	-413-10
								
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YOUGHT LOW SPEED WIND TUNNEL TEST	IT 63	ŝЭ	0
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DELTA DATA

ID.NO. 97

(RUN 97=RUN 10)/ 1.00

	MIN	ID AXES	JATA.	FULL SC	ALE DATA	SUP	PORT TAR	ES HEKO	VED	······································
	PNI	ALPHA	PSI	, L/W	D/0	PM/Q	SF/Q	RM/E	YM/q	
	1	-12.00	0.03	#33·811	17 + 424	114.86	7.248		=162,44	
		#8.00	0.03	=29.426 =25.868	15 · 836 14 · 343	127·30 138·38	7.370 \ 7.157	45.33	≈167°45 ≈162•66	
				=20.629 =14.749	13.353	131.65	7+272 7+372	: 28.32	=160÷05 =156•25	44.1
	ě	0.00 #8.00	0.03	=8 * 671 =2 * 522	12.277	93.86		. 22.48 16.22	=145.54	
	8	2:00	0.03	2.733	11/868	69+8 <u>2</u>	6.455 6.348	10.05	=140.55 =137:17	
1.	, 10	6.00	0.03	11.554	17.853	59 • 41	6.447	#3.11	=133.70	
	<u> </u>		0.03	15.801 20.189	11.833	59 • 8 4 60 • 92	7.203	=17.49		
' •	13	12.00	0.03	24.519	13.601	60.70	6.281	=16.78	-141.26	

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A-192

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 98

(RUN 98=RUN 10)/ 1:00

MINC	AXES D	ATA	FULL SC	ALE DATA	SUPF	PORT TAR	ES :KFWG	/ED
PNT	ALPHA	PSI	. L/G	D/G	PM/Q	SF/Q	: RM/0	YMZQ
1	=12+00	€0+0	≈33 +553	17 • 408	115 • 68	6 • 834	57.92	-155.06
2	m10 + 00	0+03	W29 . 491	15.816	123.57	6.985	48.56	=156 ⋅ 67
3	*8 · 00	0.03	-25.847	14.339	136+96	6.844	41.08	#150+44
4	-6.00	0.03	-20.729	13.415	130+16		33.85	-149 -43
5	-4.00	0+03	-14.810	12.762	112.35		: 25.44	=146+53
6	-2.00	0.03	-8.245		93+99		19.90	=139 · 10
7	0.00	0.03	=2 . 38s	12.028	76478		13.70	m137:12
8	2.00	EQ.O	2.696	11.754	68.90			
9	4 00	0.03	7. 284		62+95		0.10	
10	6.00	0.03	11.637	20 101	59.40		=5 +44	=126.78
	8.00	0.03		The state of the s		The state of the s		
	10.00	0.03	20.315					=135.08
13	12.00	0 . 03	24 . 785	13.781	60+16	6.162	=18.09	-137+04
	PNT 12 34 5 6 7 8 9 10 11 12	PNT ALPHA 1 =12.00 2 =10.00 3 =8.00 4 =6.00 5 =4.00 7 0.00 8 2.00 9 4.00 10 6.00 11 8.00 12 10.00	1 =12.00	PNT ALPHA PSI .L/@ 1 =12.00	PNT ALPHA PSI . L/G D/G 1 =12.00	PNT ALPHA PSI L/G D/G PM/G 1 =12.00 0.03 =33.553 17.408 115.68 2 =10.00 0.03 =29.491 15.816 123.57 3 =8.00 0.03 =25.847 14.339 136.96 4 =6.00 0.03 =20.729 13.415 130.16 5 =4.00 0.03 =14.810 12.762 112.35 6 =2.00 0.03 =8.245 12.282 93.99 7 0.00 0.03 =8.245 12.282 93.99 7 0.00 0.03 =2.389 12.028 76.78 8 2.00 0.03 =2.696 11.754 68.90 9 4.00 0.03 =7.284 11.680 62.95 10 6.00 0.03 =1.637 11.806 59.40 11 8.00 0.03 =1.893 12.168 60.25 12 10.00 0.03 =2.315 12.804 62.444	PNT ALPHA PSI .L/G D/G PM/G SF/G 1 =12.00	PNT ALPHA PSI .L/G D/G PM/G SF/G : RM/G 1 =12.00

VOUGHT I	LOW	SPEED	WIND	TUNNEL	TEST	630
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DELTA DATA

ID.NO. 99

MERUN 99-RUN 10)/ 1.00

INC	AXES	DATA	FULL SC	ALE DATA	SUPF	PORT TAR	ES .KEMO	/ED
NT	ALPHA	PSI	. L/G	D/G	PM/Q	SF/Q	. RM/Q	YM/0
1	=12+00	0.03	-26+337	15 • 270	150+03	8 • 135	. 65+40	=176+50
2	#10 · 00	·0.03	-25.213	14.052	151 • 51	8 . 352	: 54.48	-175.91
3	-8.00	0.03	-24.051	13.099	154.51	8.153	44.20	-164-85
4	-6.00	0.03	-21.877	12 • 117	150.61	7.980	: 35.99	-155+44
5	-4.00	0.03	-18.055	11:385	120.86	7,559	: 26.43	-148+33
6	=2.00		=14.224	10.795	91.53	7.163	: 20.84	
7	=0•00	0 . 03	-11.344	10.576	71.39	8 + 823	12.39	=133 <u>22</u>
8	2+00	0 + 03	=7+017	9.932	42+05	6.446		=130.52
9	4.00	0.03	-3.731	9.603	19.59	6.269	-1.68	=130+24
10	6.00	0.03	-0.459	9+397	-0.07	6.266	-6-16	=132×43
11	8.00	and the same of the same	2 . 841	9+303	-82.03	6.197		-135.92
12	10.00		6.099	9.572	=46 - 18	6.921	■17,59	
 13	12.00	0.03	9.750	10+100	≈71 ∗04	6.315	-19.38	4135°495
							-	

ORIGINAL PAGE IS OF POOR QUALITY

A-194

YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 100

(RUN 100=RUN 10)/ 1.00

	WIND	AXES D	ATA	FULL SC	ALE DATA	SUP	PORT TAR	RES REMO	/ED
and the state of t	PNT	ALPHA	PSI	L/8	0/0	PM/G	SF/G	RM/Q	YM/0
	1	=12+00	0+04	w28.563	16+168	177+75	14.324	. 65#41	⊲200 •05
	2	#10:00	0 • 03	426.684	15.022	170.90	14.676	61.93	=202 • 16
	3	-8.00	0.03	-24.360	13.977	157.26	14.304	44.27	=185+30
	4	-6+00	0.03	-21.828	12.873	145.93	13.675	. 33.76	-166794
	5	-4.00			12.043	125.28	12.734		-154+49
nikisida a madasindidapahing di 1764 kanggi<u>nggan</u> Ka_na	6	=2.00	0.03		11.381	101.17	11.632		=139+39
	7	=0.00	0.03	F11+730	10.749	73+06	10.672	9 • 44	
	8	2 . 00	0 + 0 4	-8 - 169	10.234	50.00	9.282	4.66	=125 ·32
	9	4.00	0.04	·a4.538	10.020	. 23.40	8.757	* -3.12	-124.96
	10	6+00	0+04		9 . 853	-0.41	8.546	9:07	-126 - 15
	11	8+00	0+04	. 2.149	9.828	.=22.53	8.298	-13.62	=128+30
7	12	10.00	.0.04	5.632	9 • 8 6 8	-46 - 42	7.915		=129 • 56
V.,	13	12:00	0+04	9 + 196	10.298	=71 • 43	7.282	:=21.21	

ORIGINAL PAGE IS

				of Pi	or quali	* u,	A-1	.95	
(* **:			YOUGHT !	OW SPEED	WIND TU	NNEL TES	T 630		
Managara da araba da manag	· · · · · · · · · · · · · · · · · · ·		سمور _{ان م} ی در برای بازی افغان بر برای به	DELTA	DATA				
representative consistence and the consequence of t	,, , , , , , , , , , , , , , , , , , ,			ID, NO	1. 101				
and the second s	 	a specific control	 	RUN 101-	RUN 10)	/ 1.00		 	
				11/20/81	1438				
	MIND	AXES	DATA	FULL SC	ALE DATA	SUP	PORT TAP	RES . KEMO	/ED
<u> </u>	PNT	ALPHA	PSI	. L/B	10/0	PM/G	SF/G	RM/Q	YM/Q
		=12:00		=36.304	18.307	143 - 07	15,610		=214+19
	2	=10.00		=30.998	16.771	139.02	14.849	58.45	
	3	-8:00		-25.983	15+385	131.12	14.579		-189418
	4	-6.00		721.001	14 - 117	125.90	13.636		-168 + 28
<u> </u>	5	-4.00		-15.349	13.402	109.82	12.737		-155-57
	6	=2 +00	0 + 0 3	-9.5 08	12.824	95.71	11.944	: 20.55	
	7	0.00	0 • 0 3	-3.428	12 • 461	81 • 48	10.926		*137 *33
	8	2.00	0.03	1.997	12:166	70.27	9.678		⊭128•71
	9	4.00		6.597	12.068	62.85	9.372		-122-73
	10	6.00		10.773	12.238	57.94	9.440		-120-46
· ·	11	8+00		15.159	12.522	. 56 • 54	9.451		-119 -63
h oo .	12	10.00	0 • 03	19.396	13.220	58.01	9.524		=126.03
,**	13	12.00	0.05	23 • 869	14.191	56 • 17	8.257	⇒18+7 0	=126.02

VOUGHT LOW	SPEED	WIND	TUNNEL	TEST	630
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DELTA DATA

ID.NO. 102

(RUN 102-RUN 10)/ 1.00

11/20/81 1438

	WINC	AXES D	ATA	FULL S	CALE DATA	SUP	PORT TAR	ES HEMO	/ED
	PNT	ALPHA	PSI	. L/a	5 D/G	PM/Q	SF/Q	RM/Q	YM/G
	1	H12:00	.0.02	≈36+18 0	17.911	148 • 18	15.871	66.97	-212.20
	چ	=10.00	0.02	=30.796	16.452	139 • 45	-14 - 782	55.89	-197-17
	3	-8.00	0.02			131.43	14.294	. 43.16	=180.23
		-6+00	0.02	-21-150	13.763	128 - 80	13.485	33.62	-165+69
	5	=4+00	0.02	-15.514	12.928	116.27	12.451	: 25.10	-153.18
apara, ay ay ay an	6	=2.00	0.02	=9+446	12.389	99 • 58	11.474	19.69	-141.00
	7	0,00	0.02	■3.588	12.066	85+35	10.571	12.18	
	8	2.00	0.02	1 +923	11.833	72 • 83	9.725	5.83	=125•23
	9	4 + 00	0.02	6.523	11+734	65.43	9.371	=1.54	=119+32
	10	6.00	.0.02	10.937	11.840	61.41	9.270	-8.91	-116 .63
	11	8.00	0.02	15.201	12.233	59 - 84	5.469	=14.22	-119.02
7	12	10.00	0.02	19 4 4 1 5	12.937	59.91	9.387	.=20.79	-119.26
*.	13	12:00	0.02	24.020	13 + 835	58.77	8.213	=19.22	-121 • 16
		•			•			7	ą •

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VOUGHT LOW SPEED WIND TUNNEL TEST &	230	O:
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DELTA DATA

ID.NO. 103

.(RUN 103-RUN 10)/ 1.00

	MINI	AXES D	ATA	FULL S	CALE DATA	SUP	PORT TAR	ES .KEMO	/ED
- () - ()	PNT	ALPHA	PSI	. L/G	D/G	PM/G	SF/Q	RM/U	YM/Q
	1	=12:00	0.02	=32.650	19•911	.141.41	14.043	69.35	=192,58
	2	=10.00	0.02	=28.833	18 • 289	140.29	13.884	53.76	-192.60
	3	*8.00	0.02	-24.496	16.612	134+04	13.774	42.11	m178.15
	•	#6.00	0.02	-20.249	15.201	130 + 55	13.365	33.54	-166-27
7	5	-4.00	0.02	-15.052	14.260	114.37	12,719	24.90	-154.98
	6	=2.00	0.02	=9.552	13.550	99.24	11.867	18+73	=145.26
	7	0 • 0 0	0.02	=3.987	12 • 838	84+96	10.999	10.58	=136.06
	8	2+00	0.02	1.928	12.524	71.79	10.309	4.00	-130%66
- CO - T-	9	**00	0.02	7 7.059	12.533	63.92	9.974	⇒3.85	4126+14
	10	6.00	0.02	12.051	12.639	61.17	9.906	.#10.15	-122×93
	11	8.00	0.02	16.826		58.08	9.898	-15.03	-120 .82
	12	10+00	0.02		13+700	61+96	9.757	.=22.04	=126.84
	13	12:00	.0.02	25 • 653	14.769	** '		.₩2U.85	=126 - 67
						€ 490	8.546		

DELTA DATA

10.Na. 101

TRUN "104-RUN 101/ 1.00

W	IND	AXES D	ATA	FULL S	ALE DATA	SUPPORT TARES REMOVED			
<u> </u>	NT	ALPHA	PSI	~L/Q	D/G	PM/U	SF/Q	: RH/G	YM/Q
	1	#12 *00	.0.02	=31+087	19 • 827	125.07	5.634	. 47.57	=130•ĢŌ
	2	=10.00	0.02	=27:025	17.976	128.79	5.728	85.8E :	=126 + ₽3
	3	-8+00	0.02	-24+429	16 • 155	136 * 29	6.056	32+44	-128-77
	4	-6+00	80.0	-19.819	14.796	129.87	6.702	27+15	=135.98
	5	-4.00	0.02	-14.584	13.722	115.32	7.127		=139.58
**************************************	6	=2.00	0.02	-8.910	13.218	92,59	7 - 144		=137.28
	7	0 + 0 0	0.02	42.889	12.721	74.92	7.082	8 . 89	
	8	2.00	0.02	. 2.230	12.367	65.37	7.100	2.59	=133 #73
	9	4+00	0.02	7 . 651	12.353	60.01	7.337	-4.12	-132 18
	10	6.00	0.02	12.585	12.372	57 • 76	7 . 654	.=11.77	-132-12
	11	8.00	0.02	17.392	12.868	56.24	7.831	-14.53	-130/-97
Mariania atamber di al-	12	10.00	0.02	21.880	13.570	57.76	7.955	×19.97	
	13	12.00	0.02	26.031	14.392	59.27	7.087		=131.46

A-199

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID,NO. 105

(RUN 108-RUN 10)/ 1+00 .

	WIND AXES DATA			FULL BCALE DATA SUPPORT TARES REMOVED					
	PNT	ALPHA	PSI	L/G	0/0	PM/Q	3F/Q	RM/Q	YM/Q
	1	=12.00	0 :: 02	-30+911	16+518	128+00	6.336	52.88	=146+81
	2	#10.00	0 .02	≈26 + 664	14.767	124.77	6 . 173	43.85	=147 ×93
	3	-8+00	0.02	#23.999	12.828	139.35	6.774	36.17	-148-18
	4	-6.00	0.02	-19.416	11 307	135:02	7.119	30.20	-150.83
	5	-4+00	0.02	-14.382	10+167	113.93	7.507	: 23 -69	-155 ×43
ن به منه المحمد الم	6	#2.00	0.02	=8.478	9 • 476	88 • 15	7.537	19.41	=155 · 58
	7	0.00	0.02	=2 • 5gg	8 • 901	67.49	7.529	12.77	=154+99
	8	2.00	0.02	2 9 9 9 6	8+600	57 - 88	7.500	5.31	=154.56
	9		0.02	7.991	8.501	50.83	7.461		-149 47
	10	6.00	0.02	12.977	8 • 672	46.51	7.568		-145.10
	11	8.00	0.02	17.626	9.005	47047	7.658		-139.80
•	12	10.00	0.02	21.881	9 + 7.04	48.52	7.688	: 20.51	-140.56
	13	12:00	0 : 02	26 • 195	10.630	49.38	6.784	=18.92	=134+58

DELTA DATA

ID.NO. 106

IRUN 106-RUN 61/ 1-00

	IND	AXES	DATA	FULL SC	ALE DATA	SUI	PPORT TAP	RES HEMO	/ED	
in the second	NT	ALPHA	PSI	, L/Q	p/0	PH/G	SF/Q	. RM/0	YM/Q	
	1.	≠ 0 + 07	·=24+00	9 + 631	31 +844	=11 ×35	≈ 50,905	19.22	141 683	
	2	=0.07	': =22 *00	7.091	28 • 229	4 • 67	=45.779	19.85	.118.65	
	3	-0.07	-50.00	4 4 8 7 5	25.070	. 24+67	-41.017	: 23.96	98+30	,
	À	-0.07	-18-00	3.521	22.228	33.52		. 23.05	69.22	
	5		-16-00	3.003	19.561		-31.139	21.12	36.61	
•	6	=0+07	=14+00	: 2.113	16.941	60+64		15.26	8 • 26	
	7		=12+00	1 1749	16:208	52:91	-22.909	15.22	=15.26	
•	8		-10-00	1.017	15 • 057	60.37		. 13.45	-39.96	
	9		-8.00	-0.415	14+340	71.84		17.38	-68.72	
	10		-6.00	-1-196	13.918	77+80	×7.644	: 20.73	-94.21	
	11	-0.07		=1.656	13.536	85.05	-3.614	: 22.74		S
	12	=0+07		=1.626	13.543	86 • 23		. 24.12	=127+35	
`	13	-0.07		=1.446	13+705	85 • 53	4.307	32.41	=142.91	
	14	=0 . 07		×1.535	13.913	85 • 10	9.340	: 23.26	-140 -99	
	15	-0+07		=0.989	14.311	74 • 53	14,028	. 25.70	=160 c01	
	16	-0.07	and the second s	-0.483	14.730	65.95	19.215	33.07	-201.88	J.
	17	#0.07		0.686	15 - 437	50.70	23.501	37.58		-1
	18	=0.07		1.965	16.578	34.96	28,333	37.24	=235.37	
	19	=0+07		3 + 446	17 + 817	24+26	31.945	38.96	£260.31	
	20	-0.07		4.710	19.372	14.23	37.632	37.61	=285.53	
	21	-0.07		5.813	20.964	5.40	41.758	37.45	-303,33	
	22		18+00	6.476	23.283	-6.54		42.20	-331.83	
	53	-0.07		7.222	25.876	-12.39			-365.68	
ing naka maka katawa iliku mak	24	=0.07		8.037	28.511	=26.01	55.785	45.79	=396+36	
e	25	=0 + 07		9+340	31.639	=37.88	60.799	49.32	=416 •12	

ORIGINAL PAGE IS OF POOR QUALITY

A-201,

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 107

(RUN 107-RUN 10)/ 1.00

	WIND AXES DATA			FULL SCALE DATA SUPPORT TARES HEMOVED						
	PNT	ALPHA	PSI	. 4/0	D/0	PM/G	SF/Q	RM/Q	YM/Q	
	1	=12:00	0.02	=6.342	7.505	=163.96	3.940	43.32	=122.06	
	2	=10.00	0.02	·=5 • 451	6.992	≒150 •53	3.618	: 31 . 91	#113 × 28	
	3	-8-00	0.02	-4.824	6.646	■135.54	3.455	: 26.17	-107+23	
	4	-6.00	0.02	*4.338	6.264	-118.07	3.632	: 21.87	-116.00	
	5	-4+00	0.02	-3.527	5 - 811	-101.85	4 . 534	17.31	-134+23	
ى ئىمىيىتى ئەرىلەر دىرىدىلى ئىمىيىلى ئىمىيىلىدىدىلىكى بىلىنىدىلىكى بىلىنىدىلىكى بىلىنىدىلىكى ئىلىنى بىلىنى باشى ئىلىنى ئالىرىدىلىكى ئالىرىدىلىكى ئالىرىدىلىكى ئالىرىدىلىكى ئالىرىدىلىكى ئالىرىدىلىكى ئالىرىدىلىكى ئالىرىدىلىكى	6	=2.00	0 402	.=2.818	5 • 626	=86+84	5.459			
	7	0 . 00	0 . 02	.=2.045	5.394	-75 • 32	5.825	11.434	N150 €97	
	8	2.00	0.02	-1 - 129	5.032		6.000		=148+1A	
	9	4.00	0.02	-0.284	4.837	-46 · 16	6.033		43.95	
	10	6.00	0.02	0.614	4.702	-32.65	5.966	The state of the s	41.87.11	
	11	8.00	0.02	1.456	4.802		5.937		-135-10	
	12	10.90	0.02	2.273	4.969	=0.53	6.127		=137+07	
**	13	12.00	0.02	3.092	5 • 163	16.09	6.178	.=21.23	=139 #03	

ORIGINAL PASS SO OF POOR QUALITY

A-202

es v		VOUGHT L	ON SPEED	WIND TO	INNEL TES	T, 630		
NACE CESTIFICATION OF THE PROPERTY OF THE PROP		dengan at terrena at terrena at terrena	.DELTA	DATA		g frank a new transport and the second	to and the forther and a decrease.	and the second s
	i Orași de antică de antică de a	ĺ	ID, NO	• 108			rage de la companya d	yang di panggalagan di di di panggalagan
Nacional Company on March 1997	And the second second		RUN 108-	RUN 10	/ 1.00	4.	·	····
			11/20/81	1438				
WI	ND AXES	DATA	FULL SC	ALE DATA	N SUP	PORT TAR	ES .KEMO	/ED
PN	T ALPHA	PSI	. L/G	D/G	PM/G	SF/Q	. RH/G	YMZ
	1 =12:00	0 + 03	. ≈6∘3 08	7 • 772	=166 +35	3 • 275	: 34.36	=116+84
	2 m10 + 00	0.03	-5 479	7 • 253	=152.06	2.714	•	H107:61
	3 -8 +00		-4.825	6 • 7.84	=135·83	2.446	19.50	-100.55
ing pagamanan di kacamatan di ka Kacamatan di kacamatan di kacama	M6+00		-4.386	6.392	-117-25	2.783	16.12	m108+67
	5 =4.00		#3·602	5.928	+103.41	3.825	12.40	
	6 =2.00		=2∘881	5 • 674	=88 . 25	5.04C	11.22	#143 · 78
	7 0.00		=1 · 970	5•496	= 75•76	5 + 474	7.95	=150+39
	8 2:00		=1.060	5 • 175	=60+34	5 • 630	ತ+05	=148 +80
	9 4+00		-0.197	4 . 899	-45.37	5.694	•3.25	
		A CONTRACTOR OF THE CONTRACTOR	0.719	4.734	-31.08	5,600	≈7.83	
4			1.557	4.802	=16.64	5.564		-136.31
1	2. 10.00		2 + 3 6 8	4.935	· =0.20	5.672	M16.11	
1	3 12 • 00	0.03	3 • 1 4 0	5 • 065	17.38	5 • 684	#17.15	-141 + 41

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ORIGINAL PACE IS OF POOR QUALITY

A-203

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

10.NO. 109

(RUN 105-RUN 10)/ 1:00

etti tymania et järenatassa – taa	WIND	AXES D	ATA	FULL SC	ALE DATA	SUP!	PORT TAR	ES .KEMO	/ED	**************************************	
to a grande to the second	PNT	ALPHA	PSI	. L/G	0/0	PM/G	SF/Q	: RM/G	YM/G	· · · · ·	
	1.	=12:00	0 . 03	=6+470	7+601	=163.57	2.062	: 31.70	-90+90		
	2	≈10.00	0.03	=5.579		=151.80	1.942	: 25.25	=90+67		
	3	-8.00	0.03	-4.921	6 • 8 4 5		1.741	. 19.23	-86.11		
	4	-6+00	0.03	-4435	6.419	-114.98	2.075	16.35	-92.51		
	5	-4.00	0.03	-3.635	6.068	-102.57	2.786	13.55	-106.38		
	6	=2.00	0.03	=2.864	5 • 785	=87,29	3.295	12.53	=121.78		
	7	0+00	0+03	=2.041	5.532	=74 • 11	4.563	8.52	H129 442		
	8	2.00	0 = 03	=1.079	5.336	= 58 • 95	4 . 692	2.91	=123.85		
	9	4.00	0.03	-0,180	5 • 169	-43.98	4 . 877	-4.23	-120.40		
	10	6.00	0.03	0.747	4+835	-27.52	5.030	×7.21	-120-39		
	11	8.00	0.03	1.595	4.935	-12.81	5.224	-11.06	-121-19		
/////	12	10.00	0.03	2.468	5.069	3.47	5.386	=15.49	=129 · 10		
•	13	12.00	0.03	3.297	5.363	16+62	5,559	=18.93	=132+37	i	

YOUGHT	LOW	SPEED	MIND	TUNNEL	TEST	630

DELTA DATA

ID.NO. 110

(RUN 110-RUN 10)/ 1.00

NIN	D AXES D	ATA	FULL SCALE DATA SUPPORT TARES . NEMOYED					
PN1	ALPHA	PSI	. 4/8	D/@	PM/Q	SF/Q	RM/Q	D/MY
	#12:00	0.03	=15.492	9.580	.: =184∗05	3.532	34.64	=1 02 * 73
; 2		-0.403	#11·003	8.916		2.750	: 29.17	
	-8+00	0.03	*7.316	8 • 265	-161-18	2.611	: 22.01	-95,98
	-6.00	0.03	#3+668	7.726	-138 - 87	2.731	17.48	
	-4.00	0.03	0.011	7.266	-122.66	3.462	13.76	-103.85
(=2.00	0.03	3 • 8 7 4	7.032	=1 ,00 •95	4.070	11.12	
7	0 • 00	0.03	7 + 458	7.063	≈83 •57	4.329	8 + 0 4	
3	2.00	0.03	10:616	7 • 165	=64.49	4 . 411	4.93	
	4.00	.0.03	13.539	7 * 100	-41.81	4.665		=119.78
	6.00	0.03	16.330	7.270	21.55	3.079	*3.29	
		0.03	19:147	7.572	-1.33	5.574	=12.48	
12		EQ+0.	.22 • 496	8.209	20+69	5,958	=18.99	=120.05
13		0+03	25.797	9:097	40 - 41	5.750	=19.91	#118.51

DELTA DATA

ID.NO. 111

(RUN 111-RUN 10)/ 1.00

****	WIN	D AXES	DATA	FULL S	CALE DATA	SUP	PORT TAR	ES ,KEMO	YED	.:
	PNT	ALPH	PSI	. L/U	0/0	PM/Q	SF/Q	RM/Q	YM/Q	
	. 1	=12+00	0.03	=24.091	11+431	=175+70	0.669	36.51	-87+62	
	2	#10+00	EQ#O	-21.346		-160+34	1.280	. 31.65	-96 .98	
		-8.0	0 • 03	#18.780	9.452	-143.99	2.573	27.21	=105 43	
<i></i>	4	-6+0(0.03	m16.338	8.990	-123.09	4.310	22.24	-122-76	
	5	m4+0(0.03	-14.191	8 • 633	-104+96	6.196	16.77	-141 *83	
-1 <u>-91</u>	6	-2.00	0 • 03	=11+287	8+365	-82.96	7.019	10+69	=145+87	
	7	=0+00	E0.0	=8 • 165	8 • 329	- 74 • 71	7.062	4,20	=142.52	
	8	2.00	0 • 03	≠5 • 252	8 • 366	=54.12	7.100	#1. +Q4	=135+48	
	9	4 × O(0+03	.=2.631	8.399	-36 • 68	6.935	-7.99	=134.26	
	10	6.0	0.03	0.499	8.569	-18 - 25	6.861	-13.48	=128.79	
	41	8 • 0	0.03	3.500	8.802	90.37	6.398	-15.12	=122.80	1 5 4-1
7	1.2	10+00	0.03	7 • 470	9+192	19+99	6.192	:=21.03	=119+85	
	13	12.0	0 * 03	10.091	9 • 797	39+34	5.584	. = 20+26	=120 e03	

VOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630
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DELTA DATA

ID.NO. 112

(RUN 112-RUN 10)/ 1.00

	WINI	DAXES	DATA	FULL SCALE DATA SUPPORT TARES .REMOVED						
	PNT	ALPHA	PSI	L/Q.	p/@	PM/G	SF/Q	. RM/Q	YM/Q	11.
	1	=12:00	-0+05	=21:193	10.708	=179 + 22	2.839	35+90	=103×87	
	2	=10:00	0.05	≈18.044	9.820	m167+88	2.619	. 29.35	=107+19	
	. 3	-8.00	0.05	-14.758	9.017	=148 * 70	2.429	: 23.55	-102:51	
		#6+0C	0.05	=12.150	8 + 450	-123.50	3.333	21.48	-114-67	
	5	m4 . 00	0.05	-9.277		7 7 7 7 7	4.874		-129 -73	
Mily - Haylag Sidi - Yanisi ini da a	6	=2.00	0 . 05	=6.602	7 • 629	=91.52	6.514	12.28	=143 -22	
	7	0 + 0 0	0.05	-3.465	7.529	-73. 05	7.293	5.00	=145.46	
	8	2.00		-0.502	7.713	=54.91	7.573	#2.38	-139.21	
The state of	9	4.00	0.05	. 2.275	7.929	-35 - 74	7.737	-11.50	H134+42	
e de la companya de La companya de la co	10	6.00	0.05	4.597	8.236	=17+73	7.527		-128 .64	
	ii	8.00		6.774			6.785		-121.48	
7	12	10.00		9.898	9 + 100	18.19	6.391	:=22.27		
\ ,.	13	12.00		12.452	9.963	37 + 83	6.150	:=22+84		

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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 113

IRUN 113-RUN 101/ 1.00

*	WIND	AXES	DATA	FULL SCALE DATA SUPPORT TARES HEMOV					/ED	
inigan terrapa kanan terrapa kan	PNT	ALPHA	PSI	. L/Q	D/Q	PM/Q	SF/Q	RM/Q	YM/Q	
	1	=12+00	0.04	=37∙710	15.420	86+74	3,042	39.63	#112.65	
	5	≈ 1,0 • 00	0.06		13.031	124.21	2.465	32.58	=107:24	
Section 1997	3	-8+00		-24.883	11.285	130.58	3.010	: 24.00	-118.20	
And the second	*	-6.00	0.02	=28.138	10.054	115.27	4.090	19.25	≒128+35	
	5	-4+00	0.01	-22.615	9.203	90 • 43	5.524		-146.21	
	6	42.00	0.01	=16.984	8 • 491	64,36	7.036	10.70		
	7	0 + 00	0.01	=11.320	8 + 230	41-64	7.494	4 • 97		
	8	2.00	0.06	#5.970	8 • 200	23.69	7.273	0.49		
	9	4.00	0.06	-1.674	8+259	9.75	7,168		-134+26	
	10	6.00	0.06	2.674	8+438	-1-49	6.826		M126 . 75	
	11	8.00	0.06	7.079	8 • 835	-7.99	6.232		-120-11	
7	12	10+00	0.06	11.345	9.370	-6+36	6.156		=118.66	
	13	12.00	0.04	14.996	10 • 164	= 1.33	5.517	-18.00		

DELTA DATA

ID.NO. 114

(RUN 114-RUN 10)/ 1+00

WIN	D AXES D	ATA	FULL 8	ALE DATA	SUP	PORT TAR	ES REMO	YED	
PNT	ALPHA	PSI	, L/Q.	D/Q	PM/Q	SF/Q	RM/Q	YMZQ	
1	=12:00	0 + 01	≈38.0 01	15 • 446	96+18	3,930	. 40.62	=126 •42	
2	#10:00	0.01	=38.275	13 • 116	154.20	2.769	36.27	=114-16	
	-8.00	0.01	-34.805	11,448	162 - 65	3.374	: 28.61	H126+44	
	-6.00	0.01	-30.792	10.120	155.39	4.921	: 20.87	-144.31	
. 그 사람이 하면 가게 되는 것이 되었다. 	-4.00		-24.750	9 • 248	128.94	6.260	15.51	-154.83	an nak
8		0.01		8.720	96.46	7.767	12.05	=162.36	
7	0 + 0 0	0 + 01	=12:890	8.366	69.53	7.875	6 + 19	=156.05	
8	2.00	0.01	7.470	8 • 234	46.99	7.926		=148+09	
	4.00	0.01		8.299	: 27+94	7.769	⇒7.53	=142+87	
	6.00	.0.01	1,943	8 * 471	11,49	7.461	-12.28	=134.83	
		.0.01	6.552	8 • 833	-0.14	7.000		-132:30	
7 12		0.01	11.315	9+404	•7•30	6.756		=126.38	,
13	_	0.01	15.854	10 + 268	=13+98	6.216	:=20+28	=122+36	

DELTA DATA

ID.NO. 115

:(RUN 115-RUN 10)/ 1+00

11/23/81 0818

	WINC	WIND AXES DATA		FULL SC	FULL SCALE DATA S			SUPPORT TARES REMOVED				
······································	PNT	ALPHA	PSI	L/Q.	0/0	PM/G	SF/Q	RM/Q	YM/Q			
	1	H12 • 00	.0.00	=38+840	15 + 471	106-22	3 . 8 4 5	. 41+66	=123×89			
	2	=10.00	0 000	-38.122	13:334	-148 - 90	2.903	. 35.95	-116.11			
	3	-8.00	0.00	-34.535	11.565	157.60	3.264	. 26.94	-122-43			
	:4	-6.00	0.00	-29.860	10.399	145 . 82	4.690	: 21.43	-139.60			
	5	-4+00	0.00	424+847	9 • 403	125.68	6.297	15.12	=155 ×13			
- variable in the last of the	6	-2.00	0.00	H18.943	8 • 7.94	93.77	7 . 726	11.16	=161.36			
	7	0.00	0.00	=12+889	8 4 4 6 2	65.06	7.795	4.96	#154.70			
	8	2.00	0 + 00	≈7.5 37	8 400	44+08	7.800	#1 +84	=146.50			
	9	4.00	0.00	:-2.571	8 • 530	. 23.28	7.441	.=12010	=138.86			
	10	6.00	0.00	1.796	8+668	7.92	7.330	-12,57	=132.95			
inga ing sangangan	11	8.00	0.00	6.679	8 - 969	-3.02	6.832	.=16.49				
7	12	10.00	0.00	11+341	9 • 5 9 7	=8+14	6.625	.=21.51				
	13	12:00	₩0+00	16+154	10 + 430	=14 *90	6.250	=21.66	4123.22			

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A-210

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	Vandet	LOW SPEED	WIND TU	INNEL TEST	630	kgirlataa vanna tihuaraan admir tihuveen a	
	a significación de posición de la companya de la c	.DELTA	DATA				استجمع في المستحدث ا
		ID.NO	• 116	······································	4.	2 · · · · · · · · · · · · · · · · · · ·	
	* * * * * * * * * * * * * * * * * * *	IRUN 116-	RUN 10)	/ 1.00		مريد المحالي المستريخ	
		11/23/81	0818				
WIND AXES	DAYA	FULL SC	ALE DATA	SUPP	ORT TARE	S : KEMO	YED
PNT ALPH	A PSI	. L/G	D/G	PH/Q	SF/Q	: RM/Q	YM/G
1 412+0		=36 • 475	15 • 451	70+99			=111 <07
2 #10+0 3 #8+0		-33.362 -29.911	13.686	85+24 94+15			=100+94 =106+59
		-25.874					₹125.80
5 -4.0		-21:318	9.331	79.27	4.865		≈137 «98
6 =2.0			8 • 527	62 • 88	6 . 406	12.12	
7 0 • 9			8 • 195	41.50	6.942		#144913 ********
8 2·0 9 4 •0			8 + 234	23.58	7 . 166		=137.67
10 6.0			8+325 8+498	8 • 62 = 1 • 23	7.091	- 7 LCC	≈133+22 ≈126*39
11 8.0			8 • 802	-9.01	6.552	#15.42	=119+79
-(<u>12 10.</u> c			9.293	=8.19	6.324		=116.20
13 12:0			10.268	×4+86	5.916		=115.28
		•					
		1					
		<u> </u>	de de la companya de				
기계 보고 생각하는 경기 기계							
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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 117

IRUN 117-RUN 10)/ 1+00

	WINC	AXES DA	TA	FULL SCALE DATA SUPPORT TARES HEMOVED						
ty	PNT	ALPHA /	PSI	. L/G	D/0	PM/G	SF/Q	RM/Q	YM/Q	
	1	#1,2+0o	0.01	#39.90B	15 • 821	125 • 51	3.631	. 42.82	4122 (33	
	2	H10+00	·0 • 0 1	-36.235	14 • 101	131 453	2.922	33.39	=115 •30	
	3	-8.00	0.01	-32.529	12.343	140+79	3.000	: 28.41	-120 ×03	
	*	#6.00 ·	0.01	-27.703	11.084	121.75	4.140	: 22.28	=134-11	
		-4.00	0.01	-22.115	10.096	93.31	5.424	. 17.01	-145 -85	
	6	=2.00 ·	0.02		9 4 4 8 7	64+17	6.744	14+34	W152.46	
	7	0.00	0.02	=10.7g3	8 • 975	42 67	7.356	8.07	-150 ·42	
	8	2.00	0.01	=5 + 870	9.000	: 26.54	7.566	v •53	=143.58	
	9	4.00	0.01	-1.640	9 • 099	. 11.51	7.640	•7×45	-138 ·32	
	10	6.00	0.01	: 2.478	9.204	0.68	7.388	-12-10	=130 €90	
		8.00	0.01	6 6 6 9 5	9 • 534	84.68	6.59)	-15.43	-125.91	
	7 12	10.00	0.01	11.180	10.004	≈10+73	6 + 757	.=21,28		
	13	12:00	0.01	15 295	10+930	#17+25	6.417	:=21.82		

DELTA DATA

ID.NO. 118

(RUN 118-RUN 61/ 1+00

. 11/23/81 0818

DNIND	AXES	DATA	FULL 8	CALE DATA	sur	PPORT TAP	RES . KEMO	VED	
PNT	ALPHA	PSI	. L/8	D/Q	PM/Q	SF/Q	. RM/Q	YMZQ	
1	m0+08	:=24±00	·=4 • 584	30.078	24 • 17	=43.344	. 39+60	74497	
2	≈0÷08	:=22.00	-=4 .181	26 • 759	. 24 . 41	≈38.674	34+29	57 • 04	
3.	*0.08	-20.00	-4.548	24.096	28 - 43	-34.770	31.12	- 44+04	
	-0.08	-18-00	J#5.223		35.90	-30.163	28.32	: 25+20	- \$1 , Š
그는 사람들이 가득하셨다면 하루다.	-0.08	.=16+00	-6.675		44.18	=25.723	. 24.52	4 • 85	1.4
6	=0.08	-14+00	=8.307	17.230	63 • 64	=21.027	: 20.15	:=22 .33	
7	₩ Û+Û8	=12.00	-9:371	16.713	60 + 38	=16.754	19.55	-=44 • 8 Q	
.8	= 0+08	-10.00	=9.9 40		65 + 07	-12.258	18.53	E8#88#	
9.	-0.08	·. =8.00	-10.735	14.874	70 + 47	-7.224		1=95.08	
10	-0.08	-6.00	#11.211		70.82	-2.976			
	-0.08	-4.00	-10.813	14.307	69.38	0.037	. 21.99	-130-62	
12	=0+08	-2.00	=10:096	14+331	65.58	2,982	. 21.53	4136 499	
13	≈0.08	0.00	=9+181	14+819	59+25	4.789	. 28.96	=134 +03	
1.4	≈0 • 0 8	2.00	#8 +596		57 . 87	7 • 470	. 24.58	=123 •99	
15	-0.08	4.00	-8.283		53.94	10.634		-126.90	
16	-0.08	6.00	7.489	15.627	50.85	15.059	23.57	-147:07	nane Salata
	-0:08	8.00	-7.440	16.025	. 46.39	17.361	: 26.06		
18	≈0.08	. 10.00	=6.566		38,62	21.115	: 26.97	×172.77	
19	#0 · 08	12.00	=5.392		: 28+48	25.843	. 25.38	#194 #53	
20	#0 + 0 B	14.00	·#4 # 450	19.331	17 +10	29.900	. 27.54	=223+94	
21		16,00	-3.13g		3,67			=248.97	
52		. 18-00		23 • 133	-0.01	39.639	: 28.25	-272.26	4. ***
23	#0+0B	. 20.00	-0.565		7.26	44.433	. 28.71		
24	-0,08	: 22.00	:=1.121		-12.22	48.386	. 22.94		
25	≠0 ₹08	. 24.00	=2.771		-2.08	50.819	10.32	=291 • 97	
					ng Ku Remigrasi				

DELTA DATA

ID.NO. 119

.(RUN 119-RUN : 6)/ 1+00

		WIND	AXES	DATA	FOLL SC	ALE DATA	SUF	PPORT TAP	RES . KEMO	/ED
*******		PNT	ALPHA	PSI	. L/G	D/Q	PM/Q	8F/Q	; RM/Q	YM/Q
		1.		:=24+00	-4.609	30+464	28+20	=44.219	55+03	78 27
		2		:=22+00	-4 * 7 7 7	26 + 882	. 29 • 33	=38.594	: 38,69	58 • 41
		3	-0.08	-20-00	.#4 :686	23.923	33 413	-34.782	. 33+54	44.33
		4	-0.08	#18 a00	-5.730	21 . 826		=31.231	39.55	23.88
		5	~0+08	-16.00	-7-078	19 488	- 48+43	#25.693	1 30.01	-0.25
	<u> </u>	6	-0.08	-14.00	=9.037	16.967	· 65 · 22	-20.922	: 24+13	.=28 -72
		7	#0:08	-12.00	-9.612	16 • 459	57.02	-17 - 114	: 24.08	-49 +29
		8	=0.08	=10+00	=10.183	15.508	63+36	=12.262	19.94	-75 - 15
		9	=0.08	-8.00		14.642	69.21	-6.865	19.11	■103.36
*.		10	-0.08		-10.873	14.330	69.74	-2,877	. 20,98	=124+69
		11	-0.08			14 - 128	68+05	-0.012	23.86	=139 =13
7	·	12	=0+08		=10.120	14.289	65.61	3.373	. 22.77	≈148.00
,	•	13	#0+08	0 # 0 0	=9.452	14.548	59.32	5.271	31,43	=146,65
		14	=0+08	2.00	-8+855	14.759	56 + 25	7.548	. 26+04	=133.40
*****		15	-0.08		-8.494	14.970	52.85	10.555	24.61	
		16	-0+08	6,00	-7.892	15.362	47.85	14.667	: 27,51	
		17	-0.08		-7.380	15 - 995	42.96	18.385	: 32.19	
	<u> </u>	18	=0.08	10.00	-6.480	16.833	32.82	21.970	, 34.12	
		19	=0+08		=5.367	17 - 891	19+35	26.265	32.00	-214+19
		20	=0.08	. 14.00	-4.349	18.916	5 • 65	30.181	: 35.47	=236 •56
		21	-0.08			20 - 874	-10.22		34.24	
		55	-0.08		-1.831	22.380	-11.90	39.880	36.49	-281.47
		23	-0.08		-0.883	24 • 835	-17.31	45.063	38.75	
		. 24	=0.08		-1.591	27.962	=18.19	49.217	37.07	
		25	=0.08		=4.217	30.814	13.77	49.886	2.31	

where r_{ij} is the second of the second of the second of r_{ij} and r_{ij} is the second of r_{ij}

DELTA DATA

ID.NO. 120

.(RUN 120-RUN 10)/ 1+00

	MIND	AXES [ATA	FULL SCALE DATA SUPPORT TARES RE					MOVED	
	PNT	ALPHA	PSI	. 4/0	D/0	PM/Q	SF/Q	: RM/G	YM/Q	
	1	=12.00	0.02	=26.370	15 • 737	.144,20	10.101	61.94	=187 €08	
	2	#10·00	0.02		14 + 446	147.50	10.371	53 17	-183+84	
	3	-8.00	0.02	-23.437	13.455	.146.92	10.555	. 41.91	-172+45	
	4	-6.00	.0.02	-21.686	12.503	.145.89	10.246	33,52	-160.41	
	5	-4.00	0.00	-18.243	11.762	:120+35	9.796	. 24.78	-151.21	
	6	=2+00	0.0%	-14.458	11 + 173	92.46	9.204	. 17+58	≒139•49	
	7	0 + 00	0 = 00	=10:824	10 + 608	66+14	8.528	11.32		
	· g	2.00	0.02	=7 + 469	10.267	43 81	8.247			
	9	4,00	0.02	-4.118	9.971	. 22.07	8.135		-125.99	
	10	6.00	0.02	-0.632	9.700	1.93	8.017		-124.52	
	11	8.00	0.02	2.608	9 • 7.02	=18.41	7.864	A SECTION OF THE PROPERTY OF T	-128+24	
(12	10.00	0.02	6 • 145	9 • 669	-=43+14	7.891		≈132 €63	
**	íЗ	12.00	0.02	9.908	10.082	=69 ∙80	7.649	:=22.63		

DELTA DATA

10.NO. 121

:(RUN 121=RUN 10)/ 1+00

	WINC	AXES D	ATA	FULL S	FULL SCALE DATA SUPPORT TARES REMOVED				
	PNT	ALPHA	PSI	. 4/0	D/0	PM./Q	"SF/Q	. RM/Q	YM/Q
	1	m12+00	0 • 00	=26.943	15 • 138	150.78	10.065	68.07	-193+04
	2	=10+00	0.00	=25.184		152.09	10.354	52.19	=185 #89
	3	-8.00	0.00	#23.365	13.533	447 *59	10.494	41.81	4174703
사람이 하는 것으로 하는 것이다. 	*	-6.00	0.00	-21-377	12.402	147 - 11	10.287	: 31.95	=161.99
그 싫어됐다.	3	-4-00	. 0.00	-18.258	11.769	123.56		: 23.75	-152.65
, , , , , , , , , , , , , , , , , , , 	6	-2.00	. 0.00	=14.369	11+155	93.71		. 17.35	=139+84
	7	0.00	0.00	-10.834	10.686	66.57		10.52	=131+80
	8	2.00	0 * 00	=7.+244	10.239	43 + 51	•	2.59	≈126+49
	9	4.00	. 0.00			21.61		. =4.95	=126+19
	10	6+00	0.00	-0.754	9 • 873	1 * 51	tan and the state of the state	-10.34	-128-14
	11	8.00	0+00	2.524		=19 • 19	化二甲醇 经国际证券 医二甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基		-129+98
	12	10.00	0.00	. 6,207	9.773	=43.67			=134+36
\ .	13	12.00	0.00	9.921	10 • 148	-70.18		:#21.05	
									•

omenny pacs is of foor quality.

A-216

VOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630
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DELTA DATA

(

ID.NO. 192

(RUN 122-RUN 10)/ 1.00

IM	ND	AXES D	ATA	FULL SC	ALE DATA	SUP	PORT TAR	ES .KEMO!	ED
PN	T	ALPHA	PSI	, L/a	D/Q	PM/Q	SF/Q	: Rm/Q	YMZQ
	1:	=12+00	0.01	#39 •744	18 • 764	.117 • 61	6.102	54.50	=142*98
	2	=10∘00	0.01	35.490	17:176	125 . 34	6.098	· 40 . 01	-142 413
	3	-8.00	.0.01	-31,806	15.715	129.23	6.616	33.59	-145.21
	4	m6.00	0.01	-2%.601	14.582	.120 .98	7-074	. 28.52	-147+34
	5	#4 - 00	0.01	-81.909	13.776	96.91	7.806	20-49	-148-58
	6	=2 ∗00	0.04		13.239	71+91	8 • 635	14.50	=148+34
	7	=0.00	0.01	⊭1့် ႏို့ ∗ ဆည်ႏု	2 • 8 4 4	52.95	5 # 361	6.39	=142:39
	8	2.00	0.01	#6 0 6 N	12.700	39 + 38	8 . 966	#U+46	■135 • 69
	9	4.00	0.01	m1.73&	12.928	. 24.51	9.097	*9.42	#131+16
- 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 .	6.90	0.01	2.713	13.039	14+41	8.893	-13.90	-127-23
	1	8+00	0.01	7.034	13.500	3.82	8.320	=16.35	4122.70
1	2	10.00	0.01	11.307	14.004	1 • 88	8.422	:=23.28	=120.57
1	3	12.00	0.01	15.462	14 850	4 4.99	7.584	:=20.92	#119 w39

VOUGHT LOW SKEED WIND TUNNEL TEST 630

DELTO, DATA

ID.NO. 12.

(RUN 123-RIN 10)/ 1:00

Anna d	KIND	AXES D	ATA	FULL SC	ALE DATA	SUP	PURT TAR	ES .KEMU	/ED
J. S. S.	PNT	ALPHA	PSI	L/U	p/Q	PM/G	SF/Q	Rm/ù	YMZQ
V.	1.	-12.00	0.01	⊭39•6 <u>18</u>	18 • 841	116.53	6.406	53.23	-145. 66
The second secon	The state of the s	=10.00	0.01	#35.092	17 203	155.55	6,03"	41.27	H141+12
	ජ 4	=8.00 ≠6.00	0.01	-31.491 -27.241	15 • 730 14 • 643	128 • 75 120 • 68	6 • 50 t	28.07	=142.15 =145.19
	5	#4+Uñ	0.01	-21.752	13.815	58+04	7.653	20.56	-150.11
	6 7	#2*00	0.01 0.01	*16:217 *10:620	13.312 12.897	72.23	8 · 4 · 2 8 · 63	15.96	-147 · 25
	9	2:00	0.01	-6.937	_12 * 80ປີ.	<u> </u>	8 9 9		14135.63
	10	4.00 6.00	0.01	-1.731 2.614	12.970 13.073	24.82 13.66	9+117 418 44	-13.95	#131,41 #127:32
	11	00.8	n • 🕅	7.033	13.599	3.78	8. 16.2		-124.18
-	12	10.00	0 • \$1 0 • \$1	11.200 16.239	14 • 15C 14 • 926	0 • 69 =7 • 46	8 • 4 5 1 7 • 4 7 5		=119.79 =119.79
1					*****	~ · · · · · · · · · · · · · · · · · · ·			171

YOUGHT LOW SPEED WIND TUNNEL TEST 630.

DELTA DATA

ID.NO. 124 (RUN: 124-RUN 10)/ 1.00

	MIK	AXES	DATA	FULL S	CALE DATA	SUF	PORT TAR	ES HEMOV	'EO,
	PHT	ALPHA	Pel	L/Q	p/e,	PM/Q	· SF/Q	: RH/Q	YHZQ
	1	=12.00		=34+995	17+148	:125 * 48	7.583	54+49	m161+89
	2	=10=00	. 0401	-31,603	15/441	.125.94	6.867	43.98	4152432
	. 3	-8-00	0.01	A29.256	13+410	.140.96	6.863	36.92	-153765
	·	-6.00		-247378	12-139	127 - 27	6.658	1 29.51	4153638
	31 5	*** · 00	C. 0.00	-194748	10.937	102.45	7.346	23.52	-160%16
•	6	-2.00	0.00	*14.660	10.357	72.10	8.583	18+95	=162.89
	7	=0.00	0.01	1=9.751	9.797	· 47 .83	9.326	. 10.06	=160+70
	8	2 * 00	0.01	·=4 - 958	9 • 594	: 31.06	9.493	1.52	-151,28
	9	4,00	10.01	-0.686	9.731	. 15.86	9.533	#8.08	-146.45
	. 10	6.00	0.0101·	3.421	9.902	3.25	9.007	P13:94	-140718
	11.	8.00	0 . 01	7.426	10 - 169	-5.78	8.232	-17,84	-132488
	12	10.00		:12.179		-9-14	7.965	:=23,55	-126.39
	13	12.00	0.01	16.129		.=18+12	6.084	1=21.66	=125 = 53

ORIGINAL	PAGE 19
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VOUGHT LOW SPEED	MIND	TUNNEL	TEST	630
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DELTA DATA

25 المنتب

ID.NO. 74

:(RUN 74-RUN 32)/ 1+00

PNT	ALPHA	. PSI .	. L/Q.	*	0/6	PH/G	SFAG	! RM/0	YHZQ	<u> </u>
4,	=12+00	·· =0 +76	++600		6+683	.=25+39	=0.074	5.41	32.16	
2	-10.00		1 3 - 1 4		6.515	=17.06	0.400	-3.04	29.05	
2		1 -0-76	2.723		6+527	-10-70	1.024	+ -2.52	21.67	1 2
	-6-00	-0-76			6.516	-14.23	1.580	4-119	9750	
5	-4-00	-0-76	1:336	N.	6.398	-14-39	1.623	-3.83.	3.36	- 1935
6	-2.00	· =0+76	. 1.732		6+080	-15#89	1.897	=5+14	· =2.21	
7	0+00	· #0+76	0.932		5 • 938	=12+76	1.648	=2.65	-2*69	
8	2+00	0-76	1:592	•	5 • 655	=11.470	1.226	€3+6∃	0498	
9		· -0+76	0.167	ŧ	5+14	=11107	1.297	- =5.79		4 - 1
10		~ =0.76	-0.201	4	5-116	-9.71	1.259	. #5¥30.		
<u> </u>	8.00	·: -0-76	-0.418		4.871	- 49.42	1.479	· •7.58	10975	
_ 12	10.00	7	-0.848	•	4.599	=9.80	1.158	-6.50	11.68	
13	12+00	" #0 #76	-2-173		4 4 4 5 2	.=23 - 82	1.094	-5.42	16794	

OR	IGINAL	PAGE	S
OF	POOR	QUALI	TY

n +wath +T 200 MG to 25 WES Fr to A 1F to 5 9

	٠	ORIGINA OF POO	l page R quali	iy Y	A-220			
	y gugh y	LOW SPEED	WIND TU	INNEL :TES	iT 630			
		.DELTA	DATA					<u></u>
		ID.NO.		/ 1.00				
		11/23/81	1303					
	AXES DATA: C .ALPHA ::PSI		MES DAT	A-CORREC	TED SINGL	er en de la de en la e ntrala en la la de la dela de la dela della de	ATAG TF	
	-12-00 = =0-74 -10-00 = =0-76		6 • 619 6 • 740	;=26 ×53 =35 • 27	20 E∙0 20 E•0=	7+03 7+04	12+07 . 11+99	
	-8-000-76 -6-000-76 -4-000-76	. 2.758 . 1.856	6.674 6.693 6.485	-19-89 -18-83 -17-55	-0.231 0.033	1.22 *2.47 *3.07	11+6+ '6+21 5448	
6 7	-2.00 · -0.76	1.238	6 • 409	=15+99 =14+20	0.627	=3.51 =0.54	0 • 17	<u> Marie de la Companya de la Company</u>
8 5 10 41	2-00: =0.76 4-00: =0.76 6-00: =0.76 8-00: =0.76		5.935 5.451 5.407 5.058	=12.53 =8.45 =7.42 =6.26		=1.34 #1.97 =1.52 =3.97	=0 473 • =4 772 • =5 476 • =8 852	
12 13	10.00 " =0.76	-1+147	4.690 4.930	-7+49 -16+22	1.421	-3.68 -3.24	-7×53 -0+64	and Anna Anna Anna Anna Anna Anna Anna A
*								
	·						ria de la compansión de l La compansión de la compa	

. VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

- ID.NO. 76

(RUN 76=RUN 36)/ 1 000

MI	NO	AXE8.	A	TA C	ORR	ECTED	AHES DAT	A-CORREC	TED SING	ALE SUPPO	RT DATA	
PN	T.	ALPHA	<u> </u>	:PSI		L/0	p/9	:PM/0	SF/Q	: RM/Q	. AWA	
		=12.00				4+640	6+866	:=30+85	0.836	9+35	4 4 1 8	
	2	=10:00				3:940		=32 - 52	0.143	7 • 08	6 • 57	······································
	3						6.615	-18.75	-0.132	5.38		
	•	6-00	ŧ. I	-0-76		1-807	6.656	-4.39	-0.035	1.02	∴7 *23	
	5	-4-00	17.	-0.76		1.840	6.628	-18.36	0.222	-1-26	2.86	
	6	-2.00	, ,	-0.76	•	1.747	6 • 291	-19+65	0.622	· =0 +56	=1 +03	
	7	0.00	. (-0.76		1:588	6 . 192	=19:01	0+666	1 + 40	- =2137	
	8	2.00	e > 1	-0+76		0 622	5 . 822	=15.50	0.531	1 • 49	-4-19	
	9	4.00	99. 1	-0.76	13.11k.?	0.458			856.0	0.03	-6.88	
	O			-0.76		0.083		+11+10	1.062	+0.00	6-65	
 In the first February Section 34 April 198 	1	8.00	Sec. 25.				5.278	-11.66	1,478	-1.37	CONTRACTOR	
	2	10.00	_			0.931	4:789	=12 + 45	1.365	-2.06	-7.06	<u> </u>
	3	12:00		-		1.660	4.906	-21.10	0.885	=1.49	=5.65	

original page 13 of poor quality

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. AGRICHL FOR SPEED MIND THUNER LEST 630

DELTA DATA

ID.NO. 77

(RUN /77-RUN '37)/ 1-00

	INI	D AXES.	DATA: G	RRECTED	AMES DA	TA-CORREC	PORTE DET	E SUPPOI	RT DATA	
	PNT	ALPHÁ	PSI	. L/0	0/9	PH/Q	SF/G	RM/0	YM/Q	
	i	-12.00	. 0.03	1 3.222	6,452	#324 •01	-1.928	10+86	. 21+84	
	2	-10.00	0.03	3 . 164	6.363	:726+89	2.095	7 • 96	. 18 ed3	
	3	-8.00	0.03	2:178	. 6.425	1-25.61		8.73	. 15-73	
		-6-00		1 800	6.374			4.84	.7455	
	5	-4-00		. 16390		'-26.55	-0.699	3.52	4761	
	6	-2.00		. 1.422	6+056	-22.55	-0.325	3+46	·1 ×43	
	7	0 + 00		1 • 157	5 + 9 4 3	≈22.20	≈ 0.377	4+24	1 .42	
	g	2:00	7	0.774	5 + 653	.=22+89	=0.345	5.02	2 - 86	
	. 9				5.483		0.020	2,12	-0-20	
e di la	10				5.130		0.175	.3.31.	. 40759	
	11	*		CONTRACTOR OF THE PARTY.	FEE*#			.0.99	-0.05	
7.7.	12	10.00		=0.298	4.709	=13.74	0.445	0.87	1+61	
Same?						· ·				
na e ^a	13	12:00	0.03	±1•281	4+462	=13*13	0.194	1.51	3.56	

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. YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

110.NO. 78

MUN 78-RUN 361/ -1-00

			N 9 19 19 19 19 19 19 19 19 19 19 19 19 1	AMES DAT	A-CORREC	LED STANE	EISUPPOR	AND CONTRACTOR	ia.
NT	ALPHA	PSI	. L/G	D/G.	PH/G	SF/Q	RH/Q.	YM/Q	NA THE RESERVE
1	-12.00	0.05	. 4.437	6+548	:=21 <42	#1+03#	7+19	16+74	
2	a10.00	0.405	3.524	6.331	=28+20	=1,631	5-75	20-10	
3	-8-00	0+05	2.014	6+051	18+05	-1.107	6.77	15:36	
.	-6+00	0.05	3.846	. 6.252	-6.38	and the second control of the	40.6	79.11	
. 5	-4:00	. 0.05					The state of the s	* ÷52	
6	-2.00	.0.05	1.810	5 • 855	.=20+74		3+74	1 > 94	
7	0.00	E0+0	1.422	5 • 725	=18.66		4 + 65	3 * 70	
8	2:00	0 405	0.750	5 + 354	=13-72		4.55	2.18	
9	4.00	0.05	10.584	;·5•233	-11.62		.1.69	3,06	
			0-184	* 4.923			19.91	3-16	
11	5.00	0.05						5737	
12	10.00	0.05						5,08	
	12.00	0.05		4.334	-19.09			5 4 6 8	
	1 2 3 4 5 6 7 8 9 10	1 =12.00 2 =10.00 3 =8.00 4 =6.00 5 =4.00 7 0.00 8 2.00 9 4.00 10 6.00 11 8.00	1 =12.00 0.05 2 =10.00 0.05 3 =8.00 0.05 4 =6.00 0.05 5 =4.00 0.05 7 0.00 0.03 8 2.00 0.05 9 4.00 0.05 10 6.00 0.05 11 8.00 0.05 12 10.00 0.05	1 =12.00	1 =12.00	1 =12.00	1 =12.00	1 =12.00	1 =12.00

original pace ic of poor quality.

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. VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 79

((RUN 79-RUN 35)/ 1.00

11/23/81 1303

	VM/Q	tm/Q	SF/Q	PM/G	D/8	_ 'L'/9_	PSI	ALPHA	DNT
			<u> </u>						
	18405	4 + 26	~0.862	19+59	6.099	· 4 • 568	. =0 :02	-12:00	1:
	20.65	4 = 46 :	=1.660	5 . 52	6 • 297	367.45	#0 #02	-10.00	2
	15.96	3.23	-0.821	P19 443	6.259		* =0 402	-8-00	3
	₹7 ∗9 6	1.70	-0.388	2-20-04	6.568	1.825	70.00	-6-00	
	3+62	1940	0.374	-19-55	6.151	1.297	O KO2	-4-00	
, , , , , , , , , , , , , , , , , , , ,	1 -52	2.63	0.496	-16.74	· 6 · 009	1 • 214	.0.02	=2.00	6
	3 + 49	3 +89	0.041	-15+60	5 + 7.64	0.910	. m0<02	0.00	7
	4812	4.35	0.028	=10 - 16	5 • 435	C • 325	- =0 02	2.00	8
	3647	1-43	0.333	-7.73	5 • 151	6.282	·· -0.02	. 4.00	9
	5-00	2.85	0.360	-6:17	5.005	0.031	1 =0.02	6.00	10
	5799	1.62	0.716	1 -6 -12	. 4.757	-Socao	0.408	8.00	11
	9+79	1 . 25	0.653	=7 · 66	4 • 434	-=0∘60g	=0<02	10.00	12
	8.51	5+46	0 + 177	=13+64	4 • 658	1.551	·· #0.02	12:00	13

OR	IGINAL	PAGE	S
OF	POOR	QUALI	γY

A-225

		* -														1.0				
	21.34			1 -4:1	4 4 4	- C	LOW			_			1		دنست د	i caracteria	and the same of			
			· · ·	/ FIT I		•		. 1966		—		NIT.		1 1			1 (2)	₩.	40	^
					-					_					1		E. 3	4 .	8.5	.
1.7	,					r .	and the second of the		-			3.00		-1-4		· ,	44.00		_ —	•
				• •			100	***			1000				- 1	141		,		
							2010/01/2015													
			100				515 KIND				 4.17 			2 *		4.1				
 								Andrew Contractor												

DELTA DATA

ID. NO. 80

(RUN -80=RUN :32)/ 1.00

. 11/23/81 1303

PN	7 A	LPHA													
				PSI		/0.	· p/G		PM/Q	8F/	/0	: RM/Q		YM/Q	
	1 -1	2.00		-0 - 01		•672	6.3	19	:=21.29	=1.7	799	3-1		36+46	
	2 -1	0.00	3. 4	-0,01		:301	6 • 4	11	-18-49	≈1.6	§ 4 5	5 4	7 :	28:41	
				0.01	2	.079	6 • 3	25	-15 -63	~ O.C	166	6.6	5.	-3717	X
	4 -	6.00	. 🙀 🛎	0.01	2	1186	. 6+1	60	:-18.73	0.8	55	. 4.3	3	-2"90	
	5 -	4.00	6,	0.01	. 4	.563	. 6.0	66	-19-02		6.7	4.3	3 *	-1753	
	6 -	2.00	-	0.01		• 7.69			-20.28			3.0		-2 <23	بقب والنظ الترييب في مناب تناف والمناف
	7 -	0.00	۱. 🖷	0.01	1	43E:			=16+60			3.5	1 ,	= 0%38	
	8	2.00	٠. 🖷	0 4 0 1		856			=14:37	-, · pa		2.1		1 + 44	•
	9	4.00	**	0.01	£ 0	.548	5.1	48	-12:06		362	0.9	0	2177	
	o	6.00	100	10.01	. 0	.291	4.9	51	-10.83		90	O.8	3	4.95	
/**· 💃	1	8.00	ŧ: .	0.01		.179		39	grant and and the same and		581	· =3.1		6707	And the second of the second o
- (- 1		0.00		0.01		.360			-10.96			2.7		3 * 13	
1		2.00	•	0.01		283			-16+25			1.6		3.91	

A-226

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

71D.NO. 81.

:(RUN 81-RUN 38) / 1:00

WIN	D AXES.	DATA C	ORRECTED	AMES DAT	A-CORREC	TED, SINGL	E SUPPO	IRT DATA	
PNT	ALPHA	PSI	. LL/B.	`p/€_	PM/G	SF/Q	RM/Q	' YM/0	
1	-12+00	-0.400	: 3.321	. 6+376	-29.16	-2.720	7+05	33#80	
2	=10:00	. 0.00	2.988	6.267	-30.10	-3.036	4.54	35,71	
	-8.00	1.0.00	2.042	6.252	25.23	-2.393	4.28	28727	
	-6-00	0.00	1.755	6.163	-21:77	-1.65#	3.02	14.76	
			1.253	. 6 - 126	-23.49		4.06	. 10.02	
<u> </u>	-0.00			5 • 9 4 7	.=22.33	=0.718	3+64	4+20	
	0.00			5 4 683	-23.40	=0.666	4.22	· =0.438	
,	2.00	0+00		: 5,418	.=24 . 25	-0.728	4.01	· =1 •39	
		0.00				-0.463	1,19	-2.11	
					-19.08	-0.074	2.44	70.61	
		0.00				아이트 중 한국 학생 때	-0752	and the second second	
12				4.550	-14-44	0.283	-0.82	-2.27	
13	•			4.327	=12.69	-0.595	2.96	-1.48	

A-227

YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. :82

(RUN 82-RUN 39)/ 1.00

11/23/81 1303

7	MIND AXES DA	LTA: CORRE	CTED AMES	DATA-CORRECT	ED SINGLE	SUPPORT DATA

	PNT	ALPHA	PSI	. L/0	D/G	PM/G	SF/Q	C RH/Q	YH/Q	
		<u> </u>						- N	•	
	1	=12+00	-0402	: 2.237	5 • 823	.=22+14	-2.312	. 14+98	. 19:52	
	2	-10.00	- =0.02	1.882	5 • 779	-22.02	-2.506	11.66	17797	
	: 3	-8:00	10 00 02	1.479	5.870	:-25.76		8+35	21.71	
		-6-00	0-02	1.153	# 5.818	-26177	:-2.053	3.40	25.47	
	5	-4-00	50.0=	0.722	: 5.853	:-29.16	-1.509	.2.08	. 15478	
	6	=2.00	-0.02	0.378	5.562	-26+94	-0.892	0+76	7.21	·································
	7	0.00	• - 0 •02	0+031	· 写《411	26.98	= 0∙883	2 4 4 2	5 = 03	
	8	2.00	=0.02	-0.091	5 * 145	26.73	≈0.916	1.95	4*60	
	. 9	4.00	4 -0 .02		5.040	28.55	-0.530	1,31	2745	
	10	6.00	0.02	-0.531	4+735	27 .39	-0.223	0.61	· =3 k13	
	11	8.00	0.02		. A.648	:-27:15	0.099	· •0.77	-3.86	
	12	10,00	-0:02	-0.517	4+411	:=27+80	0.344	· #1+44	. =4.62	
•.	13	12.00	·; =0 «02	#0.732	4 * 250	1-27075	0.339	#3.06	· #7474	

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original page 13° of poor quality

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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 183

:(RUN: 83-RUN: 40)/ 1+00

. 11/23/81 1303

			7								
	NT	ALPHA		P31	L/Q	Ø/G	PH/0	: SF/Q	I-RM/G	<u>ાં :</u>	YM/G
	1·	-12+00		0.400	2 - 441	5 • 442	:=26+13	-3.672	. 14.37	;	21.61
	2	=10:00			1:902	5 • 637	:-25-13	-3.450			27.79
	3	-8-00	1 15	0.02	1.389		-26 -54			:	28 423
		-6.00	i vi 🖷	0.02	1.160		:-29.11	7.00		cti. Se¥	19.63
	. 5	-4-00	, 54 · m	0 402	1 - Q56	5.709	1=30 -46	-1.521	1919		39.61
	6	-2.00	1. 🗯	0 . 02	0 • 788	5 • 493	=31 : 67	-1.067	2.69		5+20
	7	0 + 0 0	=	0.01	0 + 494	5 + 184	.=27 <52	=1.396	3.57		7.441
~~**	8	2 + 00	·: =	0 +00	0.397	5.208	=31 • 13	-1.213	3.36		0498
	9			0-00		· 5•136	:-28-29	-0.816	3.79	*	-1 €83
	10	6.00	į š ,	0.00		**822	1-27-85	-0.457			-6-83
	11	8.00	P	0 = 00	-0-30s	· 4.507	:-27 +19	=0.241	1.33	*	=2.55
	12				-0.524	. 4 4 3 3 9	.=23+45	0 . 146	=0+60		-3+39
	13	12:00	, ·· 🗯	0.01	~0 ₹7.4 5	4 • 13 4	=20 +54	0.302	=2.03	•	-7 • 41

ORIGINAL	PACE	S
OF POOR	QUALI	ŢΥ

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yought low speed wind tunnel test	
	430

DELTA DATA

10.NO. 84

(RUN 84-RUN 41)/ 1.00

PNT	AI DUA	:PSI	1.70	6/0	P#/G	: SF/Q	PHZG	' YM/G	
	AMPITA		, 8, 4,		THE WAY	· 35/4	A. B.O.		الفرمان والمالية المالية المالية
4:	=12.00	. =0.01	: 2.265	5 • 698	=26+04	-3 .582	. 15*58	11+10	
ž	=10.00	# =0 e01	* **771	5 • 669	=27.61	=3 . 265	. 13.37	. 12+80	
3.	-8-00	-0.01	1.418	5.678	:=29 (52	:-2.632	. 11:23	13.28	
	-6.00	-0.01	1.1.086	5.877	-28.49	-2-017	7.34	-6-14	
Š	-4:00	· =0.01	0.732	5.519	-25 -92		.6.31	2.15	
6	#2.00	-0.01	0.283	5 4 4 6 4	.=27.68	=0.682	5.41	1 =1 945	•
7	0.00	-0.01	0.046	5 + 255	:=25+26	=1.014	6.91	-2.97	
8	2.00	· =0.01	=0.049	5 - 117	=24 - 80	=1.171	6.99	· *2 . 65	
e e	* # OO	# =0.01	-0.266.	The state of the s	.=25 .81	-1-156	5.83	-3488	
10	6.00	#13####			:-24+02	-0.944	4.94	#3%15	
7	8.00	7 -0 -01	-0.261			-0.712	3 ÷ 10	-2706	
12	10.00		-0.269	4.253	29-02	=0.520	2.21	-1.98	
13	12,00		-0:373	4 - 144	=27 -82	=0.399	0.81	-1-65	

VOUGHT LOW SPEED HIND TUNNEL TEST 630

DELTA DATA

10.NO. 85

(IRUN 85-RUN 49)7 1-00

				11/23/8	1 1303					
•	DAIN	AXES	DATA : CO	PRECTED	AMES DAT	A-CORREC	TED SINGL	FISUPPOR	T DATA	
	PNT	ALPHA	:PSI	. L/a.	9/0	PM/Q	SF/Q	RM/G	YM/Q	
	1	-12.00	· =0.01	: 2:189	5+970	-23+20	-2.281	. 15+17	18.26	
• • • •	· · · · · · · · · · · · · · · · · · ·		-0.01	2:012		-26 482	-2.112	12.30	13.35	V 3
		-6:00	-0.01 0.01	0.889	6.008	;=26.93 :=23.36	-1.884	3.60	20.50 13.06	
سنسي	6	-2.00	· =0.01	0.085	5+660	=26 +55	-0.989	0 .38	. 11 • 13	
	7	2:00		#0 • 254 #0 • 403	5.342	-26 · 17 -26 · 45	-1.192 -1.042	3 • 02 0 • 77	. 12×13 8•09	the Albertan Street Control of the Assessed
	9 10		-0.01			-25.06		0 + 89 0 + 88	3 - 04	
	11	8.00	# #0.01	.÷C.889	4.612	:=24.83	=0,063	-0.21 + =2.86	· =1*68	
	12		#0.401	=0.796	•	=24+09 =25.94	0+170	3.48	-1×77	

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venin no ಕಾರ್ಯ ಕಾಷ್ಟ್ರಿಯ ಪ್ರಾಥಾಗಿ ಸಂಪೂರ್ಣ ಸಂಪೂರ್ಣ

Cases.		. 1	VOUGHT	LOW SPEE	t dath c	UNNEL TES	T 630			
taras interes interes		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1444-) - 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 	.DELT	A DATA	itu. basin maraja mara	and and an and	ant i na tribu, maraillai nin		
	 	:	· · · · · · · · · · · · · · · · · · ·	/ID.N	386	er e			هوان بهروان الناسط المساور والدائد التي ويوران ا	
		; C	,	HRUN .86	-RUN :52	1/ .1.00				
		THE STREET OF POSICION AND A		11/23/8					•	
	WIND	AXES	DATA	CORRECTED	AHES .DA	TA-CORREC	TED SING	LE BUPPE	RT DATA	name of the second seco
ent the desired	PNT	ALPHA	PSI	. 6/8			\$F/Q		77 2 13 A	e
			i · =0 «0 =0 •0		6+455 6+458		=3.344 =3.516	3+14	· 42467	
den den der der den der	1 35 +	-8 .OC	#:#0 ₹0 #: #0 ₹0	2 3.082	7 4-186	:-28.93	-2.981	2:27	24.82	
	<u> </u>) · =0 •0				-1.368	1.91	12+69	
	7	0 + 0 0) + ₩0 ¢0	2 . 2:155	6.108		-1.137 -1.202	1.97 3.96	. 11 +33	
	<u>8</u>) - =0 <0		5 • 715		-1.418	3.92	12:31	
e e e e e e e e e e e e e e e e e e e	10 11	6.00	4 4040		5.163	-14-43	-1:358 -0:637 -0:148	3.22 2.68 1.0.28	10446 6472 5439	
-	12 13	10.00	=0.0 =0.0	2 0.951	. 4:664	-10.02	=0.063 =0.740	*1+14 3+06	3-69 -0-46	market and the second second second

original pace ij of poor quality.

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AGRICAL FOR SESED KIND INNEF LEGE 930

DELTA DATA

ID.NO. 87

(RUN '87-RUN 54)/ 1+00

PNT	ALPH	A :	PSI	. L/G	p/G	.PM/Q	SF/Q	RH/G	YHZO
								المنظمين المنظمين <u>في في في المنظم المنظم</u> المنظمة	<u> </u>
i	-12.0	o ·	#0+Q4	* 4.864	6 • 5 4 6	-32 -12	-1.424	13.55	. 11+15
· a	=10.0	0 1	-0-04	3 . 895	6 • 225	-28.37	m1.563	9 - 29	19 k38
	-8+0	Ú H	-0.04	2.699	6+100	1-22-86	-1.018	. 11.24	.6.46
	-6-0	0 1	-0-04	2.424	6.139	;=21+84	-0.037	77769	* -1.1
. 5	-4.0	0 "	-C.O.	: 2:366	6.095	:-21 :67	0.117	5,35	f * 4*25
6	-2.0	Q·	#0+Q4	. 10.949	6.024	=18+75	0.314	5,37	-3.31
7	0 • 0	0 ·	≈0 ±04	1.802	5 . 902	-15 *22	-0.093	5+59	=4+41
	2.0	0 .	-0+04	1.483	5.551	=12.98	=0.493	6.57	=1 ×83
1 9	→ *0	0	-0.04	1.287	5.306	-9+64	=0.285	5.40	* =3.00
10	6.0	0	-0-04	. 0.710	5.121	-9-54	0.077	4.02	+ - 2∓65
<u></u>	8 7 0	Q +8	-0-04	0.674	- 4 · 832	× =8+41	0.502	0.46	-2:29
12	10+0	0	-0+04	0 • 1 93	· 4+584	. #9 + 26	0+496	-0.50	-1 -02
13	12:0	0 '	-0+04	m0.812	· 4 • 250	=15+47	0.003	1 +53	0+14

VOUGHT LOW SPEED HIND TUNNEL TEST 630

DELTA DATA

ID.NO. 88

(RUN 188-RUN 155)/ 1+00

. 11/23/81 1303

				, ,	· -				
-	WIN	D AXES	DATA : C	GRRECTED	AMES DAT	TA-CORREC	TED SING	LE SUPPOR	TIDATA
			Charles bander in the second					e Sangliain i dengante Otto oli saine valaini	· senfol · al Con · Ose · Say · sell · · · · · · · · · · · · · · · · · ·
•	PNT	ALPHA	PSI	. L/G.	10/G	PM/Q	SF/Q	RM/Q	YM/Q
								as desirab	40
	1:	-12.00				=32 +95	-1.154	9.70	13+00
_	2	-10+00			6 • 222	:=26:37	=1.446	9 • 79	. 13+27
_	3	-8.00	-0-04	, 2.987	6.278	-26.84	-0.802	10.08	.6.02
		6.00	EG:0=	2.547	6 • 207	-22417	0.106	76:41	-3486
	5		-0.03			-22.86		7.24	-6707
-	6	-2.00	-0.03			-19+08	0.240	3.80	- =4+89
	7	0.00	-0.05			-16:30	-0.061	4.92	. =3.40
	8	2.00) - =0 a05			-13.43	#0.359 °		=1 =40
-	9	4.00	-0.05					4+09	1.493
	10	6.00	-0.05	0.426	5.052	-13.80	. 0.146	3,48	-0.68
	/ 11	8.00	. =0.05	0.218	. 4 -892	-12.54	Var. 1	. =0.18	· =0*47
ij	12	10.00) - =0 +Q5	-0.147		=13+66	0.515	· =0+65	-0.58
	13	12:00	· =0.05	-1.132	4.512	=18:87	0.154	0.56	0.50
								-	

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, MOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

10.No. 89

:(RUN 89-RUN 56)/ 1.00

WIN	AXES DATA :	CORRECTED	AHES DAT	A-CORREC	TED SING	LE :SUPRO	RT.DATA
PNT	ALPHA (:PSI	. L/8	D/G	PM/G	∷.8F/Q	! RM/Q	: YM/Q
1	=12+00 ·· =0+0	5 : 5 + 46	6 • 175	=31.72	*1.323	9 - 0 4	. 13431
2	-10.00 · -0.0	5 4.495	6.362	=35 - 85	~1.576	9.93	. 10.81
. 3	-8-000-0	5 . 2.716	6.408	-24.13	.52P.0=	.7.64	4 695
	-6-00 4-0-0	5 . 2.443	6.347	-23.79	-0.292	6.48	* *1*20
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	60 10 2 1 Table 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-20-52		3.43	-4.47
6	-2.000.0		6+168	:=20.11	0.142	3+15	-5 < 28
7	0.00 - =0.0	-	6+020	=16+89	=0.268	5,35	· =2.58
8	2.00 . =0.0		5 • 731	=15.57	-0.405	4+85	-4.31
9			5.447			3.51	-2:65
10	6.000.0		5 • 157	-12.28	0.256	2,63	-1767
_ II	8-000.0			-11.72		0.10	-2.6A
12	10.00 - =0.0		4+614	=13.40	0.583	. =0.89	· =1 •11
13	12.00 - =0.0		4.428	=17.35	=0.065	2+20	1.35

original pace is of poor quality

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F VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

10.48. 30.

TRUN 90-RUN (57)/ 1-00

	HIN	PAXES	DATA: C	BRRECTED	AMES DAT	A-CORREC	TED SING	LE SUPPO	TATA DATA	
en e	PNT	ALPHA	PSI	LZG.	D/8	PM/G	SF/G	! RM/Q	· YH/Q	
	1	-12+00	·· =0.05	5.440	5+997	=32×98	-1.064	8.97	6∢58	
	2	-10:00	-0-05	: 3.825	6 - 172	-32.36	=1.684	8.49	14040	
The second	3	-a-00	-0.08	1.965	6.375	-21.84	-0.863	-8460	77.60	
	· •	-6.00	-0 -QE	1.973	6.313	:-23.60	-0.197	7717	1.469	
	5	-4-00	-0-05	2.274	6.304	-24×73			10.6-	Marie de la companya de la companya La companya de la co
	6	-2.00	-0.05	1.994	6+157	:=22+46	0.370	3.99	· =4 483	
	7	0.00	-0.05	1.670	6.039	=19.84	=0.052	5 - 55	41.85	
	8	2.00	=0=05	1+461	5+764	=17.58	-0.191	4.51	. #2.36	
	9	4.00	0-05	1.185		12 448		4.44	-2-00	
	10	6100	-0-05			-10-75		4:18	-0-96	adila 19
, see	11	8 .00	0-05	0.443		and the second of	" "	1,30	* =1472	
• ~ (:	12	10.00	0.05		4.668	@13.10	0.399	0+40	0.06	أراحة التقديمين المقاصد المهاري والمقديين
4	13	12:00	-0.05		4+360	-18-55	0.095	1.28	2.05	

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. VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 91

(RUN \$1-RUN 58)/ 1.00

	ID AXES	DATA : C	BRRECTED	AMES DAT	A-CORREC	TED SING	LEISUPPO	RTIDATA	
₽N	r ALPHA	:PS\	. L/8.	D/G	iPM/G	* SF/G	₹ RH/Q	C YMZQ	
) +t ==0 ×Q3		6 • 271	=32.76	-2,216	5+23	35*23	
	=10.00	ED. O- 11	4.201	6.593	:=28.64	-2.539	1 - 99	35+84	
	-8.00	-0.03	2.541	6.230	11-89	-1.469	5.10	; 23-25	
	-6-00	E0203	2.902	6.267	:-23.46	-0.487	2.71	8727	
	5 -4.QC	1 - =0 -03	2.701	6 . 045	:-21.51		-0.91	3758	
,	=2.00	1 =0.03		5.936	.=20+30	0.281	0.74	3,06	
•	7 0.00	EQ-0=	: 2.720	5.739	-18:52	■0.04 4	2.50	4.92	
	2.00	E0+0= ··		5 • 5 4 0	=16.11	-0.440	2.34	6-40	
	4.00	Q.403		: 15.314	-14:45	-0.51C	1.28	9.41	
1	6.00	E0.03		4.797	-11.94	-0.050	2.13	. 31/17	
· ·		0-03		4 - 829	.=10.39	0.503	0.61	6.65	
1	The state of the s	E0.03		4.410	-11.55	0.733	-1.92	2+00	
				4.320	-15+24	0.391	#0 +66	4+30	

original page 13 of poor quality

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٠	VOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630

DELTA DATA

10.NO. 92

TRUN 92-RUN 591/ 1-00

. 11/23/81 1303

WIND AARS	DWIN ! COUNTRICED.	WEST OF THE CALLED STUDIES SOLEON CONTRACTOR	į
	The season of the season of the contract of th	the control of the co	
The second se		ray in the contract of the factor of the fac	
PNT ALPHA	. ;PSI . L/Q.	D/Q PH/Q SF/Q RH/Q YM/Q	

. ' منيسستسم نس	PNT	ALPHA	. PSI	. 4/9.	0/9	PH/G	SF/Q	RM/Q	. ANNO	
	1	-12:00	. 50.01	· 5.374	6.300	:=30 •22	:=2.281	5.41	34.36	
				4.560		-37 - 47	=2.594	3.96	. 37 * 72	
	3	-8+00	" -0 + 01	1 3.515	6.045	:-24+67	.=1.327	•5+++	. 18-30	
	4	-6+00	-0.01	2.864	6+177	:-23.72	-C.524	3:12	77,22	
	5	-4-00	10 -0 -01	2.630	6.123	:-21.22	=0.203	0.79	1.90	الماسينينية
<u></u>	6	=2.00	. =0.01	2.254	5 • 996.	-19.51	=0.261	2.36	2 - 92	
	7	0 • 00	- =0.01	: 2.486	5 • 687	=19 -12	-0.285	3+00	+.03	
	8	2.00	<u>.</u> ₩Û∗Û1	. 2.727	5 + 5 6 9	=17.48	=0. 528	8+48	6+51	فخافصونيسن الإسيانة
(4) 	9	4-00	" -0+01	. 1.463	5+347		-0.326	1.07	9 • 39	A. 151 T
	10	6.00	# #G.Q1	1.191		-11.66	0.007	0.45	6 613	.,
300 0.	11	8.00	-C.O.	0.820	4 . 773	-11-40	0.464	-1.83	7732	: :
-	12	10.00	-0.01	0.761	4 • 677	=12.01	0.710	#3.91	3 47	
	Ei	12.00	· #0.01	=0.408	4.318	-16.11	0.226	≠0.09	3 • 39	

ORIGINAL PAGE 18 " OF POUR QUALITY

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: YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 93

(18UN 93-RUN 66)/ 1.00

		and the Control Street Control of	a serv		C CO OAII W	E RUPPOR	CONTRACTOR	
T ALPH	A PSI	. L/G	D/G	PM/G	: SF/Q	! RM/Q	YM/Q	
i =12+0	0 =0 +01	5 • 475	6+368	:=31+74	-2.051	3.56	34+74	
2 =10.0	0 0 1 01			- , ,		3.436	31.70	
3 -8.0	00:01					2.74	14.06	
				Control of the Contro	No. 20 and the result of the contract of		74405	
5 -440	00.01	. 3-135		A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	A Company of the second of the		4-16	
6 -2.0	00.01	. 3.267	5 • 816	=23.23		0.25	3.68	
7 0.0	0 4 #0401	: 2.7.24	5 • 438	-19-20	-0.264	2.31	3,35	
8 2:0	0 #0 401	. 2.184	5 + 474	=17 +59	=0.360	2.55	5.21	
9 4 0	00.01	1.627	5 - 190	-13:37	=0.197	1.04	2767	
0 . 6 . 0	00.01	1.381	. 4.960	-12-31	0.094	1,05	.8.20	
1 840	00.01	3.002	4.812	-11.51		1.07	6.03	
2 10.0	00.01	848.0	. 4.551	-12.25		-2.56	5*89	A STATE OF THE PARTY OF THE PAR
3 12:0	0 . =0.01	=0.393	4.361	-16.32		1 .02	8 * 8 9	
	1 =12.0 2 =10.0 3 =8.0 4 =6.0 5 =4.0 7 0.0 8 2.0 9 4.0 0 6.0 1 8.0 2 10.0	1 =12.00 : =0.01 2 =10.00 · =0.01 3 =8.00 · =0.01 4 =6.00 · =0.01 5 =4.00 · =0.01 7 0.00 · =0.01 8 2.00 · =0.01 9 4.00 · =0.01 1 8.00 · =0.01 2 10.00 · =0.01	1 =12.00 :: =0.01 ; 5.475 2 =10.00 : =0.01 ; 4.514 3 =8.00 :: =0.01 ; 3.264 4 :=6.00 :: =0.01 ; 3.264 5 =4.00 :: =0.01 ; 3.264 5 =2.00 :: =0.01 ; 3.267 7 0.00 :: =0.01 ; 2.724 8 2.00 :: =0.01 ; 2.724 8 2.00 :: =0.01 ; 2.184 9 4.00 :: =0.01 ; 1.381 1 8.00 :: =0.01 ; 1.002 2 10.00 :: =0.01 ; 0.948	1 =12.00 :: =0.01 ; 5.475 6.368 2 =10.00 :=0.01 ; 4.514 6.377 3 =8.00 :=0.01 ; 3.451 6.191 4 :=6.00 :=0.01 ; 3.264 6.034 5 =4.00 :=0.01 ; 3.264 6.034 5 =4.00 :=0.01 ; 3.267 5.816 7 0.00 :=0.01 ; 2.724 5.638 8 2:00 :=0.01 ; 2.724 5.638 8 2:00 :=0.01 ; 2.724 5.498 9 4.00 :=0.01 ; 1.627 ; 5.190 0 6.00 :=0.01 ; 1.381 4.960 1 8.00 :=0.01 ; 1.002 4.812 2 10.00 :=0.01 0.948 4.551	1 =12.00 : =0.01 ; 5.475 6.368 :=31.74	1 =12 * 00 : =0 * 01 ; 5 * 475	1 =12.00 :: =0.01 ; 5.475	1 =12+00 :: =0.01 ; 5.475

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YOUGHT LOW	SPEED	CAIN	TUNNEL	TEST	630
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DELTA DATA

ID.NO. 94

.(RUN .94-RUN .65)/ 1.00

WIND AXES D	SATA . CO	IRRECTED	AMES DA	TA-CORRECTE	D SINGL	Z.BUPPORT	DATA
				فالمصنعة وممتشيد تناف	مستسيدة والمستحدة والمستحدة	min min . Mo 1	

PNT	ALPHA	PSI	. L/a,	0/6	PM/Q	SF/Q	RM/G	YHVQ
1		-0.01	5.294	6+268	-31 -52	-2.247	3,57	: 38 × 12
2	-8.00		3.155			-2.279 -1.213	3.86 -3.60	1 34494 2 17909
	-4-00		: 2.776	5.987.		-0.546 -0.346	1.23	
· 7	0+00	· =0+01	. 2:531	5•879 . 5•788	=23+49 :=21 +92	=0.169 =0.381	₩0.45 1.85	2 • 08 2 • 99
	4.00		: 2.042 1.653	5 • 538 5 • 2 • 8	=17×13 =14×42	=0.367 =0.435	2.53 .0.46	3,47 5,40
(10 11	8 - 00		1.244	5.080 4.777	=11.58 =9.41	0.0+2 0.581	=1.37	8.76 .5.60
12		·· =0 < 01	1 • 036 = 0 • 375	4 • 6 9 8 • 4 • 4 7 4	=12~42 =16+90	0+705 0+121	#3+19 #0+06	6+68 4+13

VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 95

CRUN 95-RUN (63)/ 1.00

MINO	AXES.	DATA: CO	RRECTED	AMES DAT	A-CORREC	TED SING	LE SUPP	RT DATA	
PNT	ALPHA	PSI	, L/Q,	p/e.	PM/Q	SF/G	(RM/Q	YM/Q	
1.	=Q+24	-28-00	. 2.331	12+7.82	-64.48	-4.393	1 39+45	7 (37	
2	-Q+24	.=26+00	1 • 175	11+759	-51 +45	-2.914	1 36 63	3 • 92	
3	-0.23	:=24+00		-11-375	*#45 . 51	-2.230	34.68	:129 158	
	-0-22	:-22.00	1-635	:12.376	-47.51	-4.121	30.37	9.56	
5	-0.30	2-20-00	. 1°367	11.909	-42:42	:=3.391	: 27.29	12.96	
6	-0.26	=18.00	0 • 859	11.440	.=37 . 49	-2.550	: 24.41	7 437	
• 7	=0+24	=16+00	0 + 8 2 7	11:191	#32+54	=1.641	. 16 - 54	7 482	
8	=0+24	.#14+00	1.113	11.322	-29 - 37	=1.845	13.10	9.75	
9	-0+24	.=12.00	1.642	11.436	-=41 -48	mi.769	8.58	. 11.75	
10	-0.24	-10.00°	24704	11+836	.=49 .03	-2.923		17:29	
	-0-24		2.929		:-57 - 11	-2-175	0.09	. 18 43	
(12	-0.24	. 46.00	: 2.211	11.977	-55 -20	-1,273	-0.51	. 15,52	
13	=0+23	·: =4+00	1 683	11.959	=54 ×32	-0.111	+1.46	9.51	
14		-2.00	1.877	11.838	-54 - 74	-0.626	0.37	11 403	
15	-Q#24	0.00	1.947	11.748			<u> </u>	9.90	
16		2.00	1.777			805.0	The state of the s		
17	-0.24	4 . QQ	17729	11.611		1.204	-1.86	2.04	
18		6 . 00	1.763	11.827	-50 - 26	2.147	· =6.77	-6:42	
19	-0 624		1.874	11.477	·#49 • 13	2.365	-5.21	=4.68	
20	#0 · 24	10.00	1.750	11.768	#51.24	3.419	·8.96	-10-92	
21	-0.24	. 12:00	1.764	11.754	-48+29		-11-73	-13-30	
22	-0.24	14.00	1 7553	11.851	-46-95	4.890	.=14.90		
23		16-00	1:186	11+348	-32-52	* . 693	:-20,25		
24		18-00	0.691	11.825	=33 *23	5.217	.=25+09	.428+09	
25		: 20-00	0.339	11.862	-32+84	4.884	1=30.71	.=22.28	
26		: 22-00	0.233	12.227	=35+05	4.908	1=34+34	=17.53	
27		24-00	-0.209		40 ×00	.5.113	-36.96		
28		26-00	-0.718	12.773	E4. E4.	- 4.363	·#43 #46		4.1
29		28.00	-0.686	12.894	-49.24	4.389		***	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. 96

(RUN 96-RUN 63)/ 1.00

		MIND	AXES	DATA	CORRECTED	AMES D	ATA-CORREC	TED SING	LE SUPPO	RT DATA	
		PNT	ALPHA	, :PS	. 676.	: D/G	:PH/G	: SF/Q	: RH/Q	YH/Q	
		1	=0.25	5 :=28 ×C	00 - 4*103	13-45	51 =68+64	-5. 603	: 31+90	8 463	
	•	2	-0.25	5 :=26 . C		13 • 01		=4.735		3 55	
		: 3	-0+24	1724×C				=3,685		3.04	
•		4	-0.23	:-22.0					29303	2,63	
		<u>5</u>	-0.31	1-20:0	10 2 7722					20.66	
		6	-0.27	7 =18+0	00 : 2.153	13.10	6 =39+79	-5.646	: 28 . 12	18+89	
		7	=0 + 25	716 ac		12.55		-5.210	: 23.52	18+19	
		8	=0 + 25	5.=14+0		12.43		=4.658	17.79	: 20 + 66	
٠		3	-0+25	1.=12.0				-4.739		: 27.51	
		10		-10-0				-5.085		29.98	
		11		-B.		:12.92		·#4.546			
•		12		=6+(12.88		=3.957		32.43	
	** ***	13		- 1. 200.41.40.€		12.98		=1.984	-2.81	: 22 483	
		14	-0.24			12.81	•	=2.118	-1-16	. 北京・57	
		15		5 40 +(=1.495			
		16		2.(86 :=39.65	-0.004		.6.39	The control of the co
,		17		4.4		12-87		1.248	-4.00	3.75	
	a ing manganan banda	18	-0.25		00 1.916	12.85		2.359	-5.19	· =1 ×73	
		19	=0.25			12.50		3.336	¥7.32	=7.61	
		20	=Q . 25			12.76		4.250	=11,97	.≈13×96	
		21		12.0				4.562	+14.92		
	4.44	22		14.0	0 . 4.508			4.248		-14730	
•	W Section 1	23		16.0				3.726		15:37	
		24		. 18•0	0 1.302	11.97		4,703	:=23.01	-22,42	
		25		: 20 .		12.10		4.572	:=26.12	=19 -72	
		26		: 22.0				4.787	-29+43	-14-17	
-4 50,000		27		2400	0 1.001	13-1			;=32.32	-19-05	
		28		26 • (. Your Superior		4.641	:=33,59		
		29		5 2 2B • 0					:=36.27		

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WOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

110.NO. 97

(RUN 97-RUN 65)/ 1.00

WING	AXES	DATA	CORRECTED	AMES DA	TA-CORREC	TED SINGL	E SUPPO	RT DATA	
PNT	ALPHA	; :P9)	L/G.	D/0	PM/G	SF/Q :	RM/Q	" YM/8	
1	=42.00		1 . 5 . 295	6 1422	-30×73	0.066	1+13	: 20+75	
2	-10:00	0 . 0	1 4.390	6.369	=26.78	=0.061	4.07	. 16+24	
* 3	-6+00	0 . (11 7 3 3 3 1 1	6,360	-22.38	Q.324	.2.91	·5×50	
	-6+00	0 . 0	11 3 3 4 1 6	6 • 165	-22.81	0.596	2.68	0.99	
5	-4-00		1 3.205		-25-10		3.70	2.52	
6	-2+00					0.363	3+25	2 . 25	
7	0.00	0 4 0	1 : 2 632			0.161	4+09	5 * 23	
. 8	2.00	0 . (1 . 2:124	5 • 603		0.046	4.71	6 * 32	-
3	4.00	1 0.6					1.39	8 • 23	
10	6.00					0.081	0.96	. 13-00	
	8 00) O e !	1.378		2 m 1		*1,13	7.39	
12	10.00		(CC) 1)			0.371	F1+78	9+04	<u> </u>
<u> </u>	12.00	•	· .	4.283	=12.10	=0.186	0.10	3012	

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VOUGHT LOW SPEED WIND TUNNEL TEST. 630

DELTA DATA

ID.NO. 98

:(RUN 98-RUN 66)/ 1:00

. 11/23/81 1303

	WINI) AXES	DATA: CC	HAFFLED	WWER DY	A-CORREC	TED SING	LE SUPPOI	ATAULTS	
	PNT	ALPHA	:PSI	L/0.	2/9	PM/Q	SF/Q	: RM/G	. AHNO	
	1	-12:00	0.01	5 + 753	6+378	:=29 +67	0.115	1.68	. \$6+84	
	2	-10.00	0.01	4 575	6.316	:=29.36	=0.077	4 + 45	. 10/37	
	3.	-8:00	0.01	3.529	6.229	.~23·81	0.348	3.20	DE##	
	*	-6-00	. 0.01	3.304	6-148	:=25 ×05	0.496	3.58	· 0673	
	5	-=4=00	0401	1 3 40g		-27 cs	0/369	4.01	-1-51	
	6	-2.00	0.01	3.530	5.305	.=22:80	0.225	3.73	4+27	
	7	0.00	0.01	: 2.858	5 4 6 5 8	=19 +26	0.129	4.53	3 + 7 4	
	8	2.00	0.01	: 2.258	5+442		#0.060	4.52	9 - 15	•
	9	4.00	* -0.01	\$ \$1779	5 . 254	-15.01	0.105	1,53	6.91	
	10	6.00	0.01	1.550	162+	-13-03	7.284	1.01	11719	
7*	11	8.00	. 0.01	105.4		-11.51		* -1.12	7.50	
, ha	12	10 * 00		1.241	4.522	-10.31	0,531	#1 £69	7.11	**
•	13	12:00	0.01	0.563	4.372	=12.73	#0.198	-0.18	2 * 35	

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YOUGHT	LOW	SPEED	MIND	TUNNEL	TEST 6	30

DELTA DATA

:(RUN: 99=RUN 67)/ 1.00

	PNT		.PS1				•	: RM/0		
	1	-12.00	0 • 0 0	2 * 1 4 3	5.920	:=25+24	=1.281	6+14	. 13 • 70 . 15 • 76	
	2	#10·00	0.00	1:521	5 • 755	=23.78	-1.212	6.61 2/79	16.98.	
	∴ ∗ 3		.(.0.00		6.058	-32+93	-1.027	2,92	17.52	
	•		·· -0 -00	1.4242	5.863	:=26+73	-0.770	4.00	13.01	
	5		3.30 × 00		5 • 785		-0.649	4.46	. 11 %73	
	6	-2.00	0+00	0.938	5 • 623	-30.48	=0+579	4.08	10 * 50	
	7		0.00	=0+136	5 • 687	:=23.65	1.529	3.75	7.498	
	8	2.00	the same of the last of the la	0+399	5 • 336	06.62=	-0.700	1.49	5 6 4 8	2: 48 6.003
	. 9			0.198	. 5.+188	31,05	-0.613	1.84	2447	
	10			0.163	* 4.973		-0.432	경화하는 경기 보고 그 것	The state of the second	
	11		:					. ≈0.23° • ≈0.86	7 478	
	12	10.00	0 +00	-0.778	4 8 9 5	:=21 /12	0.040		8.61	
	13	12:00	0 + 0 0	-0.855	4.709	=18 +59	-0+342	-2-20	.0401	
10000	V. S V. S.	r v								
	A (2)									

OF POOR QUALITY

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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NS. 100

!(RUN 100-RUN 68)/ 1-00

. 11/23/81 1303

INIW	D BEEK.	ATA . C	RRECTED	AMES DAT	A-CORREC	TED RINGL	E SUPPO	RT DATA	
PNT	ALPHA	/ ¡PSt	. L/G	: D/9	PM/Q	SF/G	RHZQ	/ YM/g	
_	-12.00	.0.00	-0.486	6.883	3 * 60	5,336	6.21	.=11+64	
	=10:00:		=0 -175	6 • 857	0 • 9 0	5.530	13.62	.=12477	
3	-8.00	-0.01	0.955	7.028	/-26/37	5.383	.4E.S.	-2,88	
	-6.00 t	-0.01	1,208	6 . 805	:=31 .93	5 - 176	0.51	4.89	
5	사람들이 모으려고 하다?		0.686	6.568	30.86	4.703	1 725	1 24 1 1 1 1 1 1	
6	-2.00	The state of the s	=0.361	6.299	.=21.90	4.081	2.32	12.35	وتسوير والمجاولية والوشائسية بطرات تقويل وتشور والمجاور
7	-0.00		=0.486	5 • 984	.=23.34	3.504	1.23	13,52	
g	-	=0+00	=0+866	5 • 766	=22+04	2.409	3 . 05	13 488	
1. The Section 19.	4.00	-0.00				2.097	0.31	10.00	
10	6.00	0.00				2.074	-1.82	9.30	
C \mathbf{i}		-0.400		St. 14 (17)	:=28.76		=2.87	10.20	
12	10.00		.=1.099	5 • 1 0 4	.=22.90	1.347	-2.62	13.61	
13	12.00	0 +00	-1.378	4.991	=21 *43	0.658	-3.13	12.32	

OR	IGINAL	PACE	FG.
OF	POOR	QUALI	77

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та на п**озващения н**а тама на на водет и кога ее филиф

AGRICAL FOR	SPEED	WIND	TUNNEL T	EST 630

DELTA DATA

10.NO+ 101

(RUN 101-RUN 69)/ 1+00

	RT .DATA	E JSUPPO	ED SING	A-CORRECT	TAG. BEKA	RESCIED	ATA CO	AXES D	WING
	· YH/Q	RM/G	SF/G	PM/G ·	0/0	: L/0	, :P61	ALPHA	PNT
	-47+84	18.62	9.636	3.61	7 + 277	: 2+244	0.01	=12+00	1:
	:=33<18	15.21	8.534	=13.35	7 • 3 6 8	: 2 • 434	0.01	=10.00	2
		9.40	8.632	:-29:07	7 376	3.086	.0.01	-8-00	. 3
	:=20.=53	5.98	7. 830	:=28 -14	6.979	2.464	0.01	-6.00	*
	-10×08	6 6 2 6	6.729	1=29.36	6 • 831	2 - 185	0.01	-4-00	
	· =4×83	4 - 15	5,904	:=21 +65	6 • 482	1.570	.0.01	-2.00	6
	1 < 72	3+30	4,993	=15+99	6 - 184	\$ + 47B	0.01	0 + 0 0	7
	7.90	4 - 15	3.840	=18.06	5 - 877	0 . 895	0.01	2.00	, X
1:	. 12:92	.0.26	3.607	-18×33 F	5+644	0.796	10.01	(+)	ğ
	15.74	2.11.	3.601	-17-19	5.510	892+0	0.01	6.00	10
	. 15791	#3.6A	3.402	-17:17	5.228	. 0+393		8.00	11
	13.60	≈ 4+70	3.151	=17+34	5 * 105	=0.111	0.01	10.00	12
	. 10*93	#3.08	2.359	=19+54	5.014	-0.654	0.00	12.00	13

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VOUGHT	LOW	SPEED	WIND	TUNNEL	TEST	630
The second secon		14.9				

DELTA DATA

(RUN 102-RUN 70)/ 1.00

PNT ALPHA :PSI . L/Q D/G PM/G SF/G RM/G YM/G 1 =12.00		HIN	AXE9	DATA: CO	RRECTED	AMES DAT	A-CORREC	TED SING	LE SUPPE	RT DATA	
2 = 10 · 00		PNT	ALPHA	, :PSI	. 4/0.	D/G	PH/G	SF/Q	: RM/9	YMZQ	eries de la companya del companya de la companya del companya de la companya de l
3 -8.00		1;			: 2.616	. 7.+254	3.489	10.029	. 12.61	48-57	
3 -8.00		\$	-10.00	0.00	2 524	7 244	-10.37	8.555	12.51	-32.36	
# -6.00		3	8.00	10.00	3 - 175	7.291			6.74	:-29/57	
5 =4.00		•	-6.00	0.00	2.506				4.24	20 35	The state of the s
6 =2.00 0.00 1.818 6.400 =19.86 5.603 5.15 =4.68 7 0.00 0.00 1.500 6.124 =14.20 4.810 3.75 1.89 8 2.00 0.00 1.002 5.819 =17.70 4.027 3.06 6.69 9 4.00 0.00 1.020 5.606 =13.11 3.722 =0.84 12.08 10 6.00 0.00 0.546 5.381 =15.29 3.602 =2.93 14.69		5	-4-00	0.00				the second secon			
7 0.00 0.00 1.500 6.124 -14.20 4.810 3.75 1.89 8 2.00 0.00 1.002 5.819 -17.70 4.027 3.06 6.69 9 4.00 0.00 1.020 5.606 -15.11 3.722 -0.84 12.08 10 6.00 0.00 0.546 5.381 -15.29 3.602 -2.93 14.69	•	6	-2.00								
8 2.00 .0.00 .1.002 5.819 =17.70 4.027 3.06 6.69 9 4.00 (.0.00 .1.020 .5.606 =15.11 : 3.722		7	0.00	0 • 00				4 11 11 11 11			
9 4.00 (.0.00 1.020 .5.606 -15.11 3.7220.84 12.08 10 6.00 .0.00 .0.546 .5.381 -15.29 3.602 -2.93 14.69		ġ	2.00	0.00				The second of			
10 + 6.00 -0.00 : 0.546 5.381 -15.29 3.602 +2.93 14.69		9	4.00	0.0.00							
그런 제속을 보내는 그런 전 하나 되는 이 있었다. 그에 이 있는 하네 이 아는 그 요요. 이 이 나를 살아 있다. 그 전에 가는 점점 하는 것이 집에 그리고 있는 이 이 이 있는 데이 그 있는 것이 없다.		10	and the second of the second o				10.25 L	3 A 3 A 3 A 4 A 4 A 4 A 4 A 4 A 4 A 4 A	1		
。 2 ⁴⁴¹ 3 1.350 1110.00,20束UD的比较级点UD的比较级点,这个数据数据,这个数据有数据有数据数据数据数据数据数据数据数据数据数据数据		11	2 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	0.00			=16.11	3,541	=4.43	12.70	요한 하이 가장 많이 뭐
12 10 • 00 0 • 00 0 • 274 5 • 120 = 17 • 30 : 3 • 115 • = 4 • 24 . 17 • 14	<u> </u>	12									
13 12.00 0.00 =0.415 4.929 =18.06 : 2.427 =3.35 12.71	1								• • • •	12.71	

OR	IGITIAL.	PAGE	
OF	POOR	QUALI	TY

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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ED. NO. 103

:(RUN-103-RUN 71)/ 1.00

	RT DATA	EisuPPe	ed. Singli	A-CORRECT	MES DAT	RECTED	ATA : COR	BEXA	NIN
	YM/Q	RM/G	SF/Q :	,PM/Q	D/G	L/Q.	, PSI .	ALPHA	PNT
	41+05	16+09	9.434 .	-6-52	6 • 344	0.547	- 0+00	-12:00	1
	-45.38	15757	8.902	-9.50	6 • 293	0.389	0.00	-10:00	ē
	-39 •25	8.94	8.584	-30-49	6.457	7 + 427	1.0.00.	-8.00	a -
	:-27 -60	6.93	7.888	-29.59	6-274	1 258	. 0.400	-6.00	
	-16-30	5.70	6,962	-30,59	6 - 385	1.284			5
	-6 064	2 + 55	5,714	=22+84	6.269	1.371	. 0.00	-2.00	6
	1+94	2 - 19	4.758	=18+03	5 • 777	0.939	0+00	0.00	7
	6+70	1.80	4.016	=20.85	5 • 695	1.078	Ö+00 .	2.00	ģ
		#0.81	3.666	-19.76	5.580	1.061	-0.00		9.
	. 15735	*3.13	3.560	-15+60	5.348	0.699	0.00	- 6:00	10
	The second secon	#5 #43		=16.60	5.276	0.760		8.00	11
Market Parket	. 14+99	#5·43	3.208	-15-39	. 4.920	0.124	.0.00	10.00	12
	11 • 87	-5,35	2.597	-17+05	4.941	=0+352	0.00	12:00	13

original page 13 of foor quality

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VOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID.NO. to4

:(RUN 104=RUN :72)/ 1+00

11/23/81 1303

	ND AXES	DATA L. C	RRECTED	AMES DAT	A-CORREC	TED: SINGL	E SUPPOR	T DATA
PN	T ALPH	A PSI	. L/Q.	D/Q	*PH/9	SF/Q	: RM/9	. Auna
	1 =12+0		: 2+160	6+107	:一位的《高學	2 » 43 6 6	80+0	. 15+44
** **-	2 -10.0	0 0 • 0 0	1.828	5 • 886	FARLEY.		1 +94	16436
	3 -8-0	0 .0.00	1.472	5,839	10,21.038	1.9.5564	* *0 * 21	6.90
	4 -6-0	0 0 . 0	1.561	5 + 7 67	" Gulleting	X . \$68	20001	0.93
	5 -4 .0	0 0 . 00	1.557	: 5.717			6.51	0893
- A Charles - Ch	6 =2+0	0 0+00	. 1.912	5 • 7.95	DESEGO	Sign	**************************************	1.30
	7 0.0	0 - 0 - 0	. 1.881	5.614	:•26 o 50	0.903	∂ ∞63	₽ *13
	8 2.0		1.440	5.424	107 9 P. Total	6.88.60	0.78	2740
	9 4 0			5+384	- 100 A 11 A 100 A	. Olygia.	W1-18	4377
1	0 6.0			5.109	.=2.7.4.	i Com	¥5¥15	4 613
1.0000000000000000000000000000000000000	1 8.0	TO 1570 M. L. COLOR OF THE P. L.		4.920		1.44		3*45
	2 10.0		0.672	4 • 697	=18+37	III PL	-2.95	5.46
****	3 12.0		0+057	4 4 4 6 5	=18+62	1.206	=3.33	·6·51
•				7,700	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	*********		***

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i,	AGL	IGH	T	LOW	SPE	ED.	WIND	TUNNEL	TEST	630

DELTA DATA

.ID.NO. 105

(RUN 105=RUN 73)/ 1+00

	100 CM		*****			TA-CORREC				
and the second	MI	ALPHA	:PSI	. L/O.	· p/G	-PM/G	SF/Q	RM/Q	YM/Q	
	克	#12.00	0.00	: 2.567	5+887	:#33 • 88	1.632	=0.80	: 20.41	
	ž	710.00	- 1	1:979	5 822	1=28.21	1,125	1.21	. 16 .22	
		-8.00	0.00	0.780	5.597	:=21.86	1.356	* *1+49	5.45	
	. 👆	-6.00	0.00	1.438	5 . 749	-28.44	1.435	=1.03	3+70	
	i 5	-4-00	10-00	1.678	5.777	:=29.45	1.276	-0:07	2.62	
	6	=2.00	0.00	. 1.870	5 - 7.72	:=28.21	1.038	=0+14	2 463	<u> </u>
	7	0.00	· 0 • 0 0	. 1:4879	5+584	:=25 +89	0.838	0 + 65	2.64	
	8	5.00	0 .00	1.585	5 • 485	-ZZ.64	0.828	0 + 1 4	1448	
rt de la constant	9	4.00	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		5 * 2 * 8	-20442	0.962	# #O.96	· + *23	
	10	6.00	ഗത്തെയ്ക്കുന്നു.		5.052	-17,42	1.149	· #1.64	·4442	
	11	8.00	0.00		40774	-15.46	1.418	. =3.15	.4732	
	12	10.00		0.248	. 4.535	-17.23	1.501	*3.37	3,46	
	13	12.00	0.400	0.326	4.315	-14.61	0.871	• •0 •95	2.99	
				• •		>				

YOUGHT LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ID . NO. 106

(RUN 206-RUN 63)/ 1-00

. 3

	TO CO		•						
WIND	AXES	DATA: CO	RRECTED	AMES DAT	A-CORREC	TED SING	LE SUPPO	RT DATA	
PNT	ALPH	A PSI	. L/G,	D/Q.	PM/G	: SF/Q	RH/Q	AWNG	
1	=0.2	4:=28+0Q	. 3+661	14.665	=67 • 97	=5.556	. 36+26	3+54	
ż		4:=26:00	3.329	13.739	=63.55	-5.527	30.32	5.21	
N. 160 S. 184 S. 18		3 =24-00	2.583	13+019		-4-209	28.91	5.81	
*		5 -55-00	1.895	12.373	-51.26	-3.801	25.75	3*78	
5	and the second second	020.00	1.525	1 T T T T T T T T T T T T T T T T T T T	-45.88				
6		6 =18.00	0 . 804	11.463	-44+14	=2.301	22.85	5 4 6 8	The state of the s
7		4 =16+00	0.995	11.071	·#40 • 10	-1.670	. 17 - 94	4 * 43	
7		4 =14+00	1:329	11-001	=37 + 87	=1+476	12-65	7 81	
9		+ -12.00	: 2.096	11.891	5-52+37°	-2.437	9.43	. 15 48	
10		4 =10.00	: 2.766		-59.07	-8.406		19404	
		-8.00	1 2.414	12.204				17.76	
12		46+00	. 2+094	12.376	.=59.47	-1.549	2.87	. 18.58	
13		3 -4-00	1.802	12.274	-57.80	-0.755	1+49	12 • 87	
14		3 . =2+00	1 . 879	12.321	=60.24	=1.335	2.16	13.96	
1.5		4 . 0.00	: 2.037	:12.260		=0.772			
16		2.00	. 1.898	12.341	-54,08	1.263	The second secon		
17		4 . 4 . 400	: 2 FD 93		-56-73	2,699			
18		4 6+00	. 2.157	12.499	-56:37	3.618	⇒5 +18	-12.52	
19	=0.2		. 2.494	12.312	=56+49	4 - 187	· #6.62	9+70	
20		4 10-00	: 2.546	12.652	=56 • 11	5 . 474	#10:27	:=20 499	
21		12.00	2.801	12.7.63	-52-05		-13.55		
.53	-0.2	4 - 14-00	2.534	12+887	-49 #23	6.548	.=19708	:-28-05	
23	-0.2	4 . 16-00	: 2:180		-37 ·66		:-21.77		
24	-0.2	5. 18+00	1.808	12.890	-38+73	6.296	=22.36	-31+79	
25		5 : 20+00	1.320	12.995	-38+78	5.575	:=24+46	-28-19	
26		5: 22 -00	0.890	13 - 147	=44 = 08	5.000	-26-94	-22+20	
27		5: 24.00	0.708	:13-670	45.81	5.430	3-31.38		
28		5 : 26 . 00	1:057	14.168			-40353	a see a fire fire	
29		5 . 28 - 00	J. 0.066	14.751		4,697			
							·····		

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POLICE TEST LOW SPEED WIND TUNNEL TEST 630

DELTA DATA

ಂದಿಯ ಕಂಡ ತಹದನಿಕ್ಕಳು ಕುಂಗಿ ಬರು ನಿರ್ವೀತ

ID-NO. 107

16RUN 107-RUN 451/ 1+00

* 11/23/81 1303

									·	
- The state of the	TITAL		TATA: CO	RRECTED	AMES DAT	A-CORREC	TED SING	LE SUPP	RT DATA	7.
eggegett <u>skilling a skil</u> leng ATOLISE (1985)	Dar	ALPHA	PSI	. L/0	D/Q	PH/Q	SF/Q	RM/Q	YM/Q	ja Alaina kanan aya da da maran ay
	1	=12:00	-0.01	: 2.590	6 • 529	-32.06	=4.604	-15+39	80+70	
	2.	=10.00	· =0 .01	2.340	6 • 4 6 6	-27+35	-5.581	-17.17	92.21	
	3	-8-00	10 -0401	2+495	6+661	-26.07	.=5.882	-16-35	1 96 452	•
*,		-6.00	# -0.01	0.595	6.646	:-22-12	-5.207	-13-13	78.26	
200	<u> </u>		-0.01	0.223	6.331	-19.06	-3.788	-7.58	48-55	
ستايد ما قب تنظيمين خياب آن سيسي	6	-2.00		=0+144	6 • 122	:=22+98	-2.286	-3.56	: 28.26	
	7	0 • 90		=0.416	5 . 841	-26.26	-1.494	=1.56	14+49	
	Ŕ	3.00		= 0 ÷586	5 - +59	=27+42	-0.859	· •1.30	6,90	
	<u>-</u> -	4.00		-0.871	5 - 181	:-27.18	-0.273	· -1.61	· •0°453	->
	10	6200	-0.01	-0-847	4.898	-28.57	0.192	-2.40	-2-14	
-	11		. =0.01		4.678	-28-13	0.577	- 4417	1621	
- ~ ~ ·····	12	10.00		=0.863	4 • 5 4 1	=28.88	0.671	■4.37	1 * 48	
**	13	12.00		=1.009	4 * 417	#29·37	0.738	=8:37	4 453	

APPENDIX B - Run Schedules

This appendix presents the run schedules from Low Speed Wind Tunnel Test 550 conducted in November 1977 and the 40- by 80-foot Wind Tunnel Test also conducted in November 1977.

Table B-I. Run Schedule for Low Speed . Wind Tunnel Test 550

											M	DDE	L (ONE	סודום	NS	- ₁					·		-		· ·	TUNI	EL C	HDITI	NS.	-	1				1	Ì
- 1	RUH NO.	PT. No.				CON	FIG	iúk,	ATIC	Ж				RAI	u NGE Kej	Ψ RANGE (DE61	•	φ φ	TUF	١.	TUFT PICS	PICS	1	- Callery -	resr ¶		361			1	TARE		Ι.	ALIGN	REMARKS •	ENG	
-	*26	ببست	вс	W.,	H, 1	N, F	60	1	rev	Q I	າ ສາ	(TS),	+-	715		+	0	OH	+	-	x	-	+	test) 75	-	94 94		64	29.26	-	876	-	R/liao	Sail on; includes partial lip fairing	RHO	
-	227		77	Ť	Ť	Ť	Ē		\prod			1	_ <u></u>	1		Ť	†	Ť	Ï	7		x	-	7	Ť	-			 	29.27	1	17	-	0/137	Add fuselage afterbody		7
-	*28		-1-1-	!	.J	\vdash	-			П		1	Ī	厂	$ \cdot $		\dagger		$ \cdot $	7		x	╁	7		\vdash			ΙŤ		28	11	7		Wing off	$\dagger \dagger$	1
\prod	29		11	¥2	H ₁	\top				17	-,		7	1			1	1-	П	7		x	1	-	1						27	11	7		Thin wing	11	7
	30					Τ					s ₂	1	7	F			T	1	\prod			x	1	7	7				66	29.27	 	11	1		Aft controls fairing	.11	7
Ţ	31																1									Τ			60	29.43	1	11	7		Thin Wing; repeat of 29	\prod	1
	*32			W ₂																		x							64	29,48	35				Wing trailing edge fairing	\prod	٦
_	33		Ш	W _{3F}	_	ļ	L		Щ					-6	/6							x							66		35				Fillets at wheel pod	\prod	
L	*34		Ц.		L	L			Щ	Ц	J ₂		_	-15	/15		_	L		1		x	_	_					70		34				Float kit	П	
-	35		11	1	_	L		_	\parallel	Ц	J ₂	_	4	<u> </u>		_ _	_	L		_		x	_	_	_						34				Faired float kit		
L	_36		11	₩ <mark>3</mark> r	_	<u>_</u>	_	_	1			_	4	_			_	_	Ц	 -+		x	_	_ .	_ _				71	29.1/9	34	$\perp \downarrow$			Change wing incidence from +5° to 0°	\perp	\bot
_	37			W _{lf}	_	_	_		\parallel	Ц		_	1	_			_ _	Ļ		_		x	1	_	_ _						34				Thick wing T.E. fairings	11	_
L	38			¥ <u>J.</u>	<u> </u> _	_	L	Ц			A	_		_			1	_		_		x	_	_		_	_				23	$\perp \mid \perp \mid$	\rfloor		Stroub's strakes	Ш	
-	39			W _{lf}	-	_	_		4	Н		_		<u> </u>	_	4	_ _	<u> </u>	- -	_		x	_	_	_ _	_					23	44			Thick wing; T.E. fairing	11	_
-	*40			W _{3F}	-	_	L			-		_		<u> </u>	_	_ _	- -	_		_].		x	_	_	_ _	_	_		66	29.70	40	_ _ .		_	Thin wing with T.E. fairing	44	_
Ĵ.	41			W ₃	.	_	-	-	4	Ш		_		 -		_ _	1	┞	OFI	4		x.	- -	_	_ _	_			71	1	40	11	_		Tag. fairing (Cear pod-to-wing pairing still on)	11	_
-	42		++	- -	_	├-	L	H	#	1	5	-		╄			- -	\vdash	\sqcup	4		x	-	_	_ _	-	_		81	29.72	40	- -	_		Fair over exhaust ducts	11	_
-	43		- - -	- -	-	-	-	_	#	-	Y ₁		_	-	!	- -	- -	-	- -	4		X	-		_ -	-			80	- -	110		4	_	Alternate T/R gearbox fairing	44	4
-	1,1,		- - -	- -	-	-	-	-	44	+		-			/25	+	- -	-	\vdash			×	-		- -	-			84	- -	140	+-	-		Remove slat on tail	+	4
-	45				L.	L		<u>_</u>	Ш	Ĺ			X ₂	-15	/15	- -	- -	-	H	4		x	-	\dashv	- -	-	$\left - \right $		85	29.71	1			H/A·	Faired model strut	44	4
-	+46		ــــــــــــــــــــــــــــــــــــــ											\vdash		_L	-	1_	1	-		<u>_x</u>	-	-	_L_	-	-		86	29.68	46	8/43	19	8/439		- -	_
-														┢						-			+-	-		╂-				ļ	 	┥	-			-	_
-				—			_										╢		-	-		 											-			-	
+	-+											_		-			-			-		├	-	_Į		-			 			-	_			-	

& INDICATES STATIC TARE TAKEN

NOTE 1 - Left wing angle incorrect on Runs 29 and 30

Table B-I. (Continued)

:[MODEL C	ONDITIO	ONS							TU	NNEL C	OKDITI	ONS		Ė.	T -		Τ	T
	NO.	PT. NO.	Canalguration	Q RANGE (DES)	∳ RANGE (DE€)	ф	TUFTS		CONF PICS		TEST	9 ₅₆		TÉMP	PRESS	1	T&1	ALIGN	REMARKS	ENGI	RICAT
 						(PE4)				******	(PSF)	the H ² C	1	(n	(IN-HE)						197
-	*1		BCW1 K2 N2 R1z HT TEVGQ P1 P2	15/15	-우_	<u> </u>	CFF		x		75	11.9	<u> </u>	.93	29.31 ¹	1_	B/439	8/439	N-6	RHO	10/3
L	2		TS,						х					11	29,29	1			No.60 grit add to nose, canopy, wing, vert fin, H.T., endplates & cowl. Grit on til		
	3			0							5.0 to	.79 i 11.94	q	90		n/A			further notice. 0-35psf in 5° iner; 35-75 in 10° iner.	П	П
	14		R30	0/-10					х		75	11.9l				1	П			11	11
	5		B.60	-6/6			\sqcap		х		Ιï	П			29.28	1			Stub blades off	1	11
	6			1					х	 		一	1	91	1	1	-	- -	Trees hades of I	11	\forall
							-			<u> </u>	- -	- -	1	1	29.27	1	- -	 -		1+	++
			╽ ╗═┩═┦═┦═ ╏ ═┋═┦═┦═╏ ╏ ╏╏			<u> </u>	-			 -	 	- -	-	17	59.61		 - -	┞┼		╫┼	++
p -	-9		R ₁₄	15/15 -6/6	H	 			Х		 - -	╁	┼			1	$\vdash\vdash$	╁┼	Main rotor off		+-!
J -	-9		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6/6	- -		-		_x	 —	 - -	- -	-	86	29,25	1	- -	 - -	Stub blades on		11/2
-	-10		╽┧╌┠╌┨╼╏╌[╩] ╋═╂═╏╕╏╡╏╂╏═┸╂╏╴	-1	-						<u> -</u>	-	-	┦		1	 	- -		++	44
-	11		┟┦═╁═┧═┧═╁═╁═╏═╏╒┦╒┦┸┻═╂┸	15/15	-		<u> -</u>				- -	- -	-	81.	29.26	1	 	 	Flt, test protrusions removed	\perp	4
_	15		<u> </u>	-					х				_	79	29.26	1	1_ _		Prod. protrusions removed	Ш	
L	*13]							x		<u> </u>					13			Hain rotor off		
	14								X					81.	29.30	13			Tail rotor off	П	T
Į	15		н, п,						х			\Box		79	29.25	13			Jand, gear doors on	TT	\prod
	16								x					TŤ	\sqcap	13			Wings off	T	
	17						-		x			-	1	82		13	1-1-	- -	Endplates off	11	+
	*18						-				-	- -	+	-	29.27	18	- -	1-1-	Horiz, tails off	11	+
_			 - - - - - - - - -	11-			 		<u>x</u>		- -	- -	-	17	53.51	1	- -	┨╼┟╼		╁┼	+
	19	—Ì		 -	-		 - - -		<u>x</u>		┼┼╴	- -	-	 	╢	18	┦ ╌	 	T/R guard antenna off	-	+
-	×20		W ₃ M ₁ R _{1a} n [†] TE V G	 		├-{	 - -		_ <u>x</u> _	FLOW	╂╼╂╌	- -	-∤	 	<u> </u>	20	- -	 	Vert, fin off	- -	41
-	57		W ₁ M ₁ R _{1s} HTE V C	-1-		-	<u> </u>		x	PICS		i- -		62	29.30	-1	- -	-	Flor visualization	- -	_ 11.
- -	*22		╽┈╎┈┝┉╏┈╸┝┉╶┨╸╸╇┈ ╌┼┑╏╶┠╼┞═┨╸╼═╸┈═╂╸╸ ╴	15/27	-	<u> </u>	ON	·	<u>x</u>	 		<u> </u>	<u> </u>	68		22_	_	_ _	Stub blades off		
]_	×23			-15/15	. .l	Ц			x	ļ <u>.</u>	1	<u> </u>	ļ	65	29.30	23		<u> </u>	Exhaust fairing		
	24			0	-30/30					<u> </u>				69		24	11/43		Stability run		
	25		L	-6/6	0		11		х	1		1		66	29.28	23	8/439	1	Fair over cost hip		

^{*} INDICATES STATIC TARE TAKEN

Table B-II. Run Sch ule for Full-Scale M222 Test in 40- by 80-Foot Wind Tunnel.

STATIC	, DATA	•					
TARE	RUN	ģ.	CONFIGURATION .	2	Ψ	C REMARKS	
1		5	HELICOPTER SURFORT STRUCTURE WITH DUMMY 7" DIAMETER STRUT, NEITHER VERTICAL FAIRING INSTALLED	c	-30°/30°	 STATIC TARE RUH TO VERIFY HO INTERFERENCES	OF POOR
	1	16.6	WIND OX TARE RIM	0	0 /+30	TARE RUN TO GET DRAG OF SUPPORT STRUCTURE IN YAW	7
	2	32	WIND CH TARE RUN	٥	-30" /30"		
z		5	LARGE ISCTICAL FAIRING AND DUMMY STAUT FAIRING INSTALLED, THE RO	-15 /+15	-		05
	3	65	WIND ON TARE BUN	-15/15			
3		s	DUMMY STRIT AND ITS FAIRING REMOVED	-15/415	a	LARGER VENTICAL FAIRING STILL ON	
	4	65	WIND ON TARE RUN	-15 /+15	1		
4			•	-15/+15		STATE TAKE FOR JUDGE CONCRETE ATTEM	
+ 555 5555544444444677777778900 UUUUU	5 6 7 6 9 0 1 1 2 3 14 5 6 7 18 19 0 1 2 2 3 4 5 6 7 18 2 3 14 5 7 18 2 3 14 5	0 70 30 65 440		-15 /+15 -14 /+15 -14 /+15 -14 /+15 -14 /+16 -16 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -10 /+16 -11 /+17 -12 /+17 -12 /+17 -12 /+17 -12 /+17 -12 /+17		STATIC TAKE FOR INITIAL CONFIGURATION WIND ON, THIS RIM ABORTED DUE TO STRIKE OF YAM BOOM AND A MAIN RODE ASILY REMOVED, FOULD BETWEEN SUSPENT FAIRING CREEKE C. SKIP GEAR UNDERSELLY FAIRINGS OFF, FUEL SUMMER ARE EXPOSED MOSE FLOAT BASE OFF YOU BY REMOVED COMP (ENTER SUPPORT CARE), MAIN ROTCE FLIP RING. SKIP GEAR CREEK THE FAIRINGS OFF, CROSS THEE TAMBURE HAVE OF FOR FAIRING HOSE FLOAT BAGS AND ALIGN FLOAT SWITCHES FLA SKIP LANDING GEAR OFF RESCUE HOIST FAIRING OFF RESCUE HOIST FAIRING OFF RESCUE HOIST FAIRING OFF RED WEDGE-SHAPED AFTERBODIES TO THE WING FLOAT TIPE ENTIRE FLOAT KIT OFF ROD MAIN FOFOR ASTY, WO STUE BLADES, SET TO TO ABIMUTH AZIMUTE CHANGES TO SAS, SHOULD HAVE SEEN GO """""""""""""""""""""""""""""""""""	ROTES, LINE ON TOTE EVALUATED TOTE, FARENCE STILL CO. TOTE, FARENCE STILL CO. TOTES TOTELLED TOTELLED

Table B-II (continued)

TIRE R	ATA .	4		C	Cafig	URATION				<u>ا</u>	ψ	REMARKS
11	11 12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	25 A A A A A A A A A A A A A A A A A A A	E POR PRESENTATION PROPERTY OF THE PROPERTY OF	H			12°	74 Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	I ₂ J ₂ J ₃ Q A	-12/41 -6/48 -6/48 -12/41 -12/41 -12/41 -12/41 -12/41 -6/46 -6/		INTIGHT FLIGHT TEST EXPANSE ETECTOR FAIRINGS, FARME OF LOTY UND THE FAIRING PERSON ENGANT MUMP TAKEN EDGE FAIRING. RECOVE EXCHAIN EACH PRINCE PARTIES. RECOVE EXCHAIN EACH EXPLANT EDGE FAIRINGS. FILL SAIL INTIGHED FAIRING. ON FIX MAIN ROTOR AT 60 ARIMOTY. REMOVE ANY ROTATION CONTRILS FAIRING. PLEASANT TOLL-RATOR GEARGIA FAIRING, SO-CALLED "COPPANAN" FAIRING. PLEASANTE TOLL-RATOR GEARGIA FAIRING, SO-CALLED "COPPANAN" FAIRING. "HESTER" LARGE FILLET AT WHEEL FOR REMOVED FAM. MING. "COPPANAN" FAIRING. "HESTER" LARGE FILLET AT WHEEL FOR REMOVED FAM. MING. HERIZOCITIAN THE WING. HERIZOCITIAN THE WING. HERIZOCITIAN FAIR SAIL SLAT REMOVED FARED MAIN FORM ARIL, NO STUB BLADES, AZIAUTH POSITION GURSTICHARIS ARILAND FARED MAIN FORM ARIL, NO STUB BLADES, AZIAUTH POSITION GURSTICHARIS ARILAND MINGALE FLOAT INFLATION SUITCHES, PLICAND FIA, SLATED FLOAT NEIS BASS INSTALLED HERIZOCITAL STABILIZE EMIDDLATES RAMBURD. IN 80 GAIRA ALIGARD FIA, SLATER SHIGHT NAT MINGALED HARIZOCITAL STABILIZER EMIDDLATES RAMBURD FIA, SLATER SHIGHT NAT MINGALED HARIZOCITAL STABILIZER EMIDDLATES RAMBURD. FLOAT STABILIZER EMIDDLATES RAMBURD FOR SUITCHES FAIR SAILED FLOAT NOSE BASS AND SUITCHES REMOVED MAIN ROTOR ACTY, CLEMBROS FERROVED FROM FLOAT THE FAIR ROTOR ACTY, CLEMBROS FERROVED FROM FLOAT THE FLOAT NOSE BASS AND SUITCHES REMOVED MAIN ROTOR ACTY, CLEMBROS FERROVED FROM FLOAT FLOAT SHE BASE AND SUITCHES REMOVED STANDARD WING BAKE ON, MAIN GEAR DOOR ON, GAAR FETRACTED VOCTER GENERATIES HISTALLED ON SIE OF FURLAGE WING TEACHER PLAY PAGE MINGTER FAIL MAIN ROTOR ATTY, TURNING 2 90 TO NR., OPEN MINGT FEXINATE PLAY FAIR MORPHED FILL SAIL AFT THE OF FORWARD FOUR COOLING SCREEN UNICOTERED REMOVED FAIL MORPHED FILL SAIL AFT THE OF FORWARD FOUR COOLING SCREEN UNICOTERED REMOVED FAIL MAIN PAGE ATTY, TURNING AT 3072 HK